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# Solid by-products of a  $CF<sub>3</sub>I-CO<sub>2</sub>$  insulating gas mixtures on electrodes after lightning impulse breakdown

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#### Abstract

This paper investigates the solid by-products of  $CF_3I-CO_2$  gas mixtures and their proposed use as an alternative insulation medium in gas insulated switchgear and lines. The deposited by-products of a  $30\% - 70\% \text{ CF}_3$ I–CO<sub>2</sub> gas mixture are experimentally investigated using stainless steel, aluminium and copper contacts whilst a standard 50 kV lightning impulse is used to cause electrical breakdown in the gas mixture. Following breakdown, the accumulated by-products over the electrodes surface were examined using an imaging microscope and scanning electron microscope. This paper discusses the results of microscope analysis on the surface of the electrodes and explores the effects that the detected by-products could have on high voltage  $CF_3I-CO_2$  gas insulated equipment.

## 1. Introduction

Sulphur hexafluoride  $(SF_6)$  is the most reliable gas insulation medium used worldwide in the power industry in gas insulated switchgear (GIS) and gas insulated lines (GIL).  $SF<sub>6</sub>$  is used in the power industry because it has an insulation strength approximately three times that of air at atmospheric pressure which has led to compact and reliable GIS and GIL equipment [[1](#page-15-0)].  $SF<sub>6</sub>$  is also chemically inert and has advantageous arc extinction qualities. However, it is now widely known that the global warming potential (GWP) of  $SF<sub>6</sub>$  is extremely high, with a value of [2](#page-15-0)3 900 times that of CO<sub>2</sub> [2]. SF<sub>6</sub> also has a reported atmospheric lifetime of 3200 years [2] which coupled with its infrared radiative capabilities has led to its extremely damaging effect on the environment when released into the atmosphere. It is important that any substitute insulating gas possess a high insulation strength at a relative low pressure whilst maintaining long term stability in any container. Furthermore, it is important that if any breakdown occurs in the gas, it can recover without a vast increase in by-products. If by-products occur that reduce or compromise the overall insulation capability of the gas, this could affect the long-term usefulness of any alternative insulation medium.

One alternative insulation gas that shows promising insulation properties to replace  $SF_6$  is Trifluoroiodomethane (CF<sub>[3](#page-15-0)</sub>I) and its mixtures [3]. An important characteristic of CF<sub>3</sub>I includes its ability to rapidly decompose in solar light which results in a GWP of less than  $5[4]$  $5[4]$  $5[4]$ . CF<sub>3</sub>I also has an extremely short atmospheric lifetime of less than 2 days[[4](#page-15-0)]. The result of CF3I's short atmospheric lifetime and its very low GWP mean that its negative effect on the environment is virtually non-existent compared to  $SF_6$ .

Under uniform field conditions, it has been shown that  $CF_3I$  has a breakdown voltage 1.2 times that of  $SF_6$ [[4](#page-15-0)] and so could potentially be used to insulate future power equipment. It is, therefore, important that research, such as that conducted in this paper, examines the effects of breakdown on this new insulation medium and examines its deposited by-products when in close proximity to common materials used in GIS and GIL.

When examining the by-products of CF<sub>3</sub>I, it is important to note that  $SF<sub>6</sub>$ , which is currently used in the power industry, produces many by-products when subjected to a high voltage breakdown, such as SOF<sub>2</sub> (Thionyl Fluoride), SO<sub>2</sub> (Sulphur Dioxide), SO<sub>2</sub>F<sub>2</sub> (Sulphuryl Fluoride), SOF<sub>4</sub> (Sulphur Oxide Tetrafluoride),  $SiF<sub>4</sub>$  (Silicon tetrafluoride) and CF<sub>4</sub> (Carbon Tetrafluoride) which can, in most cases, be removed using



absorbents [[5](#page-15-0)].  $SF<sub>6</sub>$  also produces solid by-products during arcing such as metal fluoride (white) powders which are extremely acidic [[5](#page-15-0)].

In this paper, the deposited surface by-products of a  $30\% - 70\%$  CF<sub>3</sub>I–CO<sub>2</sub> gas mixture are examined following electrical breakdown due to lightning impulses being applied to a point-plane electrode configuration. These studies will help improve understanding of the process that takes place across gas gaps in switchgear[[6](#page-15-0)] and GILs [[7](#page-15-0)] if insulated by  $CF_3I$ –CO<sub>2</sub> gas mixtures. Research has shown that  $CF_3I$ –CO<sub>2</sub> gas mixtures are capable of insulating gas gaps in MV switchgear[[6](#page-15-0)] and models of GILs[[7](#page-15-0)]. However, little is known about the deposited by-products that gas breakdown could produce. In [[8](#page-15-0)] the production of Iodine  $(I_2)$  is simulated and theorised from a CF<sub>3</sub>I–CO<sub>2</sub> gas mixture but not experimentally proven by using an SEM/EDX as is shown in this paper. In [[8](#page-15-0), [9](#page-15-0)] the insulation characteristics of  $CF_3I-CO_2$  gas mixtures is evaluated using partial discharge inception voltage. This paper examines the deposited surface by-products created during this process and further develops the process of detecting solid by products [[10](#page-15-0), [11](#page-15-0)]. This paper experimentally uses an SEM/EDX to identify the solid by-products produced by a CF<sub>3</sub>I–CO<sub>2</sub> gas mixture, a task which has not previously been undertaken.

#### 2. Experimental test setup

Throughout the experimental research conducted in the following sections, the deposited by-products produced on the surface of electrodes made of common GIS and GIL materials were investigated. In this experiment, a high voltage impulse generator was used to apply a 50 kV standard positive lightning impulse  $(1.2/50 \,\mu s)$ , at a current level of 165 A, to the point electrode for all material types. The equivalent circuit diagram is shown in figure 1 and an example waveform of the voltage (no breakdown) and current (after breakdown) is shown in figure [2.](#page-3-0) The build-up of by-products was examined after breakdown events occurred. A gas mixture of 30%–70% CF<sub>3</sub>I–CO<sub>2</sub> was used throughout the testing program with the gas insulation medium separating a point-plane electrode configuration as shown in figure [3.](#page-3-0)

In each experiment, the pressure vessel, shown in figure [4](#page-3-0)(a), contained the test electrode system and was evacuated using a vacuum pump. A gas mixture of  $30\% - 70\%$  CF<sub>3</sub>I–CO<sub>2</sub> was then used to fill in the pressure vessel at a pressure of 0.15 MPa or 0.5 bar(above atmospheric pressure) and the breakdown test undertaken. After each breakdown test, the gas mixture was re-covered and re-used using the equipment shown in figure [4](#page-3-0)(b).

In order to test different materials, three point electrodes were constructed from 5 mm diameter stainless steel, aluminium and copper with a rod having a tip length of 10 mm. These point electrodes were each connected in turn to an air insulated bushing through which the lightning impulse was applied. In each system, the plane electrode was 45 mm in diameter with a rounded edge and is constructed from the same stainless steel, aluminium and copper alloys as the point electrode. An approximate inter electrode gas gap of 20 mm of 30%–  $70\%$  CF<sub>3</sub>I–CO<sub>2</sub> was then set between the electrodes for testing.

A Zeiss Axio Imager M2m imaging microscope was used to examine the surface defects of lightning impulses on each polished plane contact for each material. A Hitachi TM3030 scanning electron microscope (SEM/EDX)

<span id="page-3-0"></span>





Figure 3. Gas chamber point-plane electrode geometry.



Figure 4. Rigs and test facilities. (a) Pressurised test vessel with window during lighting impulse breakdown and (b) gas mixture filling and recovery equipment.

was also used to identify basic material elements of by-products that were deposited on the surface of the different electrodes after 1, 3 and 400 lightning impulse flashovers had been applied. The SEM/EDX analysis conducted after 1 lightning impulse shows the by-products produced from the gas mixture. Analysis after 3 impulses demonstrated that surface effects were repeatable. The use of 400 lightning impulse breakdowns allowed for the continued production of by-products to be demonstrated and analysis to show whether new byproducts were produced in such quantities that they could not have been detected after only 1 breakdown.

## 3. Stainless steel electrode test results

This section utilises point-plane electrodes made from stainless steel. Stainless steel was chosen because previous research has indicated that when CF3I is stored in close proximity to stainless steel, no degrading or chemical

% Present from speci- fication $[13]$	% Present from SEM/EDX analysis
$17.5 - 19.5$	22.92
$8.0 - 10.5$	12.22
$0.0 - 2.0$	$\Omega$
$0.0 - 1.0$	$\Omega$
$0.0 - 0.11$	$\Omega$
$0.0 - 0.05$	$\Omega$
$0.0 - 0.03$	$\Omega$
$0.0 - 0.03$	0
Balance	64.85

Table 1.Chemical composition of stainless steel (grade 1.4307).



interaction could be observed [[12](#page-15-0)]. Stainless steel alloy grade 1.4301/304 (Commercial designation 304L)was chosen because of the relatively few elements that exist within its chemical composition in any large quantities as shown in table 1. Figure 5 shows the SEM/EDX examination result of a small area of the surface of the stainless steel electrode before any breakdown test was undertaken which also indicates the percentage of elements detected. As shown in table 1, the SEM/EDX results and the specified elements from the datasheet of the stainless steel alloy are in good agreement. The slight differences can be attributed to the limited viewing window of the SEM/EDX which is a small 2D surface. It is expected that slightly different compositions may be present for different surface areas of the same contact.

A single lightning impulse at 50 kV was then applied to the point electrode, and the voltage of the gas breakdown through the 30%–70%  $CF_3I$ – $CO_2$  gas mixture was measured using a capacitive impulse voltage divider. After the gas mixture had been recovered from the pressure vessel, the plane electrode was examined using the imaging microscope, and the resulting impact of the breakdown on the stainless steel plane contact is captured in figure [6.](#page-5-0) The same imaging microscope is further utilized under dark light conditions, as shown in figure [7](#page-5-0), to highlight the exact surface defects that have been introduced as a consequence of the gas mixture breakdown onto the previously mirror finished electrode.

The same electrode is then analysed using the SEM/EDX and the center of the breakdown impact is shown in figure [8](#page-5-0). The detected elements from the area displayed in figure [8](#page-5-0) are shown in figure [9.](#page-6-0) By identifying the differences between figures 5 and [9](#page-6-0), the new elements that are deposited on the stainless steel electrode surface due to a CF<sub>3</sub>I–CO<sub>2</sub> gas mixture breakdown should be more identifiable. From the analysis undertaken using the SEM/EDX, it is clear that an increase in carbon deposits is identified and possible iodine deposition is seen. However, because the identifiable energy levels of iodine and chromium are very close to each other, it is quite difficult to distinguish between the two elements and identify exactly how much iodine might be deposited on the contacts surface as a result of breakdown in  $CF<sub>3</sub>I$  gas mixtures.

Subsequent testing involved three lightning impulses impacting a new polished stainless steel plane electrode as shown in figure [10.](#page-6-0) This is important as the surface effects of each impulse can be seen to exhibit similar surface deformation/deposits and indicates the repeatability of the SEM/EDX results shown in figure [9](#page-6-0). Each individual breakdown impact indicates a similar element percentage present in and around each area as that shown in figure [9.](#page-6-0) Figure [10](#page-6-0) also shows how the surface of the stainless steel electrode, previously polished silver in colour, has been turned a brown colour around the breakdown arc impact area. Figure [11](#page-7-0) shows the center of

4

<span id="page-5-0"></span>

Figure 6. Polished stainless steel plane electrode after one lightning impulse breakdown to the surface as observed through an imaging microscope (bright light setting).



Figure 7. Polished stainless steel plane electrode after one lightning impulse breakdown to the surface as observed through an imaging microscope (dark light setting).



<span id="page-6-0"></span>



one such impact which is also brown. This is important as deposits of iodine are often brown, as shown by the work carried out in [[14](#page-15-0)].

## 4. Aluminium electrode test results

In this section, we report the surface examination results following CF<sub>3</sub>I gas mixture breakdown in an aluminium point-plane electrode system. The results of surface degradation and deposits are examined when the aluminium electrodes are placed in a pressure vessel with a 30%–70%  $CF_3I$ – $CO_2$  gas mixture that undergoes breakdown when subjected to a 50 kV lightning impulse. The results with aluminium will be useful to evaluate the probable utilisation of  $CF_3I-CO_2$  gas mixtures in gas insulated lines where aluminium is commonly used to manufacture the enclosure and central conductor  $[15]$  $[15]$  $[15]$ . The aluminium contacts in this research are manufactured from aluminium grade 6082/T6, and the specified percentage of alloy elements are shown in table [2.](#page-7-0)

Initially, the aluminium plane contact is examined under an imaging microscope after being polished to a mirror finish. It can be observed from figure [12](#page-7-0) that the plane contact has more scratches than stainless steel.

<span id="page-7-0"></span>

Figure 11. The center of a lightning impulse impact on a stainless steel polished plane electrode as observed through an imaging microscope (bright light setting). The area shown in figure 11. is shown as a dashed box in figure [10](#page-6-0).







Figure 12. Polished aluminium plane electrode before a lightning impulse is applied as observed through an imaging microscope (bright light setting).

This is because aluminium is a softer alloy and is more susceptible to surface defects. After examination under the SEM/EDX, the results for detectable elements are shown in figure [13.](#page-8-0) These elements, as a percentage of a small area of the total surface, are shown in table 2. It can be shown that although most elements are present in similar values to those specified, the amount of manganese (Mn) present on the surface of the plane contact is higher than specified, and so may have an impact on the obtained results which are presented here.

Following the initial evaluation of the composition of the aluminium plane electrode, a single 50 kV lightning impulse was applied to the point aluminium electrode, which initiated breakdown across the 30%– 70%  $CF<sub>3</sub>I-CO<sub>2</sub>$  gas mixture. The resulting impact of the lightning impulse, on the aluminium plane contact, can be seen in figure [14](#page-8-0). In general, it has been found that developing streamers branch out and propagate short distances to form corona in air [[17](#page-15-0)], and it is likely that a similar process takes place in  $CF_3I$ –CO<sub>2</sub> gas mixtures. This branching process is clearly visible in figure [14.](#page-8-0) Figure [15](#page-8-0) shows an enlarged image of the branching effect observed from the center of the breakdown across the surface of the aluminium under an imaging microscope.

<span id="page-8-0"></span>





Figure 15. Polished aluminium plane electrode after 1 lightning impulse breakdown to the surface as observed through an imaging microscope showing branching effect (bright light setting).

Evaluation of this single lightning impulse breakdown on an aluminium contact under the SEM/EDX gives the image shown in figure [16.](#page-9-0) In this figure, it can be seen that there is a round central impact region. To the naked eye, this is brown in colour. The elements detected by the SEM/EDX are overlaid on the image and the distribution is shown in figure [17.](#page-9-0) As can be seen in figure [17,](#page-9-0) iodine is deposited across a large area of the

<span id="page-9-0"></span>

Figure 16. Polished aluminium plane electrode after 1 lightning impulse breakdown to the surface as observed through the SEM.





Iodine (I)—75.85%, Manganese (Mn)—1.82%, Magnesium (Mg)—0.39%, Aluminium (Al)—21.18%, Silicon (Si)—0.36%.

electrode, and it is not only concentrated at the centre of the breakdown impact region. This means that an absorbent for iodine may be needed to minimize or prevent detrimental effects inside GIS and GIL. Figure 18 shows the graphical representation of the elements shown in figure 17. It is important to note that a quick comparison of the percentage of elements found in figures [13](#page-8-0) and 18 indicates that, although iodine is detected, the peak that represents the existence of manganese is in exactly the same energy region and it very difficult for

Table 3.Chemical composition of copper(CW004A).





Figure 19. Polished copper plane electrode after 1 lightning impulse breakdown to the surface as observed through an imaging microscope (bright light setting).

the SEM/EDX to distinguish between the two elements. However, the percentage of elements shown on the surface of the contact in figure [18](#page-9-0) seems to identify an increase in the amount of iodine detected on the surface of the electrode.

#### 5. Copper electrode test results

In this section, copper electrodes were used for both the plane and point electrodes to examine the by-products deposited on these electrodes following the breakdown of a 30%-70% CF<sub>3</sub>I-CO<sub>2</sub> gas mixture. Copper tungsten electrode tips are commonly used in GIS in order to prevent arcing deterioration [[18](#page-15-0)], and so it is important to understand the by-products produced when copper electrodes and a  $CF<sub>3</sub>I-CO<sub>2</sub>$  gas mixture are used.

The copper electrodes used in this investigation were all manufactured from copper commercial grade C1101/CW004A as shown in table 3. A sample of this copper was analysed using a scanning electron microscope (SEM/EDX), and the results of this are also shown in table 3. These results indicate that the electrode was made up almost entirely of copper and that, in the sample area, there may have been a small level of impurity, but the quantities of these elements were not large enough to register on the SEM/EDX analysis.

Initially, a single 50 kV lightning impulse was applied to the copper point electrode, which results in the point-plane electrode electric breakdown of the 30%–70% CF<sub>3</sub>I–CO<sub>2</sub> gas mixture. The impact on the surface of the copper plane electrode can be seen in figure 19. Using the SEM/EDX, the elements extracted from figure 19 are shown in figure [20](#page-11-0)where the elements detected are detailed and the presence of iodine is visible on the electrode surface. However, it is not present in sufficient quantities high enough to register clearly on the SEM/EDX.

Following this initial test, a new copper electrode was used. Three lightning impulses at 50 kV were applied to the plane electrode, and the surface effect of this is shown in figure [21](#page-11-0).

In figure [22](#page-11-0), an enlarged version of the central impact shown in figure [21](#page-11-0) is displayed. A close-up of the branching effect of the impact on the surface of the copper electrode is shown in figure [23](#page-12-0). When the surface breakdown impacts regions from figure [21](#page-11-0) are compared against the image shown in figure 19, it can be shown that this impacted region is repeatable. SEM/EDX results of impacts shown in figure [21](#page-11-0) also show that iodine is present across the surface of the plane electrode. However, the very small quantity makes it difficult to identify clearly.

After these initial lightning impulse tests through  $CF_3I-CO_2$  gas, a copper electrode with 400 lightning impulse breakdowns at 50 kV was tested and analysed. Four hundred lightning impulses were applied with the objective to produce larger quantities of by-products which should be easier to identify positively. The copper

<span id="page-11-0"></span>





Figure 21. Polished copper plane electrode after 3 successive lightning impulse breakdowns to the surface as observed through an imaging microscope (bright light setting).





electrode surface with four hundred lightning impulse impacts from breakdown through the 30%–70%  $CF<sub>3</sub>I-CO<sub>2</sub>$  gas mixture is shown in figure [24,](#page-12-0) where it is clear that all lightning impulses attached at the centre of the electrode and none impacted close to the edge of the electrode. The central region of breakdown impacts is shown in figure [25](#page-12-0). It is important to note that the branching effect shown in figure [23](#page-12-0) is no longer visible in figure [25](#page-12-0) because of the extent of breakdown impacts in this small region.

The central region shown in figure [25](#page-12-0) is examined using the SEM, as shown in figure [26](#page-13-0). This image is then analysed for constituent elements, as shown in figure [27.](#page-13-0) From figure [28](#page-13-0), it is evident that iodine is now present

<span id="page-12-0"></span>

Figure 23. Polished copper plane electrode after three lightning impulse breakdown to the surface as observed through an imaging microscope showing branching effect (bright light setting).



Figure 24. Polished copper plane electrode after 400 successive lightning impulse breakdowns to the surface.





<span id="page-13-0"></span>







at the centre of the electrode. Iodine is positively identified by the initial peak at energy level 0.5 keV in figure 28 and also by the subsequent peaks around 4 keV which clearly indicate the iodine's unique presence.

SEM/EDX analysis was also undertaken on the edge of the copper electrode that was subjected to 400 gas breakdowns. The elements present on the surface clearly indicate that iodine is spread not only around the center of the electrode but also at the edges. After examining the iodine deposited on the electrode, it is clear that Table 4. Summary of added elements on electrode surface.



a light covering can be observed on the electrode but not in large quantities. It is likely that iodine separates from  $CF<sub>3</sub>I$  in the hot temperature inside the leader arc inbetween the point-plane electrode geometry when this is more than 457.4 K or 184  $^{\circ}$ C, which is the boiling point of iodine [[20](#page-15-0)]. Once the iodine separates from CF<sub>3</sub>I, it boils into a gas form and then spreads throughout the pressure vessel, when the iodine gas sufficiently cools below 386.85 K or 114 °C [[20](#page-15-0)], it will change phase to solid and deposit on any surface, including the electrodes within the vessel. If this iodine could be absorbed during its gaseous state, it could be completely removed from GIS and GIL equipment and subsequently pose little problems for  $CF<sub>3</sub>I-CO<sub>2</sub>$  gas mixtures use in power equipment.

#### 6. Discussion

This paper examines the interaction of 30%–70%  $CF_3I$ – $CO_2$  gas mixtures with aluminium, stainless steel and copper electrodes when a 50 kV lightning impulse breakdown occurs across an electrode gap. The results are summarised in table 4. The results show that, with stainless steel contacts, brown deposits are left on the surface and that iodine is detected using an SEM/EDX. However, the chromium within the contacts makes it difficult to detect the exact by-products and in what percentage they are produced. When aluminium electrodes are used, a breakdown through the gas mixture clearly produces a branching pattern from the point of impact across the surface of the plane electrode. When surface deposits are analysed using the SEM/EDX on the aluminium contact, iodine was detected as a by-product. However, due to the manganese in the contact, it is difficult to define clearly the exact by-product element.

Copper electrodes were also examined and, because of the purity of the electrode, it was easier to identify deposits of iodine on the surface of the electrode. However, it took four hundred impulses to produce iodine in a quantity that was recognisable. Four hundred impulses is approximately equivalent to half the operations of a rated gas insulated switch disconnector on the network today, which is rated for 1000 operations[[21](#page-15-0)]. This means that throughout a piece of switchgear's lifetime, insulated by a 30%–70% CF<sub>3</sub>I–CO<sub>2</sub> gas mixture, it would be unlikely that iodine would be produced in large quantities. However, because of the low current of these impulses, it is possible that iodine may be produced in larger quantities in real-life equipment if high current arcs are present.

With the copper electrodes, the SEM/EDX indicates that the iodine is deposited in a widespread area which would make the use of an absorbent easier in GIS and GIL equipment, especially during iodine gaseous state when heated.

## 7. Conclusion

This paper experimentally demonstrates the effect of 50 kV lightning impulse breakdowns across a 30%–70%  $CF<sub>3</sub>I-CO<sub>2</sub>$  gas mixture in order to evaluate the solid by-products produced. It is shown that iodine is produced in small quantities as a solid by-product after 400 breakdowns. However, it is difficult to detect as a by-product after 1 or 3 breakdowns.

When using stainless steel or aluminium electrodes, it is difficult to detect iodine using an SEM/EDX as alloy components affect clear detection. However, iodine is easier to detect on copper electrodes. It was observed and shown experimentally that iodine was spread in a wide area inside the pressure vessel tested. This indicates that iodine is produced as a gas inside the hot breakdown arc before cooling to become a solid deposited by-product. This paper demonstrated the likely effect of a breakdown within GIS/GIL equipment which is insulated with a  $CF<sub>3</sub>I-CO<sub>2</sub>$  gas mixture and the resulting iodine by-products from a breakdown event. If an absorbent could be used to absorb iodine during its gaseous state, it would likely have little impact on the lifetime insulation of a piece of GIS or GIL. Future work will examine the gaseous by-products that are produced by  $CF_3I-CO_2$  gas mixtures through the use of gas chromatography and mass spectrometry.

## <span id="page-15-0"></span>Acknowledgments

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