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## A hybrid strain and thermal energy harvester based on an infra-red sensitive Er<sup>3+</sup> modified poly(vinylidene fluoride) ferroelectret structure

Sujoy Kumar Ghosh<sup>1</sup>, Mengying Xie<sup>3</sup>, Christopher Rhys Bowen<sup>3</sup>, Philip R. Davies<sup>4</sup>, David J. Morgan<sup>4</sup> & Dipankar Mandal<sup>1,2</sup>

In this paper, a novel infra-red (IR) sensitive Er<sup>3+</sup> modified poly(vinylidene fluoride) (PVDF) (Er-PVDF) film is developed for converting both mechanical and thermal energies into useful electrical power. The addition of Er<sup>3+</sup> to PVDF is shown to improve piezoelectric properties due to the formation of a self-polarized ferroelectric  $\beta$ -phase and the creation of an electret-like porous structure. In addition, we demonstrate that Er<sup>3+</sup> acts to enhance heat transfer into the Er-PVDF film due to its excellent infrared absorbance, which, leads to rapid and large temperature fluctuations and improved pyroelectric energy transformation. We demonstrate the potential of this novel material for mechanical energy harvesting by creating a durable ferroelectret energy harvester/nanogenerator (FTNG). The high thermal stability of the  $\beta$ -phase enables the FTNG to harvest large temperature fluctuations ( $\Delta T \sim 24$  K). Moreover, the superior mechanosensitivity,  $S_M \sim 3.4 \text{ VPa}^{-1}$  of the FTNG enables the design of a wearable self-powered health-care monitoring system by human-machine integration. The combination of rare-earth ion, Er<sup>3+</sup> with the ferroelectricity of PVDF provides a new and robust approach for delivering smart materials and structures for self-powered wireless technologies, sensors and Internet of Things (IoT) devices.

There is a widely recognized need for the development of sustainable energy sources for our modern society due to the depletion of fossil energy resources and their impact on the world atmosphere. The miniaturization of commercial wearable device systems, wireless sensors and small electronic systems has reduced their power requirement to the mW and even  $\mu\text{W}$  level. In this regard, the conversion of fluctuating mechanical and thermal energies into electrical energy by exploiting piezoelectric and pyroelectric materials has attracted considerable attention<sup>1-6</sup>. Despite the high piezoelectric activity and properties of several inorganic and semiconducting piezoelectric materials, their toxicity (many contain lead for example), high processing temperatures, complex fabrication steps, and their intrinsic rigid and brittle mechanical properties restrict some of their practical applications<sup>7</sup>. In contrast, piezoelectric polymers such as poly(vinylidene fluoride) (PVDF) and its co-polymers exhibit a number of attractive properties such as, flexibility, light weight, chemical resistivity, large area processing feasibility, low processing temperature and environmental compatibility (lead free). In recent years, it has been noticed that PVDF is one of the most studied engineering polymers due to its ferro-, piezo- and pyro-electric properties<sup>8</sup>. The material is a semi-crystalline polymer that exhibits primarily four crystalline polymorphs; namely  $\alpha$ -,  $\beta$ -,  $\gamma$ -, and  $\delta$ -phases. Among them, the  $\beta$ -,  $\gamma$ -, and  $\delta$ -phases are electro-active. In particular,  $\beta$ -phase (all trans, *i.e.*, TTTT conformation) is fully polar and ferroelectric, as the polarization can be repeatedly switched between opposite but energetically equivalent directions along the two-fold *b*-axis compared to paraelectric  $\alpha$ -phase (TGTG $\bar{c}$  conformation). Thus, the presence of  $\beta$ -phase in PVDF films is highly desirable as it can provide ferroelectric properties, necessary for sensors, actuators, electro-optical, non-volatile memory and biomedical

<sup>1</sup>Organic Nano-Piezoelectric Device Laboratory (ONPDL), Department of Physics, Jadavpur University, Kolkata, 700032, India. <sup>2</sup>Institute of Nano Science and Technology, Phase-10, Sector-64, Mohali, 160062, India. <sup>3</sup>Department of Mechanical Engineering, University of Bath, Bath, BA2 7AY, UK. <sup>4</sup>Cardiff Catalysis Institute, School of Chemistry, Cardiff University, Cardiff, CF10 3AT, United Kingdom. Correspondence and requests for materials should be addressed to D.M. (email: [dipankar@phys.jdvu.ac.in](mailto:dipankar@phys.jdvu.ac.in))

applications<sup>9</sup>. In addition, ferroelectric poly(vinylidene fluoride-co-trifluoroethylene), P(VDF-TrFE), a copolymer of PVDF, is attractive for device fabrication owing to its more thermodynamically stable  $\beta$ -phase. However, the relatively lower operating temperature range and higher cost of P(VDF-TrFE) restricts its use in large-scale device fabrication<sup>10</sup>. Since, PVDF exhibits a wider operating temperature zone than P(VDF-TrFE)<sup>10</sup>, there have been a number of interesting efforts to induce the nucleation of  $\beta$ -phase in PVDF which includes, electrical poling, mechanical stretching, extreme thermal and pressure conditions annealing and spin coating<sup>11</sup>. However, multistep fabrication techniques often lead to undesired structural deformations or structural limitations and restrict the manipulation of device dimensions and thus the range of applications. Currently, PVDF continues to exhibit relatively low piezoelectric charge co-efficients after such post-processing techniques<sup>8–12</sup>.

An alternative approach to the production of ferroelectric polymers with higher piezoelectric charge co-efficients is to use additives that create a structure that combines a self-poled ferroelectric  $\beta$ -phase and a porous electret structure. This approach has proven useful to achieve superior piezo- and pyro-electric harvesting without the need of a secondary processing methods<sup>1,12</sup>. Among the several additives that have been explored, lanthanide ions such as,  $\text{Ce}^{3+}$ ,  $\text{Eu}^{3+}$ ,  $\text{Yb}^{3+}$  etc. have been proven to be useful for facile fabrication of PVDF based high performance piezoelectric nanogenerator (NG)<sup>13–15</sup>. Despite the noticeable optical properties of the lanthanide ions doped PVDF films, they have yet to be used for pyro-electric energy harvesting and sensing. Among the other lanthanide ions,  $\text{Er}^{3+}$  is known to possess superior optical activity in the infrared (IR) region<sup>16–20</sup>. Infrared rays are known to induce a photo-thermal effect, especially the near infrared rays (NIR), i.e., 760–1500 nm wavelength region<sup>21</sup>. Thus, there is a scope to develop materials for infrared driven pyroelectric energy harvesters for non-contact and remote energy transfer. In addition, thermal sensitivity can be enhanced by integrated design of  $\text{Er}^{3+}$  and PVDF under an IR irradiation for sensor applications. While thermoelectric materials utilize a spatial temperature difference, pyroelectric energy harvesters and sensors require continuous temperature fluctuations induced by an external heat source in order to develop an alternating electrical current<sup>22</sup>.

Based on these ideas, this paper aims to produce a material with (i) a high fraction of ferroelectric  $\beta$ -phase, (ii) a porous structure to achieve electret-like properties in order to enhance the mechanical energy harvesting ability and (iii) a high optical activity in the IR region for thermal energy harvesting and sensing.

This is achieved by developing a one step approach where a hygroscopic rare earth erbium salt ( $\text{Er}^{3+}$ ) is incorporated into a PVDF film (Er-PVDF film). The resulting composite film is shown to contain a thermally stable  $\beta$ -phase even higher stability than a P(VDF-TrFE) film. Owing to its superior ferroelectric and dielectric properties, a high performance ferroelectric nanogenerator (termed as, FTNG) was fabricated which generated a maximum output power of 0.125 W/m<sup>2</sup> and 13  $\mu\text{W}/\text{m}^2$  under mechanical and thermal fluctuations respectively. In addition, FTNG can also act as a healthcare monitoring sensor and thus may be beneficial for further development of self-powered electronic skin (e-skin), sensors and other low power electronic systems.

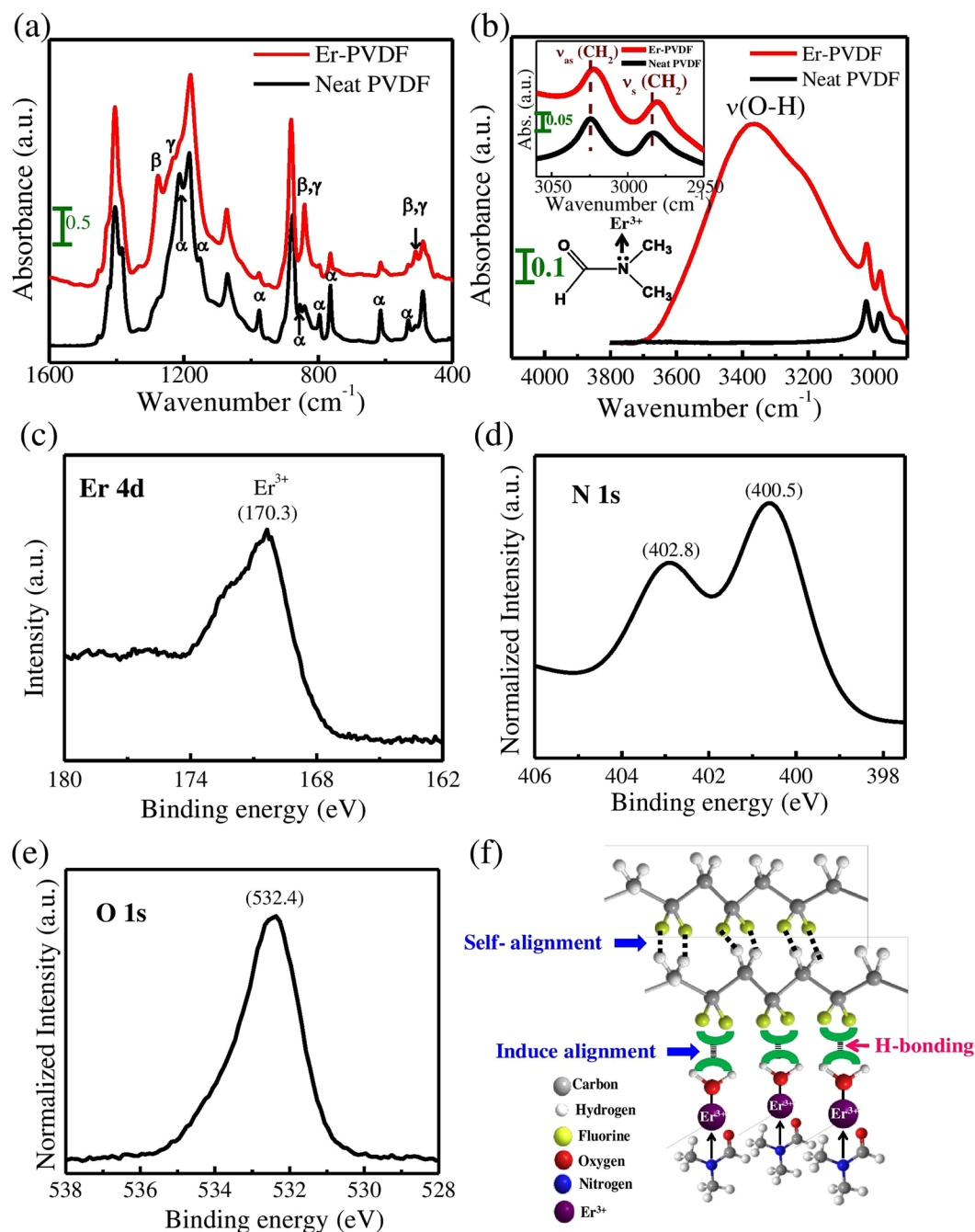
## Results and Discussion

**Structural and Electrical Properties.** Figure 1a shows that the Neat PVDF possesses mainly a non-polar  $\alpha$ -phase due to the existence of vibrational bands at 1212, 1150, 976, 855, 796, 764, 614 and 532  $\text{cm}^{-1}$ . However, the Er-PVDF film exhibits four additional peaks at 1276, 1234, 841 and 510  $\text{cm}^{-1}$  due to the nucleation of ferroelectric  $\beta$ - and  $\gamma$ -phases<sup>11,23</sup>. Among them, 1276 and 1234  $\text{cm}^{-1}$  vibrational bands represent the presence of  $\beta$ - and  $\gamma$ -phases respectively. The peaks at 841 and 510  $\text{cm}^{-1}$  are indicative of both ferroelectric phases (i.e.,  $\beta$ - and  $\gamma$ -phases)<sup>23,24</sup>. It is important to identify that the appearance of  $\beta$ -phase (1276  $\text{cm}^{-1}$ ) is strong but the nucleation of  $\gamma$ -phase (1234  $\text{cm}^{-1}$ ) is relatively weak. Quantitatively, the relative proportion of ferroelectric phases ( $F_{EA}$ ) is estimated from Lambert-Beer's law considering the band at 841  $\text{cm}^{-1}$  since it carries the dual signature of the both  $\beta$ - and  $\gamma$ -phases. The  $F_{EA}$  is found to be 75% in the Er-PVDF film, estimated using the following equation,

$$F_{EA} = \frac{I_{EA}}{\left(\frac{K_{841}}{K_{764}}\right)I_{764} + I_{EA}} \times 100\%, \quad (1)$$

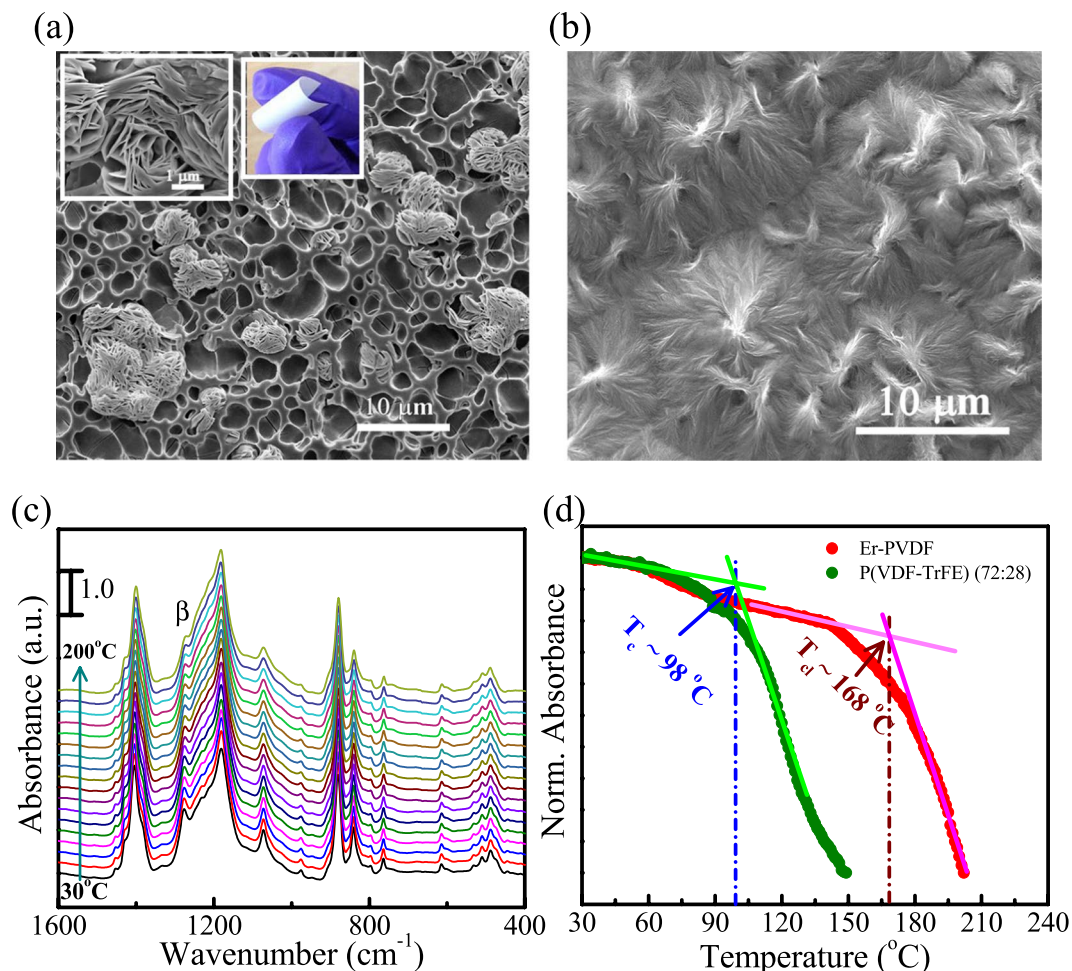
where,  $I_{764}$  and  $I_{EA}$  are the absorbance band intensity at 764 and 841  $\text{cm}^{-1}$  respectively;  $K_{764} = 6.1 \times 10^4 \text{ cm}^2 \text{ mol}^{-1}$  and  $K_{841} = 7.7 \times 10^4 \text{ cm}^2 \text{ mol}^{-1}$  are the absorption coefficients at the respective wave numbers<sup>11</sup>. An improved  $\beta$ -phase fraction ( $F(\beta) \sim 74\%$ ) with a small amount of  $\gamma$ -phase ( $F(\gamma) \sim 1\%$ ) in the Er-PVDF film was achieved (Supplementary Fig. S1) when compared to the Neat PVDF which is dominated by the non-polar  $\alpha$ -phase<sup>23</sup>.

The mechanism of ferroelectric  $\beta$ -phase nucleation is possibly due to hydrogen bonding interaction viz. O—H—F—C between the Er-salt and PVDF chains, as a stronger polarity of the hydroxyl groups is evident from the broad absorption band in the frequency region 3800–2950  $\text{cm}^{-1}$ , see Fig. 1b<sup>25</sup>. When the Er-salt is mixed with a PVDF-DMF solution, a coordination complex is formed between DMF and  $\text{Er}^{3+}$ , where the N atom is acting as a coordination site of the DMF ligand, as shown in the inset of Fig. 1b. The high-resolution core level spectrum of Er 4d by X-ray Photoelectron Spectroscopy (XPS) shows a distinct peak at 170.3 eV due to the presence of  $\text{Er}^{3+}$  in the Er-PVDF film as shown in Fig. 1c<sup>26</sup>. The splitting of the N 1s spectrum to give peaks around 402.8 and 400.5 eV (Fig. 1d) shows unequivocally, that there are two different N environments in the sample. The peak at 400.5 eV is consistent with other XPS of DMF (possibly coordinated via its oxygen, or perhaps just trapped in the PVDF)<sup>27</sup>. It is therefore reasonable to suggest that the N (1s) peak at 402.8 eV is due to N coordinated to the Er, the higher binding energy being consistent with electron donation from the N to the Er. The peak in the O 1s spectrum at 532.4 eV can be assigned to chemisorbed  $\text{H}_2\text{O}$  and DMF (Fig. 1e) which is consistent with the strong OH stretch in the FT-IR band between 3800–2950  $\text{cm}^{-1}$  (Fig. 1b)<sup>28,29</sup>. In addition, the stretching vibrational band ( $\nu_{\text{C=O}}$ ) at 1630  $\text{cm}^{-1}$  supports the formation of a  $\text{Er}^{3+}$ -DMF coordination complex (Supplementary Fig. S2)<sup>28</sup>. Under prolonged stirring of the Er-salt that is incorporated in the PVDF-DMF solution, atmospheric moisture is gradually absorbed due to its polar aprotic and hydrophilic nature. Thus, water molecules from moisture



**Figure 1.** (a) FT-IR spectra of the films in the frequency region of (a) 1600–400  $\text{cm}^{-1}$ , (b) 3800–2900  $\text{cm}^{-1}$  and 3060–2950  $\text{cm}^{-1}$  in the inset. The left lower inset in Fig. 1b shows the coordination complex structure of  $\text{Er}^{3+}$ –DMF. High-resolution XPS spectra of (c) Er 4d, (d) N 1s (e) O 1s and (f) schematic illustration of the  $\beta$ -phase nucleation process in the Er-PVDF film.

and in co-operation with co-ordination water of the Er-salt ( $\text{ErCl}_3 \cdot 6\text{H}_2\text{O}$ ) surround the  $\text{F}^-$  ions of the PVDF. Consequently, the strong hydrogen-bonding interaction of water molecules towards the  $\text{F}^-$  of PVDF (*i.e.*, O–H---F–C) drives the  $-\text{CH}_2/-\text{CF}_2$  dipoles so that they are arranged in the all trans (TTTT) configuration (*i.e.*,  $\beta$ -phase), see Fig. 1f. As a consequence, other  $-\text{CH}_2/-\text{CF}_2$  dipoles of PVDF are aligned and the induced alignment within the PVDF by H-bonding interaction further self-aligns the other PVDF macromolecular chains within the crystalline lamella of the Er-PVDF composite film; this process is shown schematically in Fig. 1f. Such an interaction is evident from the shift of  $-\text{CH}_2$  asymmetric ( $\nu_{\text{as}}$ ) and symmetric ( $\nu_{\text{s}}$ ) stretching vibrational bands towards a lower frequency, see the inset of Fig. 1b. This is presumably due to an increase in the effective mass of  $-\text{CH}_2$  dipoles during interfacial interaction<sup>23,25</sup>. As a result, damping of the vibrational frequency (*i.e.*, wavenumber) associated with  $-\text{CH}_2$  stretching occurs that, leads to a damping constant ( $2r_{\text{dc}}$ )  $\sim 4.8 \times 10^{11} \text{ sec}^{-1}$  which, indicates an improved interfacial interaction to promote an increased  $\beta$ -phase content<sup>23,25</sup>. Eventually, the overall degree

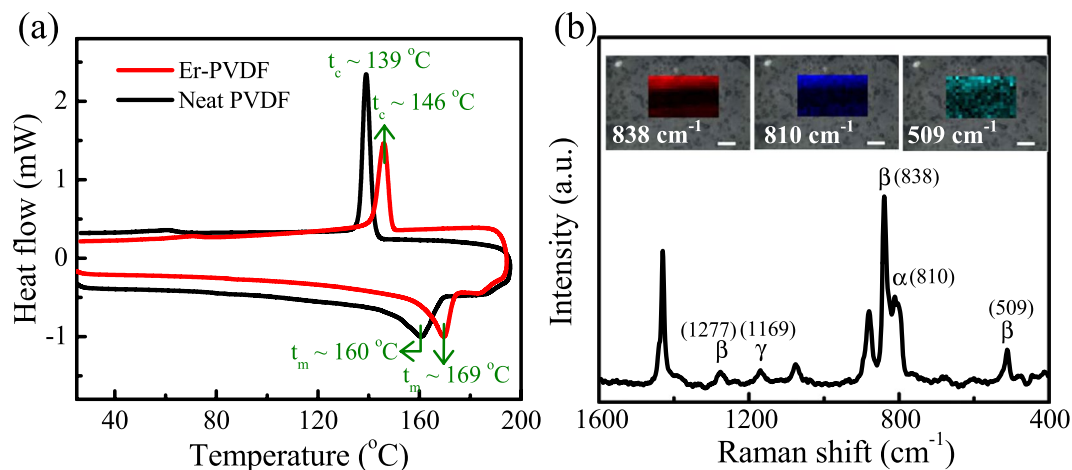


**Figure 2.** FE-SEM images of (a) Er-PVDF film with the enlarged view of the selected portion in the inset as well as digital photographs of the film and (b) Neat PVDF film. (c) *In-situ* thermal FT-IR spectra of Er-PVDF film, where the spectra between 30°C to 200°C are shown in 10°C intervals to guide the eye. (d) The variation of absorbance intensities of the  $\beta$ -phase with respect to the temperature for both Er-PVDF and P(VDF-TrFE) film.

of crystallinity ( $\chi_c$ ) in the Er-PVDF film reduces ( $\chi_c \sim 38\%$ ) in comparison to the Neat PVDF film ( $\chi_c \sim 51\%$ ) (Supplementary Fig. S3). The nucleation of  $\beta$ -phase in Er-PVDF is also prominent in the X-ray diffraction pattern, where a sharp diffraction peak at  $20.8^\circ$  can be attributed to the presence of  $\beta$ -phase, and the remaining peaks arise due to presence of  $\alpha$ - and  $\gamma$ -phases. In addition, the large crystallite size of the  $\beta$ -crystal ( $D_{\beta(110)} \sim 10$  nm) (calculated from Debye–Scherrer equation as mentioned in Supplementary Fig. S3) is also beneficial for the molecular dipoles (i.e.,  $-\text{CH}_2$  or  $-\text{CF}_2$ ) to be more cooperative to provide improved ferroelectric properties and dielectric responses<sup>23</sup>.

It is important to note that, during crystallization under heat treatment, water molecules evaporate faster than the base solvent (DMF) due to its lower density and lower boiling point. In addition, inorganic salts generally crystallize more rapidly than polymers during the crystallization process due to the high mobility of inorganic ions<sup>30</sup>. Thus, a synergistic effect of the competitive behavior between solvent and non-solvent systems by inhibiting the entanglement among the macromolecular chains of PVDF and fast crystallization of the Er-salt create an electret-like porous structure with a flower-like surface morphology within the Er-PVDF film, see Fig. 2a. The micro-pores are non-continuous and are formed in a layer-by-layer structure up to certain depth ( $\sim 5$  μm); see Supplementary Fig. S4. In contrast, the Neat PVDF film exhibits a smooth surface with several fibril-like  $\alpha$ -spherulitic growths as seen in Fig. 2b. The Er-PVDF film appears to be highly flexible due to the porous structure, see inset of Fig. 2a. In addition, the porous structure is also beneficial for superior ferroelectricity and piezoelectric output performance<sup>12,15,31,32</sup>.

In order to examine the thermal stability of ferroelectric  $\beta$ -phase in Er-PVDF (Fig. 2c and Supplementary Fig. S5), the absorption band at  $1276\text{ cm}^{-1}$  has been considered as it is indicative of only the  $\beta$ -phase<sup>23–25</sup>. For comparison a P(VDF-TrFE) film is selected since it has a well-defined Curie transition temperature ( $T_c$ ) (Supplementary Fig. S6). Figure 2d shows the relative change of absorbance of vibrational band as a function of temperature. It has been observed that  $\beta$ -phase in Er-PVDF film exhibits higher thermal stability than that of the P(VDF-TrFE) film. For instance, the ferroelectric to paraelectric phase transition occurs at  $98^\circ\text{C}$  in the

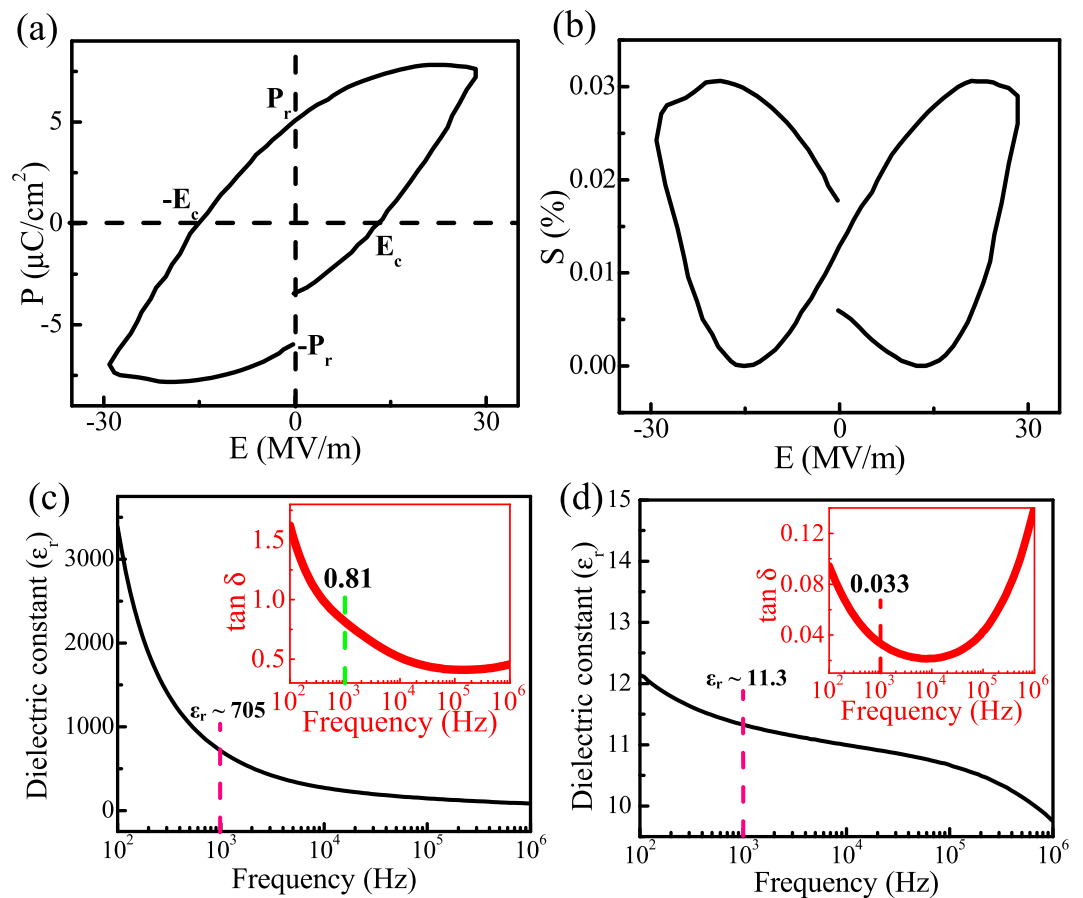


**Figure 3.** (a) DSC thermograms of the Er-PVDF and Neat PVDF films, (b) Raman spectra of Er-PVDF film with the mapping images at 838 (red mapping), 810 (blue mapping) and 509  $\text{cm}^{-1}$  (dark cyan mapping).

P(VDF-TrFE) film which is the  $T_c^{10}$ . In contrast, a similar phase transition ( $T_c$ ) is observed at a much higher temperature of 168 °C in the Er-PVDF film. Furthermore, in the vicinity of the  $T_c$ , the rate of change of absorbance as a function of temperature in Er-PVDF film is less steeper than the P(VDF-TrFE). These results indicate that the operating temperature region is expected to be higher in devices made with Er-PVDF composite since at the vicinity of  $T_c$  the chain mobility of PVDF is significantly enhanced that eventually leads to a ferroelectric to paraelectric transition<sup>10,33</sup>. Since the Er-PVDF film is mainly composed of the all-trans  $\beta$ -phase, which is thermodynamically stabilized with interfacial interaction phenomena and H-bonding, the  $T_c$ -like ( $T_c$ ) phase transition temperature is significantly improved (~62%). This provides a route to fabricate more reliable and thermally robust PVDF based electronic devices.

In order to further understand the effect of  $\text{Er}^{3+}$  on the thermal stabilization and crystallization of PVDF, differential scanning calorimetry (DSC) has been performed, see Fig. 3a. It is evident that  $\text{Er}^{3+}$  increases the melting temperature ( $t_m$ ) of the Er-PVDF film ( $t_m \sim 169^\circ\text{C}$ ), compared to the Neat PVDF film ( $t_m \sim 160^\circ\text{C}$ ). It can also be seen that the Er-PVDF film exhibits a higher crystallization temperature ( $t_c \sim 146^\circ\text{C}$ ) compared to the Neat PVDF film ( $t_c \sim 139^\circ\text{C}$ ). This is due to the fact that  $\text{Er}^{3+}$ -DMF coordination complex is acting as a nucleating agent that restricts the movement of PVDF chain segments that lead to an increase in the  $t_c$  value. In addition, the  $\chi_{c_t}$  of the films was further confirmed from the DSC data using,  $\chi_{c_t} = \frac{\Delta H_m}{(1-\varphi)\Delta H_m^0}$  where,  $\Delta H_m$  is the melting enthalpy,  $\Delta H_m^0$  is the melting enthalpy of the 100% crystalline PVDF ( $\sim 104.5 \text{ J g}^{-1}$ ) and  $\varphi$  is the weight fraction of Er-salt<sup>34</sup>. This calculation revealed  $\chi_{c_t} \sim 37\%$  for Er-PVDF and  $\chi_{c_t} \sim 50\%$  for Neat PVDF which are in good agreement with the XRD analysis. In order to map the conformational and structural changes over the large area of Er-PVDF film, we measured the Raman spectra at each point on a  $22 \times 13$  grid spanning an area of  $38 \mu\text{m} \times 23 \mu\text{m}$ , see Fig. 3b. The intensity of the Raman bands at 838 and 509  $\text{cm}^{-1}$  representing  $\beta$ -phase and at 810  $\text{cm}^{-1}$  demonstrating  $\alpha$ -phase mapped over the area of  $38 \mu\text{m} \times 23 \mu\text{m}$  which correspond to red, blue, and dark cyan images, respectively, in the inset of Fig. 3b<sup>35,36</sup>. In addition, a very weak band at 1169  $\text{cm}^{-1}$  corresponding to the  $\gamma$ -phase was also observed which agrees with the observation made from FT-IR spectra (Fig. 1a)<sup>36</sup>. In contrast, the Neat PVDF film shows only  $\alpha$ -phase in Raman spectra (Supplementary Fig. S7). Thus, the Raman spectra were found to be consistent with the FT-IR spectra. Furthermore, the representative mapping images of the Raman spectra indicate that  $\beta$ -crystal domains were mixed with the  $\alpha$ -crystal domain in the Er-PVDF film.

As piezoelectricity stems from the level of polarization of a material, the polarization behavior in the Er-PVDF film is examined from the polarization ( $P$ ) versus electric field ( $E$ ) hysteresis loop at a frequency of 10 Hz under a sweeping electric field ( $E$ ) of  $\pm 30 \text{ MVm}^{-1}$ ; as shown in Fig. 4a. The data demonstrates that the porous Er-PVDF film possesses superior remnant polarization,  $P_r \sim 5.12 \mu\text{Ccm}^{-2}$  with a coercive field ( $E_c$ ) of  $14.4 \text{ MVm}^{-1}$ ; this is in contrast to the Neat PVDF film which exhibits little ferroelectric switching (Supplementary Fig. S8). In addition, the electric field ( $E$ ) induced strain amplitude ( $S_a$ ) response arises from the converse piezoelectric effect and is demonstrated by the presence of butterfly shaped  $S_a$ - $E$  hysteresis loops; see Fig. 4b<sup>37,38</sup>. According to the macroscopic dimensional effect, the piezoelectric charge coefficient ( $d_{33}$ ) can be determined as,  $d_{33} = P_r S_{33} = -56.3 \text{ pC/N}$  where  $S_{33}$  ( $\sim 1.1 \times 10^{-9} \text{ m}^2 \text{ N}^{-1}$ ) is the elastic compliance<sup>15,31</sup>. In addition, from the  $S_a$ - $E$  loop, the longitudinal electrostrictive coefficient ( $Q$ ) can be evaluated as,  $S_a = QP^2 = 5 \text{ m}^4 \text{ C}^{-2}$  from the slope of  $S_a$  versus  $P^2$  plot (Supplementary Fig. S9). The P- $E$  and  $S_a$ - $E$  hysteresis loops indicate the preferential alignment of electric dipoles within the crystalline lamellas along the direction of the applied electric field. In addition, this may be attributed to the coupling effect of ferroelectric  $\beta$ -phase as nano-dimensional dipoles (nano-dipole) and ferroelectret properties of micro-pores behaving as micro-dipoles under the applied electric field<sup>15,31</sup>. In general, to generate electrets, charges are artificially injected into macroscopic voids of porous polymers to create oriented, “quasi-dipoles”. In this case, a large amount of charge is trapped within the porous structure at dielectric boundaries, such as adjoining crystalline/amorphous regions interfacial polarization, even without any electric poling treatment. The electrons are present through delocalization in the  $\text{Er}^{3+}$  just like space charge, which removes the need for

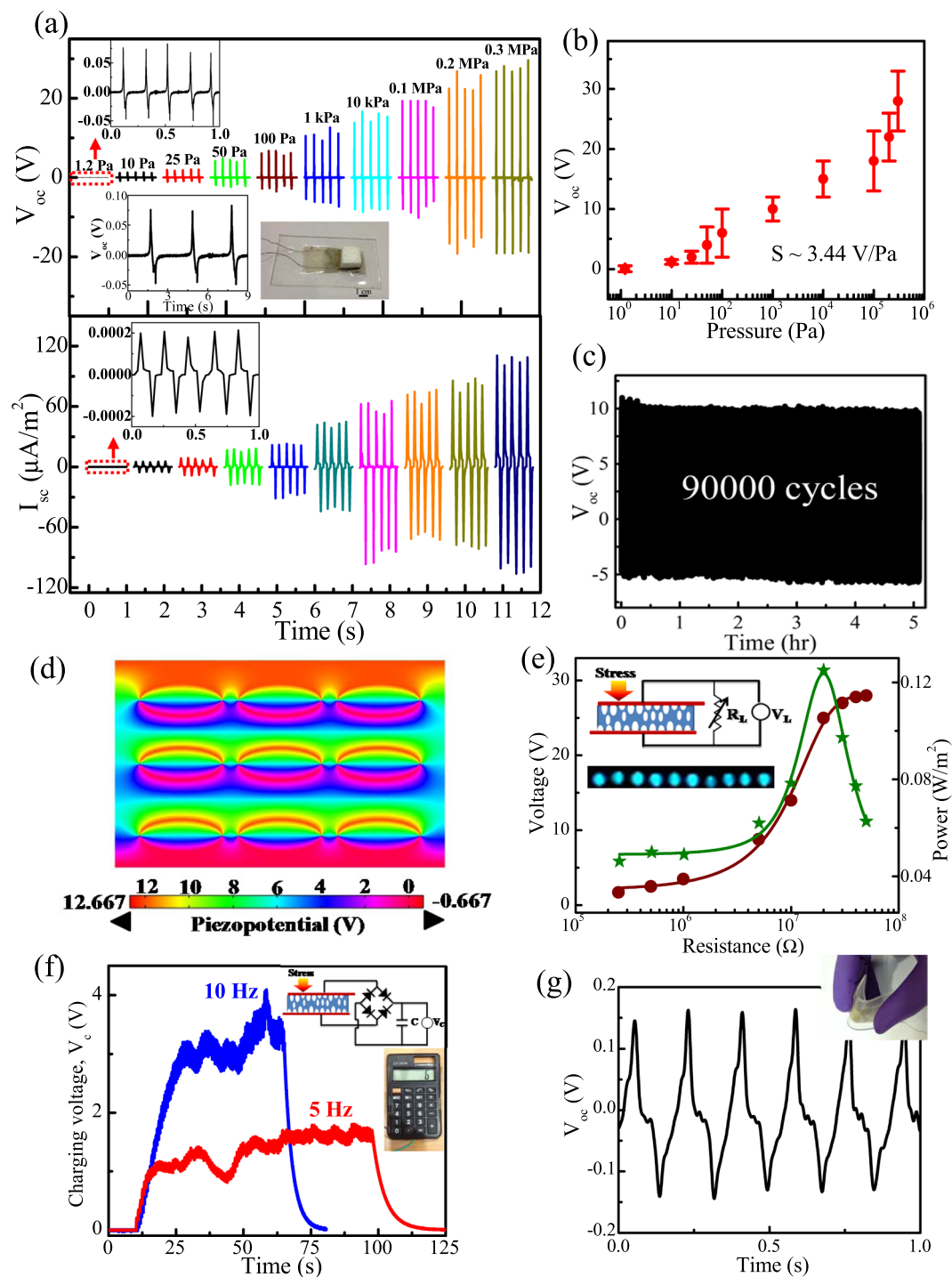


**Figure 4.** (a) Polarization ( $P$ ) versus electric field ( $E$ ), (b) butterfly shaped strain ( $S$ ) versus electric field ( $E$ ) hysteresis loops, (c) frequency dependent dielectric spectra of the Er-PVDF film and (d) the Neat PVDF film.

extra charge injection. In addition, the  $\text{Er}^{3+}$  influences charge mobilization in the Er-PVDF, and thereby facilitate hetero-polarization in the material. Therefore, during fabrication, charge separation has occurred and oriented  $-\text{CH}_2/-\text{CF}_2$  dipoles stabilize the separated trap charges due to the self-induction effect. This functionality combines the ferroelectric and ferroelectric properties which makes the Er-PVDF film a ‘ferroelectric’ material<sup>12,15,31</sup>.

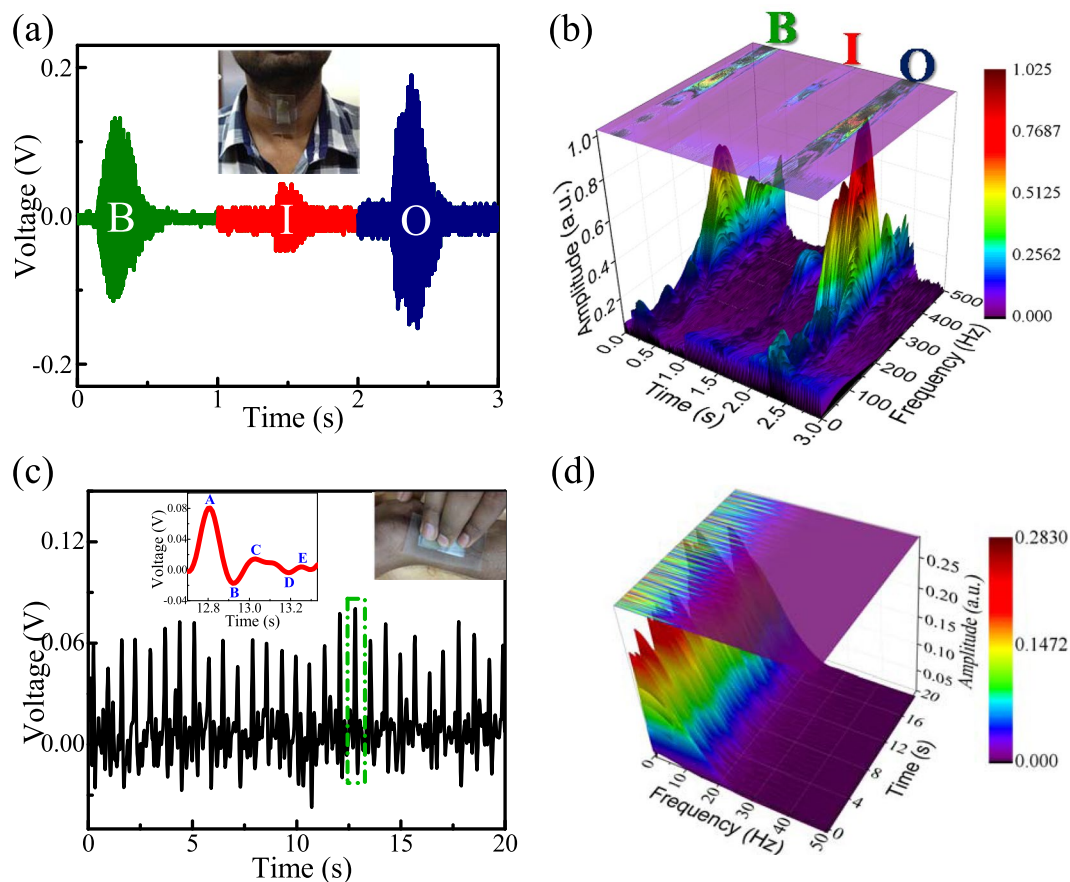
In addition, this co-operative functionality also improves the dielectric properties of the Er-PVDF film compared to the Neat PVDF film. For example, a higher dielectric constant,  $\epsilon_r \sim 705$  at 1 kHz has been observed in the Er-PVDF film (Fig. 4c) than that of the Neat PVDF film ( $\epsilon_r \sim 11.3$ ) (Fig. 4d). However, the loss tangent in Er-PVDF film ( $\tan \delta \sim 0.81$  at 1 kHz) (inset of Fig. 4c) was increased compared to the Neat PVDF film ( $\tan \delta \sim 0.033$  at 1 kHz) (inset of Fig. 4d), indicating an increase in conductivity. The dielectric spectra of the Er-PVDF film show that among the degree of polarizations, interfacial and ionic polarization mainly contributes for the increment of dielectric constant. The frequency dependent high dielectric constant ( $\epsilon_r$ ) can be an indicator of some conductivity of the material, which may also explain the higher  $\tan \delta$  in the Er-PVDF film<sup>39</sup>. The possible effects for the increment of  $\epsilon_r$  are as follows, (i) presence of micropores acting like microcapacitors<sup>31</sup>, (ii) reduction in the degree of crystallinity ( $\chi_c$ ) (resulting 33% of the  $\beta$ -crystals) according to Fröhlich’s amorphous breakdown theory<sup>40</sup>, (iii) presence of H-bonding interaction<sup>41</sup> and (iv) the influence of  $\text{Er}^{3+}$  ions in the Er-PVDF film which serve as a ionic charge carriers with low mobility<sup>42</sup>. The movement of charge along with the applied electric field leads to charge separation within the electrically neutral dielectric and developing strong electrode effects at the external dielectric-metal interface or Maxwell-Wagner polarization at internal interfaces. Thus, higher dielectric properties along with excellent piezoelectric and electrostrictive co-efficients make the Er-PVDF film an excellent ferroelectric material for mechanical and thermal energy harvesting applications.

**Piezoelectric Energy Harvesting.** Owing to the superior piezo-electret effect, the open circuit output voltage ( $V_{oc}$ ) and short-circuit output current ( $I_{sc}$ ) from FTNG was evaluated by imparting a periodic compressive stress ( $\sigma_a$ ) using a custom built pressure imparting system, as discussed earlier<sup>45</sup>. As shown in Fig. 5a, the produced  $V_{oc}$  from FTNG ranges from 70 mV to 28 V when subjected to a stress from  $\sigma_a \sim 1.2$  Pa to 0.3 MPa and a corresponding strain rate of  $6.6 \times 10^{-7}$  to  $0.165\% \text{ s}^{-1}$  (Supporting Information, Table S1). In addition, the generated  $I_{sc}$  ranges from  $0.03 \mu\text{A}/\text{m}^2$  to  $105 \mu\text{A}/\text{m}^2$  under the same applied pressure and strain rate range. An almost linear increase of  $V_{oc}$  with increasing  $\sigma_a$ , see Fig. 5b, provides a quantitative value of sensitivity ( $S_M$ ) as,  $S_M = \frac{\Delta V_{oc}}{\Delta \sigma_a} = 3.4 \text{ V}/\text{Pa}$  where,  $\Delta V_{oc}$  and  $\Delta \sigma_a$  are the differences of  $V_{oc}$  and  $\sigma_a$  respectively<sup>43</sup>. In addition, the



**Figure 5.** (a) Time-dependent open-circuit output voltage ( $V_{oc}$ ), short-circuit output current ( $I_{sc}$ ) under different pressure, (b) variation of  $V_{oc}$  as a function of pressures, (c) energy harvesting stability test over 90000 cycles under 1 kPa pressure at 5 Hz frequency, (d) simulation on piezo-potential distribution with deformed nine micro-voids nestled within PVDF under 1 kPa pressure, (e) output voltage and power as a function of external load resistances using the electronic circuit diagram and illuminated 10 LEDs in the insets, (f) transient response of  $1\ \mu\text{F}$  capacitor during voltage charging-discharging cycles under the oscillation frequencies of 5 and 10 Hz using the equivalent circuit diagram shown in the inset and operated digital calculator during discharging of the capacitor shown in the inset and (g) generated  $V_{oc}$  during repeated bending-unbending of FTNG used for sensing purpose.

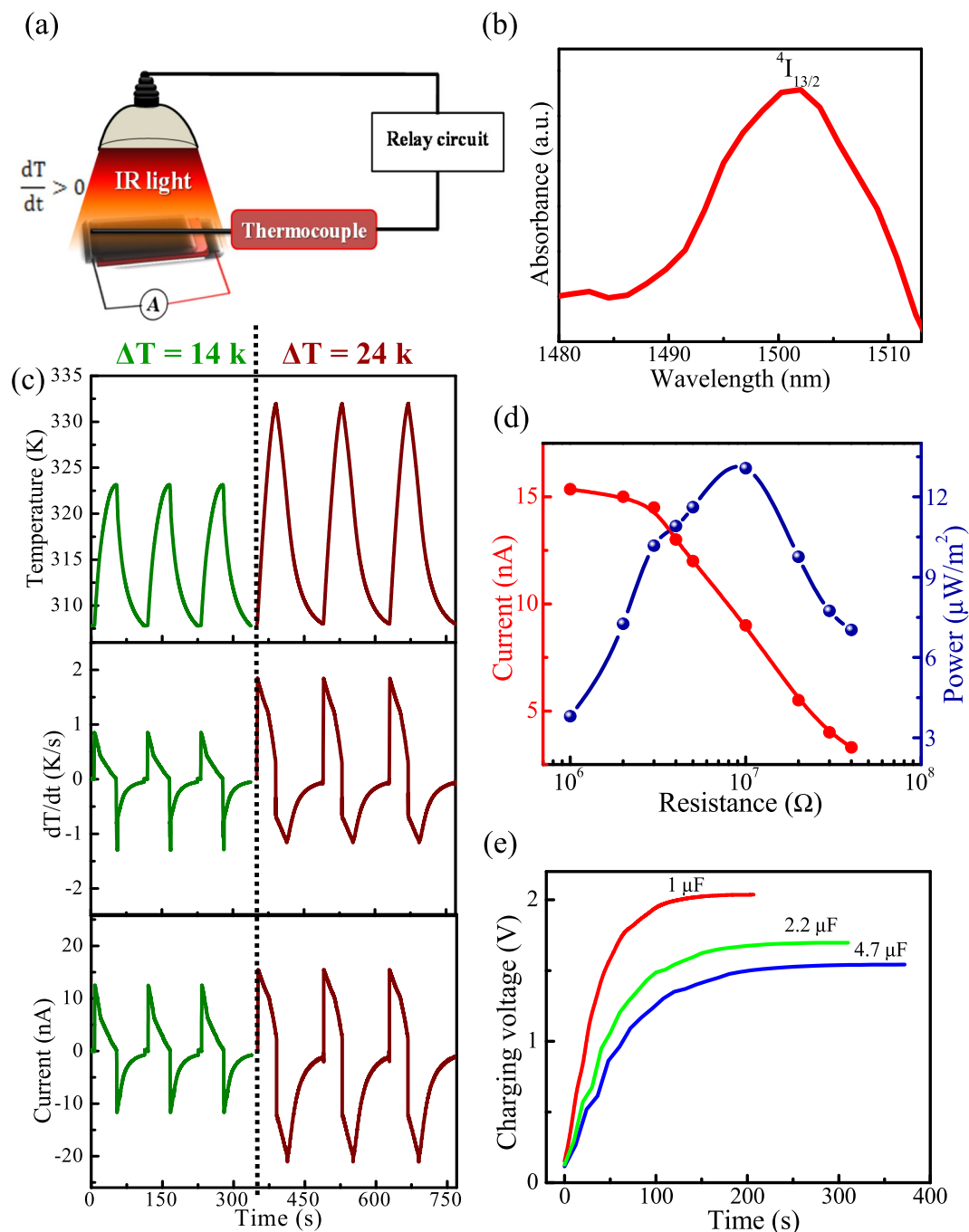
change of  $I_{sc}$  can be attributed to the variation of applied strain rate, because they are directly related to each other as,  $I_{sc} = d_{33}YA\dot{\epsilon}$  where  $Y$  is the Young's modulus,  $A$  is the effective contact area and  $\dot{\epsilon}$  is the strain rate<sup>31,38</sup>. Thus, the FTNG is proven to be a highly sensitive energy harvester and was able to detect small dynamic pressure



**Figure 6.** (a) Generated output voltage signals during speaking of the alphabets, “B”, “I” and “O” after attaching the FTNG to the throat and (b) STFT processed 3D spectrogram of the speech patterns, recognizing the frequency range of each word. (c) Wrist pulse signal detection by fastening the FTNG onto the human wrist directly (enlarge view of one signal showing details of wrist pulse) and (d) corresponding STFT processed 3D spectrogram for further analysis of the heartbeat signals.

during repeated loading–unloading of a light weight object (such as, a cube of polystyrene foam of 50 mg); as shown in the inset of Fig. 5a. The output voltage and current waveforms show synchronous alteration of positive–negative pulses with repeated compress–release of FTNG under periodic mechanical impacts. In addition, the FTNG shows reverse polarity of  $V_{oc}$  when switching the electrode connections (Supplementary Fig. S10) to undertake a ‘switching polarity test’ in order to confirm that the output responses arise due to the piezoelectric effect, and not from any contact electrification between the measurement set-up and device<sup>43</sup>. Furthermore, when two FTNGs of the same polarity and similar electromechanical responses were connected in serial and parallel configurations, the observed  $V_{oc} \sim 51$  V increased in the first case and remained almost same  $V_{oc} \sim 30$  V in second case, respectively (Supplementary Fig. S10). This further demonstrates the piezoelectric effect and also the integrability feature of the FTNG by linear superposition tests where we can modulate the output power. Additionally, as a proof of confirmation a non-piezoelectric PDMS control device (without an Er-PVDF film) was also fabricated where no reliable output voltage is obtained (Supplementary Fig. S11). The superior energy harvesting performance of the FTNG over the previously reported piezoelectric polymer based NGs<sup>5,6</sup> is attributed to the superior piezoelectric figure of merit ( $FoM_p \approx d_{33} \cdot g_{33} \approx 5.08 \times 10^{-13} Pa^{-1}$  where,  $g_{33} = \frac{d_{33}}{\epsilon_r \epsilon_0} = 9 \times 10^{-3} VmN^{-1}$ ) and intrinsic piezoelectricity of the ferroelectret characteristics due to the spongy nature of micro-voids in comparison to the stiffer surrounding PVDF matrix<sup>15,31,44</sup>. For ferroelectric PVDF, the local polarization is compensated by space charges around the crystallites and the interconnected amorphous regions behave like a spring. Thus, under an external mechanical impact ( $\sigma_a$ ), the deformation of the micro-voids in comparison to the PVDF chain is considerably larger due to the relatively weak vander Waal bonds as well as electrostatic interactions between the macromolecular chains in comparison to the strong covalent bonds within the chain which induces piezoelectric potential within FTNG<sup>31</sup>. As a result, free electrons move to the external load in order to screen the piezo-potential which leads to a positive voltage peak. On release of the applied stress,  $\sigma_a$ , negative voltage distributions are generated due to a decrease of the piezo-potential and release of the accumulated electrons. Importantly, the FTNG demonstrates a highly stable generation of  $V_{oc}$  over prolonged period of time (90000 cycles) under 1 kPa pressure at 5 Hz, see Fig. 5c, due to robust mechanical property of the nanocomposite structures under significant deformation and the flexibility of the entire structure. The contribution of the





**Figure 7.** Pyroelectric output responses of FTNG. **(a)** Schematic of pyroelectric experimental setup. **(b)** Absorbance spectra of Er-PVDF film in the 1480–1513 nm wavelength range. **(c)** The time-dependent cyclic changes in the different range of applied temperatures and temperature gradient ( $dT/dt$ ) which generate short-circuit currents. **(d)** Output short-circuit current and power density as a function of external resistances varying from 1 M $\Omega$  to 40 M $\Omega$ . **(e)** Transient responses of external capacitors (1  $\mu$ F, 2.2  $\mu$ F and 4.7  $\mu$ F) charging under heating-cooling cycles of the temperature difference  $\Delta T \sim 24$  K.

highly deformed micro-voids to the piezo-voltage generation of the FTNG was quantitatively explained by the finite element method (FEM) based simulation using COMSOL multiphysics software with nine micro-voids placed into a PVDF structure (see Fig. 5d). The piezo-potential distribution inside the deformed FTNG is represented by the color contour with a z-axis mechanical stress ( $\sigma_a \sim 1$  kPa) and the magnitude of the simulated piezo-potential ( $\sim 12$  V) is almost consistent with the experimental finding ( $\sim 10$  V). The effective piezoelectric power output from FTNG was calculated by measuring the output voltages across various load resistors ( $R_L$ ) ranging from 0.25 M $\Omega$  to 50 M $\Omega$ , as seen in Fig. 5e, using a simple electronic circuit (inset of Fig. 5e). The measured instantaneous voltage drop ( $V_L$ ) across the resistors gradually increases with an increase of  $R_L$  and saturates at very high resistances ( $\sim 50$  M $\Omega$ ) corresponding to the open circuit voltage. The effective output power density (P)

of the FTNG is calculated by  $P = \frac{1}{A} \cdot \frac{V_L^2}{R_L}$  where, A is the effective contact area and  $V_L$  is the voltage drop across the load resistance  $R_L$ . Thus, an estimated instantaneous output power density is 0.125 W/m<sup>2</sup> at an  $R_L$  of 20 M $\Omega$  which is shown to be sufficient to turn on several (~10) blue LEDs when subject to a mechanical touch without any storage system; see inset of Fig. 5e. In order to provide more a useful application of the FTNG, the device was connected to an external capacitor through a full-wave bridge rectifier, as shown in Fig. 5f. It is interesting to note that the FTNG was able to charge up a capacitor of 1  $\mu$ F capacitance up to 4 V within 70 s when impacted by 10 Hz frequency mechanical load and a higher frequency yielded faster charging of the capacitor. For example, a lower voltage (~1.8 V) was reached across 1  $\mu$ F capacitor under 5 Hz frequency impact. During discharging, the stored maximum energy ( $E = \frac{1}{2}CV_c^2 = 8\mu$ J) across the capacitor was further used to drive a digital calculator, see the inset of Fig. 5f. Owing to the high sensitivity of the device, bending and releasing of the FTNG in a cyclical manner using a human finger also generates  $V_{oc} \sim 150$  mV (Fig. 5g). In this case, a tensile strain is developed along the thickness direction ( $\epsilon_y$ , parallel to the dipole orientation) during bending of the device into an arc shape which is given by,  $\epsilon_y = \frac{L}{2r} = 0.433\%$ , where,  $r = 15$  mm is the bending radius and L is the thickness (~130  $\mu$ m)<sup>15,31</sup>. Alternatively, the strain developed along the length direction (perpendicular to the preferential dipole orientation) is  $\epsilon_x \sim 0.190\%$ , obtained from the relation of Poisson's ratio,  $\nu = \left| \frac{\epsilon_x}{\epsilon_y} \right| = 0.44$  of PVDF<sup>15</sup>. This result includes the static tactile sensing ability of FTNG which can be helpful for physiological signal monitoring.

**Wearable Healthcare Monitoring System.** As a wearable sensor, the FTNG was attached to a human throat by adhesive tape as shown in Fig. 6a. The device could recognize the vibration of vocal cords and generate a corresponding time dependent output voltage waveform in response to the pronunciation of various letters of the alphabets such as “B”, “P”, and “O” from a speaker. An alternative way to view the data is represented by short-time Fourier transform (STFT) processed 3D spectrograms, in which the spectral content appears in a color contour plot with time, frequency and amplitude along the x, y and z axes, respectively (Fig. 6b). The acoustic profile of the alphabets shows that maximum amplitude of “B” occurs around 350 Hz, “P” appears around 375 Hz and “O” lies around 400 Hz. Thus, FTNG could be non-invasively used to monitor damaged vocal cord and in speech rehabilitation training<sup>43</sup>.

In addition, when the FTNG was firmly attached to a human wrist, as shown in Fig. 6c, it could successively sense the subtle pressure changes of the radial artery blood pressure. At the rest condition, the FTNG can read out a real time heart beat (~84 beats per minute) where each peak denotes one pulse. Details of the heart beat can be found by analyzing each voltage output waveforms which is composed of mainly five parts, such as, initially positive (A-wave), early negative (B-wave), reincreasing (C-wave), late redecaying (D-wave), and diastolic positive (E-wave)<sup>45</sup>. The important clinical insights from heart beat signals could be assessed from the corresponding STFT processed spectrogram, see Fig. 6d. These results show that each heart beat pulse lies within the frequency range of 0–20 Hz and this frequency domain features could be further used in order to determine the age related heart condition<sup>43,45</sup>. Thus, the potential of FTNG as a self-powered healthcare monitoring electronic skin (e-skin) could pave the way for next generation self-powered wearable biomedical electronic systems<sup>46</sup>.

**Pyroelectric Energy Harvesting.** The ferroelectric property of the Er-PVDF film also enables the FTNG to harvest thermal energy by using the pyroelectric effect. Temperature oscillations were applied to the FTNG by illumination of IR light to assess the pyroelectric short circuit current ( $I_{psc}$ ). The design for the pyroelectric energy harvesting system is shown schematically in Fig. 7a. Interestingly, the Er<sup>3+</sup> containing Er-PVDF film is a good absorber of IR light, as shown by the absorption spectra in Fig. 7b. Thus, the material is attractive for direct thermal to electrical energy conversion which enables small-scale energy harvesting devices to operate at low temperatures. The absorption peak around 1502 nm corresponds to the transition from the ground state <sup>4</sup>I<sub>15/2</sub> to excited state <sup>4</sup>I<sub>13/2</sub><sup>16,18–20</sup>. Thus, the FTNG was placed below an IR light bulb at a 2 cm distance. The developed temperature gradient was measured using a thermocouple at the surface of the FTNG by contact conduction. When the light was switched on to heat the FTNG, the temperature increased from 307 K to a higher value and an increase of the generated  $I_{psc}$  was observed. When the light was switched off, the device cooled down and a decrease of  $I_{psc}$  was observed. Figure 6c shows that under the exposure of temperature changes from  $\Delta T \sim 14$  K to 24 K, an increase of  $I_{psc} \sim 12.5$  nA to 15.5 nA have been observed. This enhancement was achieved by a thermally induced piezoelectric coupling effect, as the output performance is proportional to  $\Delta T$  and  $dT/dt$ <sup>47</sup>. Under a mechanical stress ( $\sigma$ ) and strain (S), pyroelectrics also experience a change in spontaneous polarization ( $dP_{s_{ij}}$ ) as they are a subgroup of piezoelectric materials. The application of heat results in an applied stress and eventually, thermal strain in the Er-PVDF film. Thus, the  $dP_{s_{ij}}$  is a combination of its primary pyroelectric coefficient  $p$  and secondary contribution ( $d_{ij}c_{ijk}\alpha_i$ ) due to thermal strain and piezoelectric contribution. Therefore, in case of metal-insulator-metal (MIM) structure, the change in polarization,  $dP_{s_{ij}}$  with respect to the change in temperature  $dT$  can be written as,

$$\frac{dP_{s_{ij}}}{dT} = p - d_{ij}c_{ijk} \left( \alpha_i - \frac{dS_{ij}}{dT} \right)$$

where,  $p$  is the pyroelectric co-efficient (Cm<sup>-2</sup>K<sup>-1</sup>),  $d_{ij}$  (C/N) is the piezoelectric coefficient,  $c_{ijk}$  (N/m) is mechanical stiffness,  $\alpha_i$  is material thermal expansion, and  $dS_{ij}/dT$  is thermally induced strain<sup>48</sup>.

In addition, the IR ray absorbing capability of the Er-PVDF film enhances heat transfer and achieves both faster and larger temperature fluctuations, which improves pyroelectric energy transformations. The origin of the pyroelectric effect in the FTNG stems from the ferroelectric properties of Er-PVDF film because porosity significantly decrease the specific heat capacity and increases the pyroelectric properties for energy harvesting<sup>44</sup>. The

pyroelectric figure of merit can be expressed as,  $FoM_{py} = \frac{p^2}{\varepsilon_0 \varepsilon_r C_E}$  where,  $\varepsilon = \varepsilon_0 \varepsilon_r$  is the permittivity and  $C_E$  is the volume specific heat and derived by  $C_E = \rho C_p$ , where  $C_p$  is the measured specific heat capacity and  $\rho \sim 1.74 \text{ g.cm}^{-3}$  (according to data sheet)<sup>44</sup>. The Er-PVDF film possesses lower specific heat capacity than the Neat PVDF (Supplementary Fig. S12) which implies its higher thermal energy harvesting capability. Thus, Er-PVDF film exhibits a  $FoM_{py} = 0.05 \text{ pm}^3 \text{J}^{-1}$ . In fact, the level of polarization (P) changes as a result of a change in temperature dT (K). When the level of polarization decreases on heating, surface bound charge become free and this creates an electric field across the polar axis<sup>49</sup>. This potential difference can be discharged across an external load when the surface electrodes of the FTNG are interconnected via external load. Under short circuit conditions, the pyroelectric current is given by  $I_{psc} = A \frac{dp}{dT} \frac{dT}{dt} = Ap \frac{dT}{dt}$  where, A is surface area ( $\text{m}^2$ ) and  $\frac{dT}{dt}$  is the rate of temperature change ( $\text{Ks}^{-1}$ )<sup>1,44,47-50</sup>. Thus, the pyroelectric co-efficient of the FTNG is  $33 \mu\text{Cm}^{-2}\text{K}^{-1}$ . The pyroelectric output currents ( $I_{pl}$ ) were further measured under  $\Delta T \sim 24 \text{ K}$  across variable external resistances ( $R_L$ ) ranging from 1 M $\Omega$  to 40 M $\Omega$  (Fig. 7d). The output power (P) was evaluated using the relation,  $P = I_{pl}^2 \times R_L$ . The maximum pyroelectric output power was found to be  $13 \mu\text{Wm}^{-2}$  across the resistance of 10 M $\Omega$ . In order to demonstrate the practical application of the FTNG as a pyroelectric energy harvester, the device was used to charge up commercial capacitors of a range of capacitances such as, 1  $\mu\text{F}$ , 2.2  $\mu\text{F}$  and 4.7  $\mu\text{F}$  (Fig. 7e). Under repeated heating-cooling cycles, the FTNG stored 1.6  $\mu\text{J}$ , 1.1  $\mu\text{J}$  and 2.3  $\mu\text{J}$  of energy ( $E = \frac{1}{2} CV_c^2$  where C is the capacitance and  $V_c$  is the charging voltage) across 1  $\mu\text{F}$ , 2.2  $\mu\text{F}$  and 4.7  $\mu\text{F}$  capacitors respectively. The stored energy could be further used to drive the low power consumer electronics. This indicates that FTNG could be applicable to harvest waste heat energy as well as mechanical vibrational energy to operate our low power consumer electronic devices in addition to smart biomedical devices for self-powered wearable electronics and e-skin applications.

## Conclusion

We have demonstrated a novel infrared sensitive  $\text{Er}^{3+}$  modified poly(vinylidene fluoride) (PVDF) (Er-PVDF) film whose piezo- and pyro-electric properties are designed for superior harvesting of both mechanical and thermal energies. The  $\text{Er}^{3+}$  is shown to provide enhanced nucleation of ferroelectric  $\beta$ -phase and aids in the formation of an electret-like porous structure to provide the improved piezoelectric properties. In addition, due to its excellent sensitivity to infrared light, the  $\text{Er}^{3+}$  enhances heat transfer in the Er-PVDF film and provides rapid and large temperature fluctuations during heating, thereby improving pyroelectric energy transformation. As a new form of hybrid harvesting material and mechanical and thermal sensor, it is shown that the combination of the rare-earth  $\text{Er}^{3+}$  ion with the ferroelectricity of PVDF can find a broad range of applications in self-powered personal micro-electronics, temperature and motion sensing, and e-healthcare monitoring.

## Methods

**Film preparation.** In our experiment, we added 2.0 wt % (w/v) of erbium (III) chloride hexahydrate ( $\text{ErCl}_3 \cdot 6\text{H}_2\text{O}$ , Sigma-Aldrich, USA) salt (i.e., Er-salt) to a 6 wt % (w/v) of PVDF (Sigma-Aldrich, USA)-N,N-dimethyl formamide (DMF, Merck, India) solution and stirred at room temperature. The film was deposited by a solution casting process at 120 °C for 8 h under vacuum conditions. As a reference, pure PVDF (termed as, Neat PVDF) and P(VDF-TrFF) (72:28 mol%) films were also prepared under similar conditions. The films were named as Er-PVDF (where Er-salt is present) and Neat PVDF (where no additive is present).

**Nanogenerator fabrication.** In order to fabricate the FTNG, top and bottom electrodes (effective area, A: 250  $\text{mm}^2$ ) were made with silver paste. Electrical output leads were attached to the each side of the electrodes by means of silver paste. Finally, the electrode-film sandwich structure was encapsulated with a poly(dimethylsiloxane) (PDMS) (Sylgard 184 silicone elastomer) layer ( $\sim 10 \mu\text{m}$  thickness) to increase the robustness of the device. The PDMS was prepared by mixing the silicone elastomer with curing agents in the ratio of 10:1 and heated at 60 °C for 30 min after degassing.

**Material characterization.** The crystalline modifications and *in-situ* thermal stability (thermal ramp 1 °C/min) of the films were analyzed by Fourier Transform Infrared Spectroscopy (FT-IR, Tensor II, Bruker). Morphological features were investigated by Field Emission Scanning Electron Microscopy (FE-SEM, FEI, INSPECT F 50). The degree of crystallinity in the Er-PVDF and Neat PVDF films were estimated by X-ray diffraction analysis (XRD, D8 Advance, Bruker) with  $\text{CuK}\alpha$ , X-ray radiation ( $\lambda = 0.154178 \text{ nm}$ ). Differential scanning calorimetry (DSC) was performed (microSC, Setaram) from 20 to 200 °C at a heating rate of 1 °C.min<sup>-1</sup>. The specific heat capacity ( $C_p$ ) of the films was measured from 20 to 60 °C by a MicroSC multicell calorimeter from Setaram, with the Calisto program to collect and process the data. Raman spectra were recorded using a Raman microscope (Renishaw inVia) using 785 nm excitation from a HeNe laser in the range 1600–400  $\text{cm}^{-1}$ . The sample was excited by 7 mW incident laser power, and scattered light was collected through a 50  $\times$  objective lens (Leica, numerical aperture (NA) = 0.75) with 2  $\mu\text{m}$  spot size. We measured the Raman spectra at each point on 22  $\times$  13 grids over an area of 38  $\mu\text{m} \times 23 \mu\text{m}$  and mapped the intensity of Raman bands at 810, 838 and 509  $\text{cm}^{-1}$  over the entire region. Each data point resulted from an exposure time of 25 s. A Kratos Axis Ultra DLD system was used to collect XPS spectra using monochromatic  $\text{Al K}\alpha$  X-ray source operating at 150 W (10 mA  $\times$  15 kV). Data was collected with pass energies of 80 eV for survey spectra, and 40 eV for the high resolution scans with step sizes of 1 eV and 0.1 eV respectively. The system was operated in the Hybrid mode, using a combination of magnetic immersion and electrostatic lenses and acquired over an area approximately 300  $\times$  700  $\mu\text{m}^2$ . A magnetically confined charge compensation system was used to minimize charging of the sample surface, and all spectra were taken with a 90° take of angle. A base pressure of  $\sim 1 \times 10^{-9}$  Torr was maintained during collection of the spectra. Data was analysed using CasaXPS (v2.3.19rev1.11) after subtraction of a Shirley background and

using modified Wagner sensitivity factors as supplied by the manufacturer. The optical property of the Er-PVDF film has been studied by NIR spectrometer (DWARF STAR, StellarNet Inc.) within 900–1700 nm wavelength range. The polarization (P) versus electric field (E) hysteresis loops were measured from the ferroelectric testing system (P-E, P-LC100V, Radiant Technology Precision) connected to a high voltage interface, employing a bipolar triangular electric field (E). Frequency dependent dielectric properties were measured from a 20 Hz to 10 MHz frequency range using a precision impedance analyzer (Wayne Kerr, 6500B). The output voltages and currents of the FTNG were recorded using digital storage oscilloscope (Tektronix, TDS2024C) and picoammeter (Keithley 6485) respectively. The vertical forces were recorded by a 3-axial force pressure sensor (FlexiForce A201).

**Data Availability.** The datasets generated during and/or analysed during the current study are available from the corresponding author on reasonable request.

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## Author Contributions

D.M. conceived and designed the experiments. S.K.G. performed the experiments, theoretical modeling and wrote the paper. D.J.M. performed the XPS measurements and P.R.D. analyzed the XPS data. S.K.G., M.X., C.R.B., P.R.D., D.J.M. and D.M. analyzed the overall content and discussed the results. All authors read and approved the final manuscript.

## Additional Information

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**Competing Interests:** The authors declare that they have no competing interests.

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