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1 Critical Review of Nanopillar-Based Mechano-Bactericidal Systems 2

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15 Abstract

The rise of multidrug resistant bacteria is the biggest threat to human health globally as described by the World Health Organization (WHO). Mechano-bactericidal surfaces provides a sustainable approach to address this concern by eradicating pathogens, especially bacteria, "right-at-the-point" of first contacting the surface. However, the lack of a "design to manufacture" approach due to our limited understanding of the mechano-bactericidal mechanism has impeded engineering optimization to develop scalable exploitation routes in various healthcare applications. It can be argued that the reason, most particularly, is the

limitations and uncertainties associated with the current instrumentation and simulation 1 capabilities which has led to several streams of test protocols. This review highlights the current 2 understanding on the mechano-bactericidal mechanisms in light of the contributing factors and 3 various techniques which are used to postulate these mechanisms. The review offers a critique 4 on the variations observed on how nanostructured surfaces found in literature have been 5 evaluated such that the test protocols and the outcomes are incomparable. The review also 6 shows a strong need of developing more accurate models of a bacterium as the currently 7 reported experimental data is insufficient to develop bacteria's material models (constitutive 8 9 equations). The review also alludes to the scarcity of direct experimental evidence of the mechano-bactericidal mechanism suggesting a strong need for further in-situ monitoring as a 10 future research direction. 11

Keywords: Mechano-bactericidal; nanostructured surfaces; biomimicry; nature-inspiration;
engineering biology

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Antibiotics are crucial in treating bacterial infections. However, the misuse of antibiotics has 15 empowered bacteria to develop resistance by, most prevalently but not exclusively, secreting a 16 shielding biofilm to prevent therapeutic access. Presently, antibiotic resistance (ABR), a subset 17 of antimicrobial resistance¹ is an eminent threat to human health and human quality of life 18 globally. As the development of novel antibiotics and antimicrobials has been diminishing, 19 new approaches to combat this rapidly growing issue have become a necessity². Moreover, 20 treatment without prevention is insufficient, especially with regards to biomaterial-associated 21 22 infections, as this can dictate the fate of implant surgeries by tipping the scale in favor of bacteria in the "race for the surface" against eukaryotic cells³. Clinical statistics suggests that 23 the percentage of post-operative infections of orthopedic implants ranges between 0.7 % and 24

4.2 %.^{4–6} This percentage can be as high as 30% for complex trauma cases^{7,8} as the surfaces of 1 these implants are at high risk of bacterial contamination. The ABR of pathogenic bacteria such 2 as Staphylococci and Streptococci, among others, renders existing antibiotic treatments for 3 4 post-operative infections futile, with resistance starting to emerge for last resort antibiotics such as vancomycin⁹ (widely used in orthopedics), polymyxin B and colistin.¹⁰ Protective biofilms 5 can form within hours of implantation and therefore agile preventative methods are required, 6 which are being currently explored. Such methods have been directed towards preventing 7 bacterial contamination and biofilm formation by modifying the surfaces using various 8 9 techniques which are termed as "anti-bacterial". Contrary to the common practice in nonbiology (especially engineering) related fields, the term anti-bacterial is not exchangeable with 10 anti-microbial, but a subset of it. Herein, a classification is offered (see fig 1) to highlight anti-11 microbial surfaces by their specific functions. Based on this classification, anti-microbial 12 surfaces can be categorized as follows: 13

- Anti-biofouling or anti-adhesion surfaces that repel microbes (i.e., bacteria, viruses,
- 15

fungi) and prevent them from adhering to the surface, and

• Biocidal surfaces that can kill or suppress the growth of microbes.

Biocidal surfaces can be further divided as (i) bacteriostatic, which can prevent the 17 proliferation of bacteria, (ii) bactericidal which can kill the bacteria either through release or 18 contact kill mechanisms, and (iii) antiviral or virucidal surfaces that are lethal to viruses. 19 Focusing on bactericidal surfaces, release kill and contact kill surfaces have slight differences 20 between them. Release kill surfaces are those that cause ozone exposure triggered by metallic 21 ions^{11,12} (ionic silver, ionic copper, graphene nanosheets, carbon nanotubes etc.) or that can 22 23 release antimicrobials from the surface into the surrounding fluid to kill the bacteria. Contact kill surfaces are those which can kill the bacteria merely by their physical presence either by 24 25 virtue of the surface chemistry (coating, immobilized antimicrobial agents etc.) or their

- 1 surface topography (physical geometry, nanostructure, nanotexture, etc.), often referred to as
- 2 mechano-bactericidal.







Mechano-bactericidal surfaces have gained significant interest recently (Fig. 2) as potential
anti-bacterial biomaterial surfaces due to their premise of transferability to different
biomaterials. The bactericidal mechanism(s) behind their action remains unclear due to
complexities that accompany bacteria-surface experimental investigations and a lack of
uniformity in the reported data.



- 2 Figure 2: Timeline showing progressive learning about the bactericidal surfaces based on the
- 3 topography of cicada and dragonfly wings.
- 4 Conflicting correlations have, thus, been made between bactericidal efficiency and: (i)
- 5 surface water contact angle, (ii) surface roughness, and (iii) nanostructure interspacing,

- 1 among others. It is however categorically established that the mechanism is independent of
- 2 surface chemistry ⁴⁸ and relies on the mere topography of the surface, hence the prefix
- 3 "mechano". Moreover, it has been suggested that the biocidal action can be expanded to
- 4 affect other microbes i.e., viruses^{38,49} and yeast⁵⁰ cells.
- 5 In this mechano-bactericidal killing approach, the understanding of the bacterium's anatomy
- 6 (shown in Fig. 3) becomes increasingly important.



Figure 3: The anatomy of bacteria. Section A-A depicts the basic structure of the peptidoglycan, the cytoplasmic membrane, and the outer membrane. The grey circles represent the lipid bilayer, the turqoise (light blue circles) represent the alternating units of Nacetylglucosamine and Nacetylmuramic acid, with the N-acetylmuramic acid residues crosslinked to peptides. The yellow circles represent the lipopolysaccharides. CPS and EPS stand for capsular polysaccharids and extracecllular polymeric matrix respectively.

1 The main structural elements constituting bacteria are the cytoplasm, the peptidoglycan and the membranes (cytoplasmic and outer). The cytoplasm is a matrix that is composed mostly 2 of water (80%) and contains enzymes, nutrients, wastes, gases, ions and cellular components 3 4 such as the ribosomes, plasmid (if any), the bacterial DNA, etc. It has been reported to behave as a glass-forming fluid in some studies⁵¹, but generally its material properties remain 5 6 uncharacterized. The peptidoglycan is a very robust protective layer that is made up of repeating disaccharides of N-acetylmuramic acid and N-acetylglucosamine that are linked by 7 $\beta(1-4)$ glycosidic linkages⁵². A recent report⁵³ claims that the latter exhibits viscoelastic 8 9 behavior when subjected to indentation load under an atomic force microscope (AFM). The cytoplasmic membrane, or inner membrane of a bacterium, is a phospholipid bilayer 10 whereas the outer membrane (in case of Gram-negative bacteria) is principally made up of 11 12 lipopolysaccharide. Measuring the mechanical properties of the individual components of the bacterial cell wall continues to be a great challenge due to the cellular complexity. However, 13 cellular membranes consisting of lipid bilayers and lipopolysaccharides have been reported to 14 behave elastically under large deformations⁵⁴, making them hyperelastic materials. 15 In the next sections, the review critiques the sources of bias introduced by the experimental 16 techniques used to study nanostructured mechano-bactericidal surfaces and their mechanisms. 17

Accordingly, the review presents the settled understanding on the various bactericidal

mechanisms of such surfaces and the factors influencing the efficiency of the bactericidal

activity. It also offers a discussion and an open invitation for leading groups in the field to

consider experimental approaches and standardized techniques to eliminate bias and

circumvent uncertainty to improve the test protocols for evaluating the mechano-bactericidal

23 surfaces.

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Mechano-bactericidal mechanisms

In the quest to elucidate the mechanism(s) underlying mechano-bactericidal activity, two research approaches have been adopted which are based either on experimental data or continuum simulations. In the next sections, the techniques used to evaluate bactericidal surfaces have been discussed, followed by the mechanisms revealed by these experimental approaches, the mechanisms revealed by simulation approaches and the factors playing into the effect of mechano-bactericidal structures. The limitation of experimentation and simulations will both be discussed in their prospective sections.

9

Techniques used to evaluate bactericidal surfaces and bacteria-surface

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interactions

As bacteria-surface interactions remain largely unknown in the light of evolving experimental
 procedures, a range of techniques have been used to study bactericidal surfaces mostly at
 discrete time points.

To study this interaction, mechano-bactericidal surfaces are first incubated with a volume of 14 bacterial suspension (*i.e.*, a nutrient-rich broth containing bacteria). This can be done using 15 one of the three main set-ups presented in Fig. 4 (a); the overlay or drop-test method where a 16 droplet with large volume is deposited onto the nanostructured surface.⁵⁵ the sprav method 17 where the bacterial suspension is sprayed over the surface,⁵⁶ and the immersion method 18 where the nanostructured sample is fully immersed in the bacterial suspension.⁵⁷ The overlay 19 and spray methods introduce surface tension at the perimeter of the droplets which might 20 induce an external force that is able to drive the bacteria towards the nanostructures, hence 21 22 stimulating a high bactericidal reaction (Fig. 5 (d)). Since the overlay method consists of one large drop instead of smaller dispersed droplets as in the case of spraying, it is more suitable 23 to use when evaluating mechano-bactericidal surfaces. The high bactericidal effect-inducing 24 surface tension at the droplet perimeter can be eliminated from consideration when analyzing 25

the results. These two methods cannot be used to test the functionality of the surfaces for long 1 periods of time as they are prone to evaporation. The immersion method, on the other hand, 2 provides the possibility of long duration functional analysis, continuous durability analysis (> 3 24 h), studying potential self-cleaning cycles of mechano-bactericidal surfaces,³¹ and 4 eliminating surface tension-inducing bubbles by using dynamic incubation.⁵⁸ 5 6 To assess and compare the bactericidal performance of various nanopatterns, it is critical to consistently test the *non-specific* bacterial response using the same type strains and growth 7 conditions. However, due to vast diversity of bacteria, which is reflected in differences of the 8 bacterial cell wall composition and thickness, ^{59,60} wettability, and *specific* host interactions 9 of clinical isolates, different strains that belong to the same species, may respond differently 10 to the same nanopattern. ^{61,62} 11 12 One important aspect to study, which is largely absent in literature, is the protein preconditioning of mechano-bactericidal surfaces, especially when considering end 13 applications such as biomedical implants. As these implants are inserted into the body, the 14 first thing that comes into contact with them is blood and this results in instantaneous 15 formation of a protein film. This protein film might mask or reduce the effect of the 16 mechano-bactericidal surface as it can fill the spacings between the nanostructures rendering 17 them ineffective. That is why, it is of utmost importance to study serum preconditioning of 18 the surfaces prior to incubation with bacteria. Understanding how that protein film forms on 19 20 mechano-bactericidal surfaces can help the structure optimization process to be more efficiently bactericidal. 21 After incubation, the first objective to seek when studying a mechanically designed 22 23 bactericidal surface is to evaluate the effectiveness of this surface towards a specific bacterial strain. For that, it would be beneficial to know the number of bacteria attached to the surface 24 (dead and alive). Additionally, it is imperative to ensure that the surface is bactericidal by 25

detecting the count of dead bacteria over a timespan and, to quantitatively determine its
 bactericidal efficiency expressed as:

$$\eta_{\text{bactericidal}}(\%) = \left(\frac{(A-B)}{B}\right) \times 100 \tag{1}$$

4

3

where A is the number of dead bacteria on the test sample surface and B is the number of
dead bacteria on the reference sample surface.

Previously, bactericidal efficiency has been evaluated using the colony counting or colony
forming unit method (CFU). It is a method used to quantify the number of colonies that can
grow in a nutrient medium (agar) from a swab of bacteria-exposed test surface or after rinsing
the bacterial test surface and replating the suspension medium. This method can indirectly
quantify the number of live and attached bacteria on the test surface.

However, the CFU method does not guarantee complete removal of all bacteria from the 12 surface and often times, the technique for removal (e.g., sonication, enzyme) may cause cell 13 death. Additionally, CFU underestimates the true killing efficiency of the surface as it fails to 14 account for the number of dead bacteria on the surface and the dead bacteria that could have 15 been released out onto the suspension after death^{41,63}. This method evaluates the ability of a 16 bacteria to attach and proliferate on the surface rather than the killing ability of a surface. 17 That is why this technique is better suited to evaluate the anti-biofouling functionality rather 18 than the bactericidal efficiency of a test surface, unless accompanied by other forms of 19 viability quantification such as Live/dead staining. 20

Although theoretically, there are distinct definitions of bacteriostatic versus bactericidal
surfaces, in practice they are ill-defined. For instance, when discussing bacterial killing
agents or antibiotics, a general consensus is that in an incubation duration of 18-24 hours, if
the agent is able to kill 90-99% bacteria, it is called bacteriostatic and if it is able to kill
>99.9% bacteria, it is considered bactericidal.⁶⁴ This is to account for the *in vivo* factors in

infection with time. However, when discussing bacteria killing surfaces, the quantitative
value is not specified for the designation between bactericidal and bacteriostatic. This
constitutes an empirical need to identify the clinically relevant threshold above which the rate
of bacterial death is quicker than the multiplication of bacteria in the deep prosthetic surgical
site infection. Understanding this threshold will allow for the consistent labelling of
bactericidal surfaces in the biomedical field.



Figure 4: The incubation set-up including a) the method and volume of bacterial suspension 1 contact with the sample surface: the overlay, spray and immersion methods, b) the flow 2 conditions during incubation: static and dynamic comprising ultrasonic shaking and 3 controlled flow, c) the sample orientation: face up, upright and upside down, d) Surface 4 evaluation by rinsing, e) the bacterial suspension live/dead cell count methods, f) the 5 evaluation of bacterial adhesion on nanostructured surfaces using lateral force microscopy. 6 7 The dotted red rectangle denotes the areas that are least explored or unexplored as of vet. The durability of the bactericidal function is under question and experimental tests can be 8 intriguingly used to understand the fate of bacteria after they become non-viable on the 9 surface. Intuitively, one would think that the non-viable bacteria would remain in the pits of 10 the mechano-bactericidal structured surface and constitute a means of adhesion and nutrition 11 for newly adhering bacteria. Another possible fate of the non-viable bacteria however would 12 be the detachment and return to bulk fluid. In the latter case, considering the number of non-13 viable bacteria present in the bulk liquid would be important to quantify the bactericidal 14 efficiency of the test surface. It is also vital to quantify the time of the killing of a bacterium 15 16 to judge the degree of surface's lethalness against high bacterial loads. The experimental techniques used to address these points are relatively straightforward. For 17 18 instance, the number of bacteria adhering to the surface and/or present in the bulk liquid can 19 be evaluated by different types of assays in conjunction with labelling methods such as fluorescent staining, dye staining and several others that would allow the differentiation 20 between live and dead bacterial cells as presented in Fig. 4 (e). Most commonly, Confocal 21 Laser Scanning Microscopy and BacLight viability testing kits (Syto9TM fluorescent green & 22 Propidium iodide fluorescent red) are used for live/dead assays as shown in Fig. 4 (a). 23 Through this method, Nguyen et al.³¹ tracked P. aeruginosa bacterial cells on silicon 24 mechano-bactericidal surfaces, observing their detachment as presented in Fig. 5 (b). This 25 test method is based on the assessment of the membrane permeability of bacteria. Syto9TM is 26 a dye that can enter live and dead cells alike, while Propidium iodide or PI can only stain 27 dead cells. There have been a few problems associated with the use of these dyes in 28

1 determining cell viability, for instance in dye bleaching due to overexposure, low intensity of PI especially at high dead bacterial loads and orange-vellow coloring of some bacteria which 2 is attributed to the slow permeability of PI after SYTO9 staining. That is why care must be 3 4 taken while performing measurements which such dyes, by for example quickly and efficiently taking the measurements and closing the microscope shutter in between captures 5 6 to delay the bleaching effect. Additionally, atomic force microscopy (AFM) was used to quantify this detachment cycle using quantitative imaging mode (QITM) to avoid applying any 7 significant lateral forces to the cells (Fig. 5 c).^{31,65} 8 9 Another important objective should be to evaluate how bacteria die on the mechanobactericidal surfaces. As it has been shown by Jenkins *et al.*³³ and Ishak *et al.*⁶⁶ the number 10 of bacteria dying from penetration does not necessarily equate to the total number of dead 11 12 bacteria. That is why, to understand what mechanisms are at play in the bactericidal action of the test surface, it is important to quantify the number of bacteria that are dead specifically 13 from penetration or deformation and compare it to the total number of dead bacteria. 14 Bactericidal mechanisms, other than penetration and stretching, that surfaces can be 15 exhibiting should be investigated to see if they are occurring, such as oxidative stress or 16 others. Additionally, the driving force of the mechano-bactericidal activity needs to be 17 investigated. For instance, samples can be incubated in different orientations to evaluate the 18 gravity effect on the bactericidal activity and if it is indeed the driving force for it. The 19 20 adhesion force between the bacteria and the surface can also be investigated to see whether it is enough to invoke the rupture of the bacterial membrane. 21 Furthermore, bioAFM can be used to quantify the adhesion force between the bacteria and 22 23 the surface by lateral force microscopy as presented schematically in Fig. 4 (f), and to quantify the elastic properties of the bacterial cell by AFM force spectroscopy through 24 indentation and retraction.⁶⁷⁻⁶⁹ 25

1 These points are harder to address as techniques that could be used to do so require expensive, special and sophisticated equipment and multidisciplinary training. Furthermore, 2 investigating the detailed workings of mechano-bactericidal surfaces ideally requires real-3 time monitoring and in-depth microbiological investigations. This research area is very 4 fertile, and many basic discoveries are yet to occur. For example, investigation into whether 5 cell death was mediated by ROS on mechano-bactericidal surfaces was only done recently 6 through protein extraction, proteomic analysis and H₂O₂ labelling assays.³³ Cross-sectional 7 observation of surface and bacteria contact performed through SEM-FIB or TEM can aid in 8 analyzing if bacterial membranes are being deformed and penetrated by the nanostructures 9 present on mechano-bactericidal surfaces and to what extent (Fig. 4 (d)). 10



Figure 5: (a) CLSM images of viable and non-viable *S. aureus* and *P. aeruginosa* on
nanostructured surfaces.⁴⁴ (b) CLSM and (c) AFM tracking of non-viable bacteria on
mechano-bactericidal nano-arrayed surface. Reprinted from ref ³¹ by permission of Royal
Society of Chemistry. Copyright 2019. (d) Overlay/drop-test on Nano-Silicon surface:
Viability of bacteria as a function of time as the bacterial droplet is subject to evaporation
(ALI is the air liquid interface). Live cells are green and non-viable cells are red. Reprinted
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9 The effects of the flow on attachment and death of bacteria have not been extensively
10 explored as most experimental studies follow static incubation protocols (see Fig. 4 (b)). On
11 one hand, the efficiency under static protocols can be underrated compared to the efficiency
12 in flow conditions. That is because in static conditions, a build-up of bacteria may occur. Yet

1 on the other hand, the efficiency under static protocols can also be overrated as stated by Valiei *et al.*³⁴. They argued that in static conditions, air bubbles present between the surface 2 and the bacteria suspension could expand during microscopic evaluation and induce an 3 4 external force that drives the killing effect of nanostructures. Whereas in dynamic conditions, these bubbles are simply eliminated by ultrasonic shaking. In fact, static conditions do not 5 6 mimic reality. In biomedical applications there is fluid flow surrounding biomedical implants. Therefore, the determination of bactericidal efficiency should be done under realistic flow 7 conditions (measured shear flow rate). It is however important to keep in mind that under 8 9 dynamic conditions, the adhesion of bacteria decreases, and detachment increases compared to static conditions which might affect the results. It is also possible to postulate that under 10 flow conditions, the bacteria experience advective flow which causes their collision with 11 nanopillars with a significant impact force that might increase the killing efficiency.⁷⁰ On the 12 other hand, a recent study by Kamarajan et al.⁷¹ has reported an increased adhesion and 13 survival rate for *P. aureuginosa* PAO1 on nanostructured surfaces under flow conditions. 14 They attributed this behavior to the increased secretion of EPS adopted by the bacteria which 15 masked the nanopillar tips. This goes to show that understanding the response of bacteria to 16 mechano-bactericidal surfaces in flow conditions is vital in determining the surfaces' true 17 efficiency. A more detailed discussion of experimentation under flow conditions can be 18 found in a review by Senevirathne *et al.*⁴¹. 19

Additionally, substrate orientation (Fig. 4 (c)) is important to help determine the driving force
of the mechanism.

A summary of the techniques used to evaluate and investigate mechano-bactericidal surfaces
to date highlighting their advantages, limitations, and the errors that could possibly occur by
their usage can be found in the supporting information.

25

Mechanisms revealed from the experimental approaches

1 Through experimental approaches, nanostructured surfaces gained their reputation as mechano-bactericidal surfaces, independent from chemical effects⁴⁸ as the functionality 2 (bacteria killing ability) was shown to persist across different materials. 3 4 Early research relied on observations from techniques such as Scanning electron microscopy (SEM) imaging to form the hypothesis that nanostructures puncture bacterial cell walls 5 6 leading to the release of cytoplasmic fluid (Fig. 6 (c)). This was due to compromised cells taking the shape of the nanopillars, revealed by the SEM images which led to the conclusion 7 that the nanostructures puncture the bacteria. Techniques of evaluation then progressed into 8 9 methods that can reveal the nanostructure/bacteria interaction through cross-sectional imaging e.g., Focused Ion Beam (FIB). Recently, slice-by-slice FIB-SEM data reconstruction 10 was used to better observe the interaction of nanopillars with single cells⁷² leading to an 11 improvement from the previous postulations. Several hypotheses then emerged, one of which 12 is specific to Gram-negative motile bacteria.¹⁶ This hypothesis suggests that the biocidal 13 activity is mediated by an extracellular polymeric substance (EPS). This mechanism was later 14 15 refuted as it disregards the fact that the bactericidal effect occurred within a few minutes of contact whereas EPS secretion is thought to take significantly longer (hours to days).^{35,17} 16 Amidst the development of these hypotheses, it was experimentally established that the 17 effusion of intracellular fluid does occur for Escherichia coli on nanostructured surfaces 18 using fluorescent proteins.⁷³ This important finding confirmed that rupturing of the bacterial 19 membrane is involved in the bactericidal action presented by the nanostructures. 20



1

Figure 6: (a) Factors that may influence the initial bacterial attachment to a solid-liquid
interface adapted from ⁷⁴, (b) The stretching mechanism proposed, (c) The penetration
mechanism based on sharp nanostructures and (d) the synergistic ROS mediated mechanobactericidal mechanism.

Meanwhile, one of the coauthors Ivanova *et al.*¹⁴ suggested that the bactericidal activity of
nanostructures is actually driven by the mechanical and structural responses of the bacterial
cell as it adheres to the nanostructures. Particularly, these responses create inelastic stress
imposed by the surface nano-topography on the peptidoglycan cell wall and inner membrane

4

1 of the bacterial cells. Herein, the surface ineffectiveness against Gram-positive bacteria was attributed to the thickness of the peptidoglycan layer in the cell wall as it is four to five times 2 thicker than that of Gram-negative bacteria.⁷⁵ This was named as the "stretching" mechanism 3 (Fig. 6 (b)) and thought to compete the "penetration" mechanism.

Exhaustively, all these hypotheses were inferred from indirect evidence from the same 5 experimental approaches (mainly CLSM, SEM and FIB-SEM) with interpretations based on 6 a priori knowledge, which introduced a certain bias towards the previously conceived 7 stretching and penetration mechanisms. It is imperative to look at the problem from an 8 alternative perspective proposed here. 9

10 A few recent studies have shed light on the shortcomings of the experimental approaches employed in understanding the underlying mechanisms of the mechano-bactericidal effect. 11 One such study by Jenkins *et al.* 33 provided a baseline for a reactive oxygen species (ROS) 12 mediated mechanism as bacteria exposed to the nanostructures (be it Gram-positive or Gram-13 negative) were found to be oxidatively stressed. This occurs when bacteria are subjected to a 14 lethal stressor which triggers production of ROS as a self-destruction mechanism.⁷⁶ Bacteria 15 can detoxify low levels of reactive oxygen species (except hydroxyl radical) through several 16 protective enzymes (e.g. superoxide dismutase, catalases).⁷⁷ However, if the ROS levels 17 surge above a certain threshold, the death process becomes self-driven and irreversible even 18 if the initial stressor is removed.⁷⁶ This synergistic ROS-mediated mechano-bactericidal 19 mechanism, illustrated in Fig. 6 (d), sheds a new light on the importance of expanding the 20 experimental approach to look beyond the "penetration" or stretching mechanisms. In other 21 words, the mechanism, although shown to be surface chemistry independent, does involve 22 23 chemistry at a bacterial level contrary to the currently presented pure mechanistic models.

Nonetheless, understanding the proposed mechanisms is imperative to evaluate their role in 1 the bactericidal pathway of the nanostructures. "Penetration" as a term has repeatedly been 2 used to explain that the failure of the bacterial membrane in the area that is directly in contact 3 with the nanostructures. However, the term penetration in its essence indicates that stress 4 concentrations leading to fracture occurs at the failure site which in turn requires a very sharp 5 rigid structure. For "penetration" or puncture to mechanically occur, the degree of freedom of 6 the penetrated object should be restricted which is mostly not the case in this scenario of 7 bacteria-nanostructure interaction. Thus, if failure occurs at the apex of the nanopillar, it is 8 9 due to the local stretching or pressure on the membrane in that region. The question remains as to where the critical action site is within the mechano-bactericidal mechanism and what is 10 the driving force for that deformation. As direct observation and quantification of such 11 aspects is extremely difficult with the techniques and instruments available, simulation 12 studies have been deployed to find the right answers. 13

14

Mechanisms revealed by simulations

The simulation models developed so far can be categorized into analytical models and 15 computational (numerical) models. In analytical models, equations based on surface energy 16 considerations, thermodynamic equilibrium and energy minimization are formulated and 17 solved by introducing geometric constraints relating to both the bacteria and the 18 nanostructured surface. The deformation of the adsorbing bacteria, in these models, is 19 considered as a necessity to reach thermodynamic equilibrium. In other words, adsorbing 20 bacteria continue to envelop the nanostructures until equilibrium is reached. These models 21 differ in the way they define the change in free energy (based on local stretching degree and 22 stretching modulus;^{22,25} membrane tension and strain tensors;⁷⁸ work required to bend the 23 bacterial wall around the nanopillar shaft;²⁷ and variation of the adhesion contact angle as the 24

1 cell migrates into nanopillars²⁸).



Figure 7: a) Forces proposed to drive bacteria towards the nanopillars, b) Energy-based analytical model of bacterial cell adhering and stretching on nanostructured surfaces in four configurations depending on the pillar density, the slope and the height. α_A and α_B are the stretching degrees in regions A and B respectively. The larger stretching degree indicates the critical action site of that said configuration,^{22,25} c) a contour plot of longitudinal uniaxial strain for an adhered bacterial envelope. The contact region is probed by L1, the suspended regions are probed by L2, L3 and L4. At each location, in-plane uniaxial strains are probed at

three points through the thickness, representing each of the three layers. For the plasma
membrane, the maximal through-thickness value is found at the top plane. For the outer
leaflet, the maximal through thickness value is found in the suspended region.⁷⁹ Adapted
from ⁷⁹ with permission from Elsevier. Copyright 2021.

In computational models, the bacteria-nanostructure interaction is modelled with finite 5 6 element method based on a major assumption that the bacteria have no fluid surroundings. The simulation models developed so far have thus assumed bacteria-surface interaction in 7 vacuum – an aspect which needs to be evaluated properly. Also, failure of a bacteria is based 8 9 on the maximum strain in the membrane which is assumed to occur when the local strain value exceeds the permissible strain threshold. The value of this strain threshold reported in 10 the literature shows high percentage variability > 50%, which indicates that the currently 11 reported FEA simulation studies are incoherent. For example, Velic *et al.*⁷⁹ based the rupture 12 strain range on experimentally reported values of the rupture strains of different 13 organisms^{80,81}, bacterial threads⁸², and values obtained from coarse grain modelling of 14 mimetic lipid systems⁸³ (0.18-0.65 as longitudinal strain for the peptidoglycan layer and 0.05-15 0.35 as areal strain for the outer membrane). Mirzaali *et al.*²³ considered the rupture strain 16 value of 0.5 through the work of Thwaites and Mendelson⁸⁴ which was based on the 17 elongation of *B. subtilis* bacterial thread rather than the elongation of a single bacterium. To 18 add to this dilemma, other studies⁸⁵ have reported vivid values (0.08 for *S. aureus*, 0.12 for *E.* 19 coli, and 0.05 for *P. aeruginosa*). Clearly, this important information which is a prerequisite 20 for meaningful finite element simulations needs reinvestigation. The inconsistency reported 21 so far is largely due to the fact that the constitutive modelling of a bacteria is ill-defined and 22 23 the methods employed to evaluate the mechanical properties of the bacteria were not comprehensive enough. A full set of data can be obtained by fully developing a set of AFM 24 nanoindentation experiments, especially accounting for the anisotropy presented by a 25

bacterium. Clearly one such anomaly which can be seen as an example in the reported
literature is the assumption of a gravitational force⁴² acting on the bacteria which is an
incorrect assumption since a bacterium is not of its own but is a freely floating particle in a
fluid. Therefore, any future modelling studies needs to consider these aspects as well as other
aspects, such as the boundary conditions, loading type, strain type etc. very carefully.

6

The driving forces

7 To develop any simulation whether analytical or computational, assumptions must be made as to what are the forces driving/governing the phenomenon that is being modelled. Gravity, 8 9 as shown in Fig. 7 (a), has been incorrectly considered as the main driving force in some studies. Hence, the question arises as to whether the magnitude of a bacterium's gravity is 10 enough to cause its rupture. Xue et al.⁴² studied the stretching of bacteria due to gravity on 11 two different geometries: nanopillars and nanoridges. In their model, the stretching degree of 12 the bacterial membrane exceeded the calculated critical stretch value. The rupture of bacterial 13 membrane was inferred to be more likely on nanopillars than nanoridges. Additionally, an 14 FEA study conducted by Velic *et al.*⁸⁶ found that the force of gravity on an *S. aureus* 15 bacterial cell, coupled with the force from the water column above the bacterium (tens of 16 piconewtons) strains it enough, as it contacts a nanostructured surface, to exceed the assumed 17 strain threshold of 0.5. In both studies, the stiffness of the bacterial membrane was assumed 18 19 to be in the range of a few Pascals to a few kiloPascals (kPa).

This is inconsistent with AFM studies which have shown a wide range of stiffness i.e., 0.2 to 95 MPa.⁸⁷ Additionally, AFM studies show that bacterial cells including *S. aureus* can withstand forces of several nanoNewtons before its rupture. Based on this, gravity can be ruled out as the main driver for cell rupture.

Liu *et al.*²⁸ suggested that cell adsorption is driven by the differential energy gradient (i.e. 1 between Gibbs surface free energy and deformation surface energy) along the height of the 2 nanopillars (i.e. high at the tip of the nanopillar, and low at the base). The force induced by 3 this gradient (100 nN) drives the bacterial cell downwards towards the nanopillars, instigating 4 the elastic deformation of the bacterial cell wall. If pressure or stress exceeds the yield 5 strength of the wall, the latter undergoes creep until rupture. This model can be used to justify 6 the bactericidal effect of a nanostructure on bacteria yet imply a non-cytotoxic effect of such 7 surfaces on mammalian cells. Since the force stems from a differential energy gradient of the 8 9 nanopillars, the smaller volume of the cell in contact, the larger the effect of the pressure induced on it by a single pillar. It is known that bacterial cells have sizes in the range of few 10 hundreds of nanometers to a few micrometers, whereas mammalian cells are usually in the 11 range of tens to hundreds of micrometers. Thus, according to this model mammalian cells 12 undergo reduced amounts of pressure which do not cause damage to their membranes. 13

Another driving force suggested to cause the rupture of bacteria is the surface energy released 14 as the cell wall binds to the surface.²⁷ If the total surface binding energy is larger than the 15 stretching and bending energy, the bacterial membrane drops below the equilibrium drop 16 height, the tensile stress exceeds the tensile strength of the bacterial membrane, then the 17 membrane tears. In the case of slow binding, influenced by active interactions and responses 18 19 of the bacteria towards the surface such as hydrophobic interactions, the bacterial death 20 occurs gradually. In the case of fast binding, induced by physical-chemical forces (i.e., van der Waals forces and hydrogen bonding), the rupture occurs instantaneously as the bacterial 21 cell wall binds to the top of the nanopillar with a surplus of energy. 22

Adhesion-driven deformation of the bacterial envelope as it adsorbs onto a nanopillar was
also considered in the computational work of Velic *et al.*⁷⁹. In this model, the adhesion was

considered as an evolving "bond front" and applied as a downward pressure load on an area
 that increased in size incrementally.

When considering the motility of some bacterial strains or bacteria in flow conditions, the 3 frictional behavior in contact with such surfaces becomes of high importance. Studies report 4 frictional instabilities experienced in contact with nanostructured surfaces where shear tracing 5 showed irregular and sharp peaks across such structured surfaces compared to smooth 6 surfaces⁸⁸. These sharp spikes can present lateral force contributing to the disruptive action of 7 nanoscale features on the bacterial cell wall influencing the bacterial stress response that could 8 9 manifest in turgor pressure fluctuation and ROS production. The frictional behavior of nanostructured surfaces is highly influenced by the surface specific parameters such as surface 10 roughness parameters⁸⁹, nanofeature geometries, and their densities⁹⁰. In this light, studying 11 nanostructured surfaces exhibiting different frictional behaviors and correlating it with their 12 bactericidal performance, could give new insight into the optimization of the mechano-13 bactericidal surfaces. 14

15

Critical action sites

16 The competing "penetration" and stretching mechanisms can be considered analogous to the competing critical action sites of a bacterial membrane in analytical and computational 17 modelling. In most energy-based models, the critical action site is in the area suspended 18 between the two pillars ^{22,25,45,46,91}. That is because in those models, the bacterial membrane 19 deforms non-uniformly. The stretching of the suspended bacterium occurs to accommodate to 20 the active adsorption onto the nanopillar. Exceptionally, in an extension to work by Pogodin 21 et al.²⁵ Wu et al.²² found that by varying the heights of adjacent nanopillars, a higher 22 stretching degree is induced on the membrane region adsorbed onto the nanopillar than on 23 that suspended region. This model is illustrated in Fig. 7 (b). In most computational models, 24

however, the entire membrane undergoes the same force (body force) and the strain across 1 the entire membrane is uniform. The presence of the nanopillars restricts that deformation 2 and induces tension in the membrane at the pillar apex. Interestingly in the computational 3 model that considered adhesion-driven rupture, the critical action sites did not coincide 4 between the layers of the cell wall model of a Gram-negative bacterium (Fig. 7 (c)). 5 Uniquely, the cell wall was modelled as a plasma membrane and peptidoglycan made up of 6 two leaflets. The critical action site for the whole cell envelope was found at the pillar apex as 7 both the inner leaflet and plasma membrane fail at that location with a strain much greater 8 9 than that transpiring anywhere in the outer leaflet. The critical action site of the outer leaflet of the peptidoglycan, which is in direct contact with the pillar, remains in the suspended 10 region. That is due to the strongly modelled bond between this leaflet's adsorbed region and 11 the pillar, that forces the reallocation of deformation to the suspended region. Unlike most 12 models, this study did not over-simplify all the complexities of a bacterial membrane and its 13 components nor assumed it to be a planar elastic layer (plane strain). It instead brought 14 attention to (i) the importance of a more detailed multi-layered cell wall model, (ii) the need 15 for three-dimensional analysis of this non-developable problem, and (iii) the significance of 16 force application as a "bond front" mimicking adhesion. 17

In layered bacterial membrane models, as in reality, the stresses that can be withstood by different layers (different materials) vary. In addition, some materials can resist compression more than tension or vice versa. Knowing these material details can help shape the design of the nanostructure to engineer the location of the critical action site appropriately. This can be done by understanding and adjusting the geometrical considerations of nanostructures. It implies the need for developing material constitutive models of bacterial membranes in order to model complex membrane structures reliably.

1	Nevertheless, considering the complexities of the bacteria-nanostructure interaction, factors
2	beyond geometrical considerations can be influential as discussed next.
3	Factors influencing the bactericidal activity of nanostructured surfaces
4	The mechano-bactericidal effect is a complex interplay of bacteria and substrate-dependent
5	factors (see Fig. 8), which may be classified into four main categories: geometric, biological,
6	electric and interfacial physical factors.
7	The structural dimensions including the nanofeature radius, shape,
8	interspacing/pitch/nanofeature area density, and height/aspect-ratio are the main constituents
9	of the geometric factor.
10	Bacteria-nanofeature contact area: Radius and shape
11	The tip size of the nanofeature is of great importance because it is the first point of contact
12	between the bacteria and the surface. Studies suggest that a smaller tip radius induces higher
13	pressure on the bacterial membrane and enhances the bactericidal effect of a nanostructured
14	surface. ^{14,23,42,92} Some other studies based on the analytical models as previously discussed,
15	alluded to the fact that a larger radius provides a wider contact area. This pushes the
16	suspended region of the membrane to try and accommodate for the perimeter change by
17	stretching and ultimately rupturing. ^{78,79}
18	It is evident that there is a limited range of radii in which nanopillars exhibit enhanced
19	bactericidal effects. According to simulations, that range falls between 50-80 nm, ⁴⁶ where the
20	radii is big enough to anchor the bacterial membrane, yet small enough to push bacterial
21	membrane deformation to rupture.
22	The shape of the nanofeatures relates directly to the available contact area (see Fig. 8 (a) and
23	Fig. 9 (A)). Mo et al. ⁹³ tested micro and nano arrays of cones and pillars and found that

- 1 nanocones, as opposed to pillars, possess enhanced bactericidal activity due to the tip
- 2 sharpness. The slope presented by the nanocone features also plays a role in enhanced
- 3 bactericidal activity as it increases the contact area along the vertical region of the feature.²²



Figure 8: Factors affecting the efficacy of a mechano-bactericidal surface for a specific
bacterial strain. (a) Contact area controlled by feature radius and shape, (b) length scale of the
bacteria/structures, (c) height of the structures, (d) the nanofeature interspacing and array
density, (e) elasticity of the pillars/structures, (f) aspect ratio-controlled rigidity, (g) Gram
stain of the bacteria, (h) age of the bacteria, (i) Surface appendages of the bacteria, (j)
electrical charge of the surface and bacteria, (k) the bacteria/surface interfacial-physical
factors.

8

Nanofeature interspacing and array density

For a nanostructured surface to exert stress on a bacterium, the interspacing of the structures 9 needs to be smaller than the diameter of the bacterium, be it cocci or rod-shaped. The 10 bacterium can otherwise align to the spaces between the nanopillars, proliferate and develop a 11 biofilm (see Fig. 8 (b) and Fig. 9 (Be)).⁹⁴ The height of nanopillars should also accommodate 12 the maximum stretching of the bacterial cell wall and be larger than the sinking depth of the 13 bacterium as shown in Fig. 8 (c), otherwise the bacterium will only experience elastic 14 deformation and then rest on the bottom surface with no additional mechanical deformation 15 to cause lysis. 16

Simultaneously, conflicting reports on the role of interspacing in bactericidal efficiency can also be seen. For instance, Mirzaali *et al.*²³ suggested that higher interspacing increases the stretching degree of the bacteria which improves the bactericidal efficiency of the surface but warns that an increased interspacing could lead to cytotoxicity rendering it unsuitable for *invivo* applications.

Their finite element (FE) model predicted a combination of width and interspacing (W= 50
nm, IS = 300 nm) to be vital in inducing bactericidal effect against *S. aureus* while avoiding
cytotoxic reactions. Conversely, Modaresifar *et al.*³² investigated the effect of interspacing of

- 1 silicon nanostructures on the viability of *S. aureus* and found that a lower pitch of
- 2 interspacing led to an improved bactericidal activity with the highest bactericidal efficiency
- 3 achieved for a spacing of 100 nm.



Figure 9: A: Ranging nanostructure shapes and tip radii; Aa) blunt tip nanopillars,⁷⁸ Ab)
cotton-swab shaped nanopillars,⁷⁸ Ac) sharp nanopillars,¹⁴ Ad) sharp conical nanofeatures,
reprinted from ref ⁴⁷ by permission of AIP Publishing. Copyright 2016, Ae) nanowires,³³ Af)
cicada-like conical nanofeatures, reprinted from ref⁹⁵ by permission of ACS Publications.

Copyright 2015. B: Ranging interspacing and feature densities;³² Be) P. aeruginosa aligned 1 between nanopillar interspacing, reprinted from ref⁹⁴ by permission of ACS Publications. 2 Copyright 2010. C: Elastic and high aspect ratio structures; Ca) enhanced bactericidal effect, 3 reprinted from ref⁹⁶ by permission of PNAS. The yellow dots represent the bacteria-structure 4 interface, blue line represent the alignment of the substrate. Cb, Cc) Impeded bactericidal 5 effect. **Cb:** Reprinted from⁹³ by permission of Elsevier. Copyright 2020. **Cc:** Reprinted from 6 ref ⁹⁷ by permission of ACS publications. Copyright 2016. **D:** Biological and interfacial 7 physical factors affecting bactericidal efficiency; **Da**) bacterium (i.e. S. oneidensis) flagella 8 wrapped around micro-sized pillar to maximize the contact area, reprinted from ref ⁹⁸ by 9 permission of ACS Publications. Copyright 2013. **Db**) Gram positive S. aureus hardly 10 perturbed on nanowire-like structure,³³ Dc) Gram-negative E. coli severely deformed on 11 nanowire like structure,³³ Dd, De) superhydrophobic structures induce higher hydrophobic-12 *P. aeruginosa* attachment and death than superhydrophilic structured surface, reprinted from 13 ref¹⁷ by permission of ACS publications. Copyright 2017. **Df**) Positively charged 14 nanostructured surface induces rupture of gram-positive S. aureus.⁹⁹ 15

Velic *et al.*⁷⁹ agreed that a reduced interspacing increases the bactericidal effect of a
nanostructured surface. The authors argued that the simulation studies suggesting the larger
interspacing increases the deformation of the envelope had assumed that a "constant" load
was being applied. This assumption results in load distribution over a given number of pillars,
thus directly inducing more deformation with further spaced pillars and less contact points.
On the other hand, in the case of bacterial interaction with nanostructures, the interaction
forces are not distributed, but developed at each individual nanopillar.

23 This signifies that more contact points will induce more deformation and a smaller

24 interspacing is bactericidal enhancing.

1 Some studies suggested evaluating the area density of nanofeatures (see Figure 8 (d)), instead of their interspacing or pitch, as an important parameter in the adhesion pattern and 2 therefore the stretching degree of the attached bacterial cells.²² Kelleher et al.¹⁰⁰ observed a 3 linear correlation between bactericidal activity and the number of nanostructures with which 4 a bacterial cell comes in contact with. In their findings however, the surface that exhibited the 5 6 highest bactericidal efficiency (and the highest pillar density) was the surface with the highest feature aspect ratio (i.e., ratio of height over width) of around 1.54 with height of 241 nm, 7 pitch 165 nm and diameter 156 nm. In this case, the height and pillar density parameters 8 9 cannot be decoupled, and the distinction of which parameter had a more significant effect on the bactericidal activity was not possible. 10

11

Aspect ratio and rigidity

12 Few studies have investigated the effect of the aspect ratio and the rigidity of the nanopillars on the bactericidal efficiency of mechano-bactericidal nanostructures. When dealing with 13 14 elastic pillars, interpillar adhesion and clustering could partially compensate for the force exhibited on the bacterial membrane.^{96,101} This can hinder the bactericidal ability of a surface 15 which is shown in Fig. 8 (e) and Fig. 9 (Cb), however the flexibility of high aspect ratio 16 structures has been shown to enhance elastic energy storage in nanofeatures. They release this 17 energy by bending when in contact with bacteria, which improves the bactericidal activity of 18 the nanostructured surface as shown in Fig. 9 (Ca, Cc).¹⁰² Thus, a threshold exists by which 19 the deformation of the elastic pillar remains favorable to the bactericidal action. The 20 deformation of these nanofeatures is dependent on surface material properties, nanofeature 21 dimensions and the adhesion force of the bacterium to the substratum surface and can be 22 expressed as (in the case of nanopillars) $\Delta x = \frac{F_{adhesion}}{k}$ where k is the pillar stiffness 23 defined as k= $\pi E_{\text{material}} \frac{3r^4}{4l^3}$ where r is the radius of the nanopillar and l is its length. 24

As opposed to the elastic modulus of a material, stiffness or eigenvalue of the nanostructure 1 pillar is influenced significantly by its aspect ratio (Fig. 8 (f)). The high aspect ratio 2 nanostructures on the wings of Palapsalta eyrei (cicada species) possess an enhanced 3 4 bactericidal activity and short kill time compared to wings from other cicada species that contain lower aspect ratios, namely *Psaltoda claripennis* and *Aleeta curvicosta*.¹⁰³ The height 5 6 of the nanofeatures varies from 100 nm to 2 µm, and this largely contributes to the aspect ratio while the diameter is controlled in a limited margin within the fabricated nanopillars. 7 Ivanova *et al.*⁹⁶ reported that a height of 360 nm yielded the most efficient results against 8 9 both P. aeruginosa and S. aureus with little to no clustering of the pillars. Generally, the work done in replication and fabrication of mechano-bactericidal structures 10 has failed to report the repeatability in the feature dimensions and geometries which limits 11 direct comparison of results produced by different research groups.¹² However, of the few 12 studies that have successfully reported characterized morphology of the bactericidal surface, 13 the dimensions of effective surfaces were in the range of 100 nm to 1 µm height, 10 to 300 14 nm diameter and less than 500 nm spacing.¹⁰⁴ 15 **Biological** factors 16 As the mechano-bactericidal effect is surface and bacteria dependent, it is imperative to pay 17 attention to the biological factors that might influence the bactericidal action observed. These 18 factors, unlike the geometric ones, are not static and most of the time cannot be controlled. 19 For instance, the composition of the bacterial cell wall, as classified by the Gram stain, plays 20 a role in governing its susceptibility to the mechano-bactericidal surfaces. Fig. 8 (g) contrasts 21 the differences between a Gram-positive and Gram-negative bacterial membrane structure. 22 Gram-positive bacteria possess an inner membrane and a thick peptidoglycan layer (20-100 23 nm), whereas Gram-negative bacteria possess outer and inner membranes and an intermediate 24

peptidoglycan layer (only a few nanometers thick).¹⁰⁵ Gram-negative bacteria are thus more 1 susceptible to the killing effect of the nanostructures than Gram-positive bacteria (see Fig. 9 2 (Db, Dc)). Pogodin et al.²⁵ found that exposing Gram-positive bacteria (B. subtilis, 3 Planococcus maritimus, and S. aureus) to microwave radiation reduces their rigidity and 4 increases their vulnerability towards the mechano-bactericidal effect of the nanostructured 5 6 cicada wing surface. In the case of sharp-edged surfaces like black silicon (bSi) with very small tip radii, the sharp edge is able to disrupt both Gram-positive and Gram-negative 7 bacteria leading to their death.¹⁴ 8

9 In addition to the Gram stain, the possession of surface appendages has also been identified as an influencing factor (see Fig. 8 (i)). In a recent study by Ishak et al.⁶⁶, bacterial surface 10 proteins have been observed to play a role in facilitating the deformation of the cell wall as 11 represented in Fig. 8 (i) (top). Additionally, the motility and possession of motile appendages 12 (e.g., fully active flagella) has been associated with a higher probability of bacteria being 13 affected by the bactericidal surface¹⁰⁶. Jindai *et al.* ³⁵ suggested that since flagella makes the 14 first direct contact with the structured surface, it gets entangled with the surface nanofeatures 15 leaving the bacteria some space to move. The bacteria then suffer abrasions after hitting the 16 surface repeatedly causing effusion of intercellular fluid and death. An SEM micrograph 17 presented in Fig. 9 (Da) shows how the flagellum of a bacterium wraps around a micro-sized 18 pillar. 19

Aside from the Gram stain and motility, a bacterium's membrane will pass in phases of
fluctuating rigidity at a young age (< 6 hrs¹⁰⁷) as shown in Fig. 8 (h). This fluctuation occurs
when existing peptidoglycan sacculi breaks to incorporate new material and synthesis of a
new layer of peptidoglycan is under progress.¹⁰⁷ Thus, younger bacteria are more susceptible
to the bactericidal action of nanostructured surfaces than matured bacteria.

1 A few studies have been conducted to test the effect of mechano-bactericidal nanostructures on the adherence and differentiation of eukaryotic human or human-like cells. A common 2 denominator between all these studies is unusual elongated morphology of the cells adhered 3 on these surfaces along with the lack of cellular spreading compared to control smooth 4 surfaces¹⁰⁸. However, Le Clainche *et al.*¹⁰⁹ reported that hASCs were able to proliferate and 5 6 maintain their ability for trilineage differentiation on such nanostructured surfaces. Additionally, Bhadra *et al.*¹¹⁰ showed that human fibroblasts are able to proliferate and 7 provide a high area coverage on such surfaces. Modaresifar *et al.*¹¹¹ found that the metabolic 8 9 response of preosteoblast cells was reduced after 14 days on the most efficient bactericidal (40% dead S. aureus) surface tested compared to control flat surfaces. Additional 10 standardized studies to study the cytotoxicity of mechano-bactericidal surfaces are needed in 11 order to be able to compare the performance of these surfaces across the board and their 12 applicability to implant surfaces. 13

14

Electric and Interfacial-physical

From the mechanisms formerly discussed, the consensus is that mechano-bactericidal activity 15 is a contact phenomenon. Mechano-bactericidal activity can only be invoked by contact, 16 adsorption and adhesion between the bacteria and the surface. The adhesion of the bacteria 17 with the surface is therefore a noteworthy factor in making the surface bactericidal. 18 Adhesion is heavily affected by the electrostatic charge of the bacteria and the substrate and 19 their respective wettability, among other factors (i.e. Lifshitz-Van der Waals forces and 20 Brownian movement forces) as explained by the extended DLVO (XDLVO) theory¹¹². 21 22 Bacteria are generally negatively charged. If the surface is also negatively charged, repulsion will be dominant (Fig. 8 (j)), and the surface might be called anti-biofouling. For mechano-23

bactericidal surfaces relying on adhesion to kill bacteria,¹⁰⁴ positive charges can be beneficial

as they advocate for the attraction of the bacteria to the surface. Chen et al.⁹⁹ combined 1 2 surface structuring by femtosecond laser and positively charging the surface by Laver-by-Layer (LbL) polyelectrolyte coating in order to enhance the bactericidal effect of the 3 4 borosilicate glass surface against S. aureus and E. coli as is presented in Fig. 9 (Df). Generally, the more hydrophobic the bacteria, the higher is its affinity to a hydrophobic 5 surface and greater is the adhesion force between the bacteria and surface as shown in Fig. 8 6 7 (k) and Fig. 9 (Dd, De). Bacteria of different strains can have differing wettability (hydrophobic or hydrophilic) however, hydrophobicity/hydrophilicity of bacteria can alter 8 depending on the environmental changes and bacterial stage of growth.¹¹³ Both hydrophobic 9 and hydrophilic surfaces can exhibit bactericidal actions against a range of bacterial strains. 10 This leads to the inconclusive role of wettability in the mechanism of mechano-bactericidal 11 action.17,114 12

We must note here that the evaluation of different factors impacting the bactericidal effect of 13 nanostructures was performed either through simulations or experiments. During simulation 14 investigations, the models were based on stretching/penetration mechanisms, which discount 15 the biologically dynamic effects of bacterial cells. In the experiments, the techniques used to 16 evaluate the bactericidal activity of a surface were limited to detection of live/dead bacteria. 17 This limits the understanding of the effect of changing geometrical and electric and 18 interfacial physical factors to how those changes are physically affecting the rupture/death of 19 bacteria. It does not explore the effect of varying those factors on any possible biological 20 mechanism that is leading to bacterial death. In the following section, various experimental 21 techniques that have been used to evaluate bactericidal surfaces and the interaction between 22 bacteria and nanostructured surfaces are further discussed. 23

1 Future outlooks

One of the principal challenges that stand in the way of developing and optimizing the
mechano-bactericidal surfaces is the ambiguity and uncertainty surrounding the study of their
bactericidal mechanism(s).

Most evaluation techniques have shown a bias towards specific mechanisms even when 5 seemingly trying to investigate what is behind the killing effect of nanostructured surfaces. It 6 7 is evident that the influence of engineering in this multidisciplinary problem has long prevailed and the microbiological investigation has not taken its full stride. For engineers and 8 9 materials scientists, this enigma seems to be solely related to the mechanics of contact and interaction between the nanostructures and the bacteria. That is why the investigations are 10 focused on observing the penetration and deformation of bacteria. These investigations are 11 not of an easy nature because the experimental evaluation and decoupling of the contribution 12 of geometric, electric, and interfacial physical factors are extremely difficult. 13

14 The problem is even more complex in its essence as it encompasses biological factors. Bacteria are dynamic living cells that behave differently than passive engineering materials. 15 Bacteria can heal small pores induced in their membranes, adjust their turgor pressure to 16 accommodate deformation, induce the production of protective extracellular polymeric 17 matrix under stress, and many other functions that allow them to resist external stressors. This 18 is why it is an opportunistic time for microbiological testing efforts to explore new *in situ* 19 testing methods that can bring us a step further into identifying the reason(s) behind the 20 demise of bacteria in contact with nanostructures at the single cell level, away from bias 21 towards certain proposed mechanisms. 22

Therefore, it is recommended that multiple synchronous and interdisciplinary experimental
approaches be employed to avoid experimental bias towards a single mechanism of action
and to obtain an affirmative understanding of the mechanism(s) at play for mechano-

bactericidal surfaces. Reaching this understanding will allow the combination of different 1 "bactericidal-enhancing" factors to be applied to the design of surfaces targeted to kill 2 common bacteria which are responsible for post-operative infections (i.e., Staphylococcus 3 aureus, Coagulase-negative Staphylococcus species, Escherichia coli, Pseudomonas 4 aeruginosa, Streptococcus species), reducing or even eradicating the incidence of deep 5 surgical site infection. As such knowledge is obtained, it is imperative to use similar 6 7 methodical experimental approaches to understand osteoblast cell interaction with mechanobactericidal nanostructures to avoid impeding cell bone growth around such surfaces for in 8 9 vivo use through biomedical implants. In conjunction with systematic controlled feature design and morphological reporting, this will allow the optimization of the next generation of 10 effective, non-cytotoxic and non-resistant bactericidal surfaces. 11

12 Supporting information

13 The Supporting Information is available free of charge at [link to be inserted].

SI 1: Table summarizing the techniques used to evaluate and investigate mechano-bactericidal
surfaces to date highlighting their advantages, limitations, and the errors that could possibly occur by
their usage.

17 Author contributions

18 Sara Hawi: Conceptualization, Methodology, Investigation, Resources, Data Curation,

19 Writing-original draft, Saurav Goel: Methodology, Resources, reviewing and editing,

20 Supervision, Project administration, Funding acquisition. Vinod Kumar: Writing-reviewing

and editing, Supervision. Oliver Pearce, Wayne Nishio Ayre and Elena P. Ivanova:

22 Experimental support, Knowledge sharing, Improvement in the draft and reviewing

23 Data statement

As this is a review paper, no new data was generated.

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15 Vocabulary

Mechano-bactericidal, a functionality of a structure to kill bacteria mechanically without the 16 need for chemical intervention. Peptidoglycan, a mesh-like polymeric structural element of 17 the bacterial cell wall. It consists of glycan strands cross-linked by short peptides which form 18 a closed structure bordering the cytoplasmic membrane of the bacterium. The peptidoglycan 19 layer is substantially thicker for Gram-positive bacteria than Gram-negative. Cytotoxicity, a 20 21 term used to describe a surface, substance or process that causes cell damage and death. In the context of this paper, it is used to describe undesired human cell damage. Incubation, the 22 process of culturing bacteria under specific conditions that are optimal for their growth. That 23

1 includes a controlled temperature and access to bacteria-specific nutrients. In vivo, a process/experiment that takes in a living organism e.g., mechano-bactericidal implant 2 implanted in animals. Adsorption, a substance is said to be adsorbed when it is concentrated 3 reversibly at a surface. Here, physical adsorption or physisorption is being referred to where 4 the main interacting force is Van der Waals which, along with other interactions (Fig. 6 (a)), 5 influences the initial bacterial attachment to the surface. Strain, it represents elongation or 6 shortening in dimension in response to an applied force in the Mechanical Engineering 7 discipline but in biological discipline it is also used to distinguish subtype of a 8 9 microorganism (e.g., a virus, bacterium, or fungus)

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