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Multi-channel AlGaN/GaN Lateral Schottky Barrier Diodes on Low Resistivity Silicon for Sub-THz Integrated Circuits Applications

A. Eblabla, X. Li, M. Alathbah, Z. Wu, J. Lees and K. Elgaid

Abstract— This work presents novel multi-channel RF lateral Schottky-barrier diodes (SBDs) based on AlGaN/GaN on Low Resistivity (LR) (σ = 0.02 Ω .cm) silicon substrates. The developed technology offers a reduction of 37 % in onset voltage, Von (from 1.34 to 0.84 V), and 36 % in ON-resistance, Ron (1.52 to 0.97 to Ω .mm) as a result of lowering the Schottky barrier height, ϕ_n , when compared to conventional lateral SBDs. No compromise in reverse-breakdown voltage and reverse-bias leakage current performance was observed as both multi-channel and conventional technologies exhibited V_{BV} of $(V_{BV} > 30 \text{ V})$ and I_R of $(I_R < 38 \mu A/mm)$, respectively. Furthermore, a precise small-signal equivalent circuit model was developed and verified for frequencies up to 110 GHz. The fabricated devices exhibited cutoff frequencies of up to 0.6 THz, demonstrating the potential use of lateral AlGaN/GaN SBDs on LR silicon for high-efficiency highfrequency Integrated Circuits applications.

Index Terms— GaN, RF diodes, lateral Schottky barrier diode, sub-THz applications, fin-FET, GaN on silicon.

I. INTRODUCTION

Due to the superior electrical properties of III nitride semiconductors, lateral AlGaN/GaN Schottky-barrier diodes (SBDs) grown on LR silicon substrates are emerging as a promising device technology for fast switching speed, highpower, low-cost and compact-size communications and radar applications, such as mixers, frequency multipliers, detectors and tunable filters operating at millimeter wave frequencies [1] [2]. GaN-based SBDs with low onset voltage (V_{ON}) , high reverse-breakdown (V_{BV}) voltage, and low reverse-current leakage (I_R) , high-switching speed (R_{ON}) and high cutoff frequency (f_c) are essentially required to compete with current III-V technologies [3]. Conventional GaN-based SBD DC and RF performance is still limited to their large V_{ON} , switching loss and RF leakage when utilizing LR Si substrates. Several

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researchers have recently proposed low V_{ON} along with low I_R and high V_{BV} technologies, including recessed anode, dual-filed plates, regrowth cathodes, and dual- channel field-effect rectifier (LFER) [4] [5] [6]. However, these approaches require accurate control of anode etching to the 2DEG and a complicated fabrication process, which incorporates reliability issues and extra processing cost. Nevertheless, a 3-D SBDs integrated with a tri-gate MOS structure has shown outstanding DC characteristics at the expense of RF performance owing to the inherently large junction capacitance (C_i) and series resistance (R_S) [7]. Therefore, these techniques are only limited to low-frequency applications. To date, most of the research effort into GaN-based SBDs on silicon is predominantly focused on power electronics, with limited literature targeting RF operation. However, achieving high f_c while maintaining low I_R and superior V_{BV} remains a challenge [1].

In this letter, an optimized multi-channel RF AlGaN/GaN SBDs on LR Si structure is demonstrated using a cost-effective (GaN on LR Si) which is fully compatible with III-V THz monolithic integrated circuit (THz-MIC) technology. In contrast to conventional SBDs, the newly developed devices significantly enhanced the turn-on characteristics, switching loss, ideality factor (η_n) and f_C , where a $V_{ON} = 0.84$ V, $R_{ON} = 0.97$ Ω .mm, $V_{BV} > 30$ V, $\eta_n = 1.69$ and $f_C = 0.6$ THz were achieved. This attributes to the direct contact of Schottky anode to 2DEG at the sidewalls of the multi-mesa trenches along with proper design geometries to suppress substrate coupling effects.

II. DEVICE DESIGN AND FABRICATION

Fig. 1 indicates a cross-section of the fabricated AlGaN/GaN SBDs on LR Si using a multi-channel structure, which was simultaneously fabricated with conventional SBDs on the same substrate to allow precise comparison. A combination of multimesa and T-shaped structures was adopted to form the anode to reduce Schottky barrier height and anode resistivity, respectively. The height (H_F), width (W_F), spacing (S_F) and length (L_F) of the nanowires were ~ 50, 41, 89 nm and 2 μ m, respectively. The Anode length (L_A) and anode head length (L_{AH}) were 0.550 μ m and 1.1 μ m, respectively, whereas the junction length (L_j) was 4.28 μ m. The total physical anode

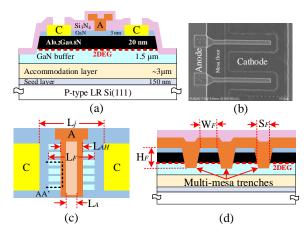


Fig. 1: (a) Cross-sectional view, (b) Scanned-electron microscope (SEM) image and (c) Top-view of the multi-channel SBDs. (d) Cross-sectional representation of the tri-anode along line AA'.

width was 2×10 µm, while the effective anode width for the fin-like anode structure was 2×5.829 µm.

The epitaxy material used in this work was grown on LR Si (111) ($\sigma = 0.02 \ \Omega.cm$) provided by Nexperia. The epilayer consists of 4.65 µm buffer, 20 nm Al_{0.2}Ga_{0.8}N barrier and 3 nm GaN cap layer. A sheet carrier density of 5.9×10^{12} cm⁻² and electron mobility of 1713 cm²/Vs are determined using Hall measurements. The device fabrication started with defining the Ti/Pt markers, followed by the deposition of Ti/Al/Ni/Au ohmic contacts and rapid thermal annealing at 790 °C in N2 environment to form the cathode. Next, a ~150 nm depth mesa isolation was performed through Cl₂/Ar-based inductivelycoupled plasma (ICP). Then, multi-mesa trenches were defined by e-beam lithography and subsequently etched using Cl₂/Arbased ICP with an etch depth of ~ 50 nm. A 100 nm Si₃N₄ passivation layer was then deposited using a low-stress inductively-coupled plasma chemical vapour deposition (ICP-CVD) at room temperature. To form the T-shaped anode, Ebeam lithography was used to define anode-foot trenches through the Si₃N₄ passivation layer using a low-damage SF₆/N₂ gas mixture reactive-ion etching (RIE), which was followed by Ni/Au metal stack evaporation to finish the T-shaped anode. Windows in the Si₃N₄ at the cathode areas were etched prior to the deposition of Ti/Au bond pads and 160 nm Si₃N₄ layer as a final passivation layer. Device fabrication was finalized by Si₃N₄ etching in the measurement pad regions. SEM image of the fabricated devices in shown in Fig.1b.

III. RESULTS AND DISCUSSION

A. DC Characteristics

Fig. 2 indicates the typical *I-V* characteristics of the fabricated conventional and multi-channel structures at room temperature using both linear and logarithm scales. The diode current (A/mm) and resistance (Ω .mm) of conventional and multi-channel structures are normalized by the total physical anode width (2 × 10 μ m) and effective anode width (2 × 5.829 μ m), respectively. Fig. 2a reveals that incorporating a multi-channel anode structure reduced V_{ON} from 1.34 to 0.84 V

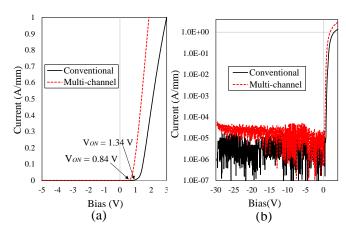


Fig. 2: *I-V* characteristics of a fabricated SBD plotted in (a) Linear and (b) Logarithm scale.

together with improved R_{ON} from 1.52 to 0.97 to Ω .mm. This attributes to the direct anode contact to the 2DEG, where the anode is wrapped around the narrow AlGaN/GaN bodies.

To further analyze these findings, the semilog I-V plot (shown in Fig. 2b) is used, which allows the extraction of η_n and ϕ_n based on the analytical equations indicated in [8]. Both device structures exhibited η_n between 1 and 2, which indicates the presence of conduction mechanism besides a thermionic emission mechanism [9]. An improvement of 14.28 % in η_n (from 1.97 to 1.69) was obtained by the developed multichannel structure as compared to conventional SBDs. Furthermore, the observed reduction in V_{ON} when using the new structure corresponds to a reduction of 17.5 % in ϕ_n (from 0.78 to 0.64 eV). However, I_R was slightly increased with the multichannel structure, where $I_R < 38 \mu A/mm$ was performed at a reverse voltage of up to 30 V. This attributes to the additional anode length where the anode is in direct contact to the GaN buffer in the multi-mesa floor regions. The achieved results are comparable to that of SBDs on semi-insulating (SI)-SiC with recessed anode and regrowth cathode technologies, with better V_{BV} and I_R [1]. This enhancement is mainly attributed to the scale of anode-to-cathode spacing and the use of T-shaped anode, owing to the reduction in peak electric field of Schottky junction [5].

B. RF Characteristics

On-wafer small-signal *S*-parameters measurements were performed in the frequency range 0.1 to 110 GHz using an Agilent PNA network analyzer (E8361A) and frequency extenders (N5260A). The system was calibrated with an offwafer calibration impedance standard substrate (ISS), using a Short-Open-Load-Thru (SOLT) calibration technique.

Fig. 3a shows the extracted small-signal circuit model of the devices, which was validated by the good agreement between modelled and measured S-parameters up to 110 GHz, as shown in Fig. 3b. This allows the extraction of SBD intrinsic elements; junction resistance (R_j), C_j and R_s , which used to determine f_c of the fabricated devices. As indicated in Fig. 3a, unlike SI-substrates, substrate parasitics (S_{sub} and R_{sub}) are incorporated into the standard SBD circuit model when considering lossy Si

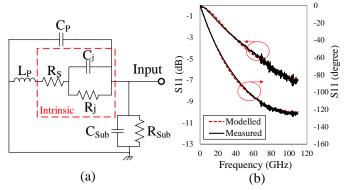


Fig. 3: (a) Schematic of the proposed small-signal equivalent circuit model and (b) measured versus modelled *S*-parameters of the fabricated multi-channel AlGaN\GaN SBDs on LR Si at 0 V bias.

Table I
EXTRACTED PARAMETERS FOR THE EQUIVALENT CIRCUIT
MODEL FOR THE FABRICATED LATERAL SBDs AT 0 V BIAS.

SBD	Intrinsic			Extrinsic			
structure	C _j (fF)	R_s (Ω)	R_j (K Ω)	L_p (pH)	C _p (fF)	C _{sub} (fF)	R _{sub} (KΩ)
Conventional	49.1	44.9	11.6	40.3	26.4	3.1	10.3
Multi-channel	46.4	51.9	11.6				

as a substrate. Furthermore, C_p and L_P represents pad parasitics. However, the external parasitic elements have a significant influence on the model at frequencies beyond 20 GHz.

Table I shows the extracted circuit element values of conventional and multi-channel structures at 0 V bias. In contrast to conventional SBDs, an increase in R_S by 15.6 % (44.9 to 51.9 Ω) and a slight reduction in C_j by 5.5 % (form 49.1 to 46.4 fF) were observed for the newly developed fin-type technology. This attributes to the additional anode length in the multi-mesa trenches and reduction in ϕ_n , respectively. In addition, the low value of C_{sub} and high value of R_{sub} indicates that substrate coupling effect could be neglected in both design structures. This was a result of the proper design geometries where the anode-to-cathode separation (2.415 μ m) is less than the buffer thickness (4.65 μ m) [10].

The extracted values of C_j as a function of the applied voltage of the fabricated devices are shown in Fig. 4a. It can be seen that C_j was inversely proportional to the applied reverse voltage, where a sharp drop in C_j was obtained when changing the voltage form 0 to -2 V. Furthermore, owing to the direct anode contact to 2DEG for multi-channel SBDs, C_j was significantly reduced at reverse biases beyond -2 V, as compared to conventional SBDs. This reflected a dramatic enhancement in f_C which can be calculated from R_s and C_j [1]. Therefore, f_C was improved by 32.7 % (from 0.457 to 0.607 THz), as shown in Fig. 4.b. However, the achieved f_C of the fabricated lateral SBDs on LR Si is still limited to their larger R_s , which mainly depends on material growth quality and cathode contact resistivity, as compared to SBDs realized on GaN-on-SI-SiC substrates [1].

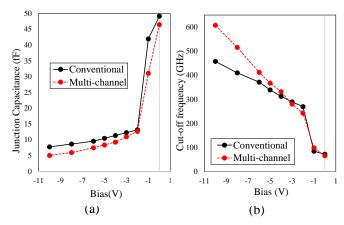


Fig. 4: Junction capacitance (C_i) versus voltage, and (b) Cut-off frequency (f_c) versus voltage of the fabricated conventional and multi-channel SBDs.

IV. CONCLUSION

A newly developed multi-channel RF lateral AlGaN/GaN SBD on LR Si technology has been realized in this work. A V_{ON} of 0.84 V along with R_{ON} of 0.97 Ω .mm and η_n of 1.69 were achieved as a result of the direct Schottky anode contact to the 2DEG resulting in a ϕ_n of 0.64 eV. The fabricated devices exhibited V_{BV} of greater than 30 V along with I_R of less than 38 μ m/mm. In addition, a newly proposed small-signal circuit model was introduced up to 110 GHz. An f_c of 0.6 THz at a reverse bias of -10 V was achieved as a result of the optimized SBD design structure and geometries. These findings enable an effective pathway for the realization of high-performance sub-THz-MIC topologies.

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