THE DEVELOPMENT AND TESTING OF AN CH₄/NH₃/H₂ COMBUSTION SYSTEM FOR A 50KW MICRO GAS TURBINE

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1. INTRODUCTION

- In an effort to target lower global warming emissions, carbon-free fuels are a cheap, long-term energy storage solution.
- Ammonia-hydrogen fuel blends are a good compromise for combustion characteristics and storage/transportation costs, and may be blended with methane to aid the transition to a carbon-free economy.
- This study outlines the emissions challenges in the utilisation of an industrial scale swirl burner for CH₄/ NH_2/H_2 blends.
- To address these challenges, a novel combustor design has been proposed for the conversion of a 50kW APU.

First, a study was carried out for an industrial scale, axial swirl burner, not optimised for ammonia-based fuels. Power = 8kW, Inlet Temp. = 293KInlet Pressure = 1 atm, Swirl number, $S_{a}=0.8$

cross-section plane

flashback protector -

 $NH_3/CH_4/air inlet$

Figure 1 - Schematic of swirl burner in baseline studies

4. DESIGN OF THE NIK15 BURNER

A novel burner design (NIK15) optimised for these fuel mixtures has been proposed. LDA (Laser Doppler anemomentry) were used for validation of a RANS CFD model.





• NIK15 burner was designed for improved mixing, such as to reduce NOx production, such as through the conversion of NO to N₂ by the thermal deNOx reactions

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2. METHODOLOGY





3. EMISSIONS ANALYSES OF AN AXIAL SWIRL BURNER NH* NH_2^* CH* OH* 16,000 10,000 8,000 6,000 CN(B-X) CH(A-X) (0,0) (1,1) (0,0) OH(A-X) (0,0) (1,1) (0,0) (1,1) 4,000 CN(B-X) CN(B-X) 2,000 NO(A-X Figure 3 - Spectrometry analysis at burner base, $\Phi = 1.2$ (fuel blends as for Figure 2) 0 (mm) 45 8 0.7 post-processing ($\Phi = 1.2$) 0.3 No 100 ["]HN 0.2 Figure 4 - Emissions at outlet, $\Phi = 1.2$ (fuel blends as for Figure 2) No Name • NH* and NH₂* trends were reversed, based on CH₄ content in the Pre-swirl vane Fixed diffuser ring fuel blend, as shown in Fig. 2. Annular reverse flow Turbine rotor • Fig. 3 gives the relative magnitude of intermediary species at the Power turbine inlet nozzle flame centre. OH, NH, CN and CH was dominant in the high CH, Exhaust ducting content fuels with NH₂ having had the highest signal in NH₃ fuels. • NO was the primary contributor of NOx emissions, with lower CH content flames having lower emissions. 6. CONCLUSION • Swirl burner emissions for $NH_3/H_2/CH_4$ blends were studied. • LDA validated CFD defined hydrodynamic behaviour of the NIK15 burner design, with plans for future combustion studies. • Prototype APU combustor designs are under development to accommodate the new design. 7. ACKNOWLEDGEMENTS This work was supported by funding from the EPSRC SAFE project (EP/T009314/1). The authors also thank Mr Malcolm Seaborne for his expertise and development of the experimental facilities used in

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40/40/20 (vol.%) $CH_4/NH_3/H_2$ 30/50/20 (vol.%) $CH_4/NH_3/H_2$ 20/55/25 (vol.%) $CH_4/NH_3/H_2$ 10/65/25 (vol.%) CH₄/NH₃/H₂ 0/70/30 (vol.%) $CH_4/NH_3/H_2$ Figure 2 - Chemiluminescence with Abel deconvolution 5. RETROFITTING OF THE APU Conversion of a Rover MK10501 APU to produce 50kW power from ammonia/hydrogen/methane fuel blends is in progress. Considerations have been made for controls (through LabVIEW) and diagnostic measurement. Figure 7 - Rover MK10501 Schematic aptation of the combustor for a rich-quench-lean configuration with stratified injection, utilising the new NIK15 burn-



The new design considers ader design.



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Figure 8 - Prototype combustor design

