

MICROMECHANICS-DRIVEN VARIATIONAL METHOD FOR DIFFUSE-TO-LOCALISED FRACTURE IN QUASI-BRITTLE SOLIDS

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Abstract. A novel multiscale variational method for modelling fracture propagation is proposed. The method employs strong discontinuity kinematics enhancement, enabling macroscopic cracks to be modelled explicitly, while minimum remeshing is ensured. In addition, the response of quadrature points in the bulk is up-scaled using a Micromechanical continua, which enables the evolution of directional micro-defects (e.g. microcracks) without venturing into prohibitive computational burden. Noticeably, the method allows the Micromechanical continua to interact with macroscopic cracks. The framework is conveniently formulated as a variational setting to provide a minimum energy solution. The new computational framework has been found to diagnose realistic failure mechanisms in quasi-brittle materials.

1 INTRODUCTION

Multiscale homogenisation is resurgent in Computational Mechanics [1], and opens the door to enhance our understanding of materials. Benefits of multiscale modelling are noticeable, when conventional inelasticity frameworks cannot reproduce the response of heterogeneous materials and structures with the required accuracy needed. Taking into account the intrinsic microstructure of materials by direct numerical simulation (DNS) is often computationally prohibitive. On the other hand, computational homogenisation, referred to as global-local analysis [2], can also become computationally demanding [3]. Therefore, there is a need for proposing efficient homogenisation strategies.

Moreover, an adequate or definitive treatment for damage to actual fracture occurrence across scales yet remains as an unresolved dilemma in Multiscale modelling [4]. Although other methods exist for macroscopic fracture, e.g. micropolar continua [5, 6], gradient-enhanced continua [7, 8], phase-field methods for (quasi-) brittle fracture [9, 10], among others, connection with the evolving microstructure is somewhat hidden in numerical length-scale parameters. Seeking a rigorous micromechanistic basis to macrocracking is appealing. This paper tackles two challenges in Multiscale modelling: (i) reduction of computational cost, e.g. by using diffuse approximations for RVE-based microstructural evolution, and (ii) energetically-consistent treatment of diffuse-micro and localised-macro fracture seamlessly.

The remainder of the paper is divided into six additional sections: **Section 2** explains a least-energy approach for multiscale modelling of inelasticity and fracture; **Section 3** describes homogenisation principles at the RVE level; **Section 4** expands on micro to macrocracking transition; **Section 5** describes the response of sharp macrocracks; **Section 6** shows some numerical results; and **Section 7** concludes.

2 A NEW (LEAST-ENERGY) VARIATIONAL APPROACH TO MICRO-MACRO FRACTURE

A new variationally consistent method is proposed for modelling the transition from diffuse microcracking to localised fracture in quasi-brittle solids. The method relies on energy minimisation principles, imposed on a multiscale weak form for solids with embedded discontinuities (see figure 2). The reader may refer to [11, 12, 13] for reference on theoretical perspectives for non-linear solids with embedded discontinuities:

$$\downarrow \text{Downscaling}, \uparrow \text{Upscaling: } \delta\Pi = \text{minimise} \left\{ \int_{\Omega} (\delta\boldsymbol{\varepsilon} : \langle \boldsymbol{\sigma} \rangle_{RVE}) d\Omega + \int_{\partial\Gamma^M} (\delta[[\mathbf{u}]] \cdot \mathbf{t}_{\Gamma^M}) d\Gamma \right\} \quad (1)$$

$$\boldsymbol{\varepsilon} \equiv (\nabla \mathbf{u}_c)^s = (\nabla(\mathbf{u}_c + \mathcal{H}_{\Gamma^M} \otimes [[\mathbf{u}]])^s \quad (2)$$

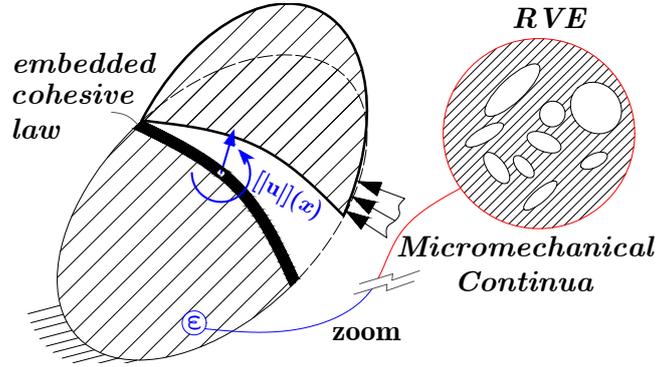


Figure 1: Fracture kinematics: strong discontinuities follow a cohesive response with characteristic *smooth* unloading/reloading (SUR) traction-separation law. For reference on SUR response see [14].

3 MICROMECHANICAL CONTINUA

The response of the micromechanical continua is non-linear, and is subjected to the evolution of directional microdefects (e.g. microcracks). Incorporating Eshelby's ellipsoidal micro-voids in a diffuse fashion [15], at various sets of preferential microcracking zones at the RVE level, and employment of volume-averaging rules of RVE-based energy variation (Hill-Mandel condition [16]), yields the following *effective* constitutive relation:

$$\boldsymbol{\varepsilon} = \langle \boldsymbol{\varepsilon} \rangle_{RVE} = D_e^{-1} : \langle \boldsymbol{\sigma} \rangle_{RVE} + \frac{1}{2\pi} \int_{2\pi} \int_{\pi/2} \mathbf{N}_{\boldsymbol{\varepsilon}}^{-1}(\boldsymbol{\psi}, \boldsymbol{\theta}) : \boldsymbol{\varepsilon}_{\alpha}^{\Gamma_m} \sin(\boldsymbol{\psi}) d\boldsymbol{\psi} d\boldsymbol{\theta} \quad (3)$$

$$\boldsymbol{\varepsilon}_{\alpha}^{\Gamma_m}(\boldsymbol{\varepsilon}, \langle \boldsymbol{\sigma} \rangle_{RVE}) = \mathcal{N}_{\alpha} \int_{\partial\Gamma_m} (r_{\alpha} \otimes [\mathbf{u}^{\partial\Gamma_m}])^s dS, \quad \forall x' \in \partial\Omega_{\alpha}^m \quad (4)$$

Remarks: (i) The evolution of microcrack density in every set of degradation micro-zones is linked conveniently to the average strain history of the RVE, in an implicit computing flow; (ii) Numerical homogenisation, as adopted in this paper, avoids the use of *physical* domains as RVEs, and exploits energetic principles to track diffuse material degradation at the Micromechanical continuum; (iii) Macrocrack degrees of freedom are condensated at the element level, while micro- and macrocracks interact.

4 MACROCRACK DETECTION UPON MICROCRACKS COALESCENCE

Upon substantial microcracking growth, macroscopic fracture is enabled. In this case, the Micromechanical continua dictates the propagation direction of macroscopic sharp cracks. New macrocracks are allowed to rotate until a critical iteration number **itfix** is reached. A computational flow is shown below:

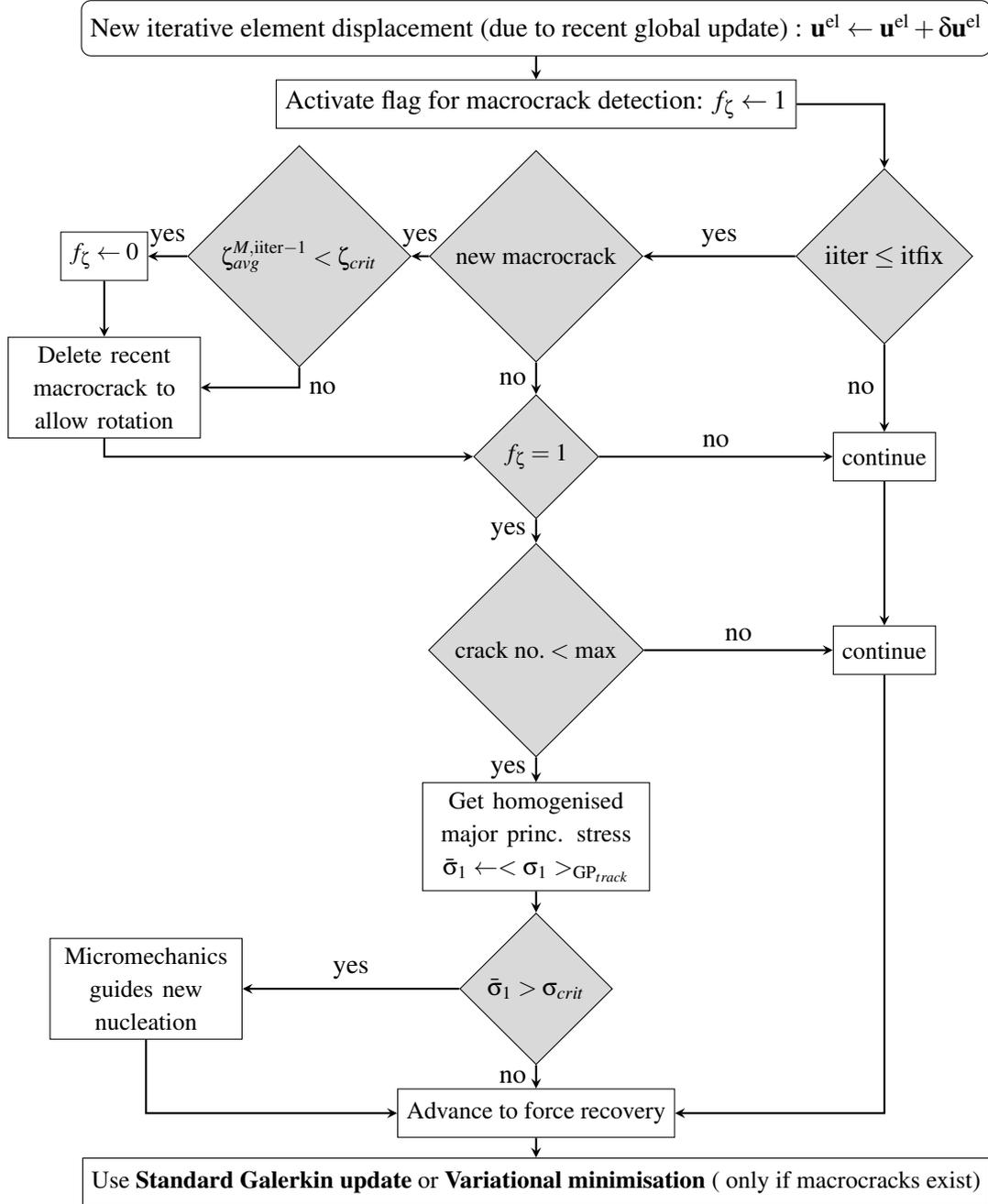


Figure 2: Flow chart - Nucleation criteria is based upon crack aperture and Micromechanical stress.

In addition, new forming macrocracks can be omitted in a near future iteration if the macrocrack average aperture (an equivalent aperture can be used for mixed mode cracks) is smaller than a critical value. This constraint has been found to conveniently delay the release of macrocracks, in such a manner that a smooth transition from micro to macro fracture is obtained in the load-displacement space. A few options are possible to adjust the transition from microcracking dominated phenomena to fully developed macroscopic fracture, although these will be discussed later in the form of a journal publication.

5 EMBEDDED COHESIVE MODEL FOR SHARP MACROCRACKS

A simple traction-separation law is used upon macrocrack detection within a localised macrocrack band of defined virtual thickness h_{ca} . It is highlighted that there is no geometric thickness of the macrocrack band in the finite element setting. A single degradation macro-state variable ζ^M , with units of length, dominates the response at each integration point of the localised macrocrack band. A dimensionless degradation scalar-variable ω^M is defined using a Smooth Unloading Reloading (SUR) approach. Such approach benefits the numerical scheme by ensuring positive tangents upon fixation of macrocracks within the global incremental iterative procedure. The (local) traction separation-law follows the expression shown below :

$$\mathbf{t}'_{\Gamma^M}(x') = \frac{1 - \omega^M(x')}{h_{ca}} \begin{bmatrix} E & 0 \\ 0 & E/(2(1+\nu)) \end{bmatrix} \Delta \mathbf{u}(x'), \quad \forall x' \in \partial \Gamma^M \quad (5)$$

The work-conjugated equivalent force vector for the embedded cohesive model reads as follows:

$$\mathbf{F}_{ck}(x') = \frac{1}{h_{ca}} \begin{bmatrix} \int_{\Gamma}(1 - \omega^M)Et_g dl & 0 & \int_{\Gamma}(1 - \omega^M)El t_g dl \\ 0 & \int_{\Gamma}(1 - \omega^M)Gt_g dl & 0 \\ \int_{\Gamma}(1 - \omega^M)El t_g dl & 0 & \int_{\Gamma}(1 - \omega^M)El^2 t_g dl \end{bmatrix} \mathbf{W}, \quad \forall x' \in \partial \Gamma^M \quad (6)$$

6 REPRESENTATIVE NUMERICAL EXAMPLE

6.1 Four-point bending test

A typical four-point bending setup is simulated using the new proposed framework. The main span of the beam specimen is pushed at two contact points, located at a distance of $L/3$ from each support axis, with L being the main span length. For details on element level performance the reader may see [17].

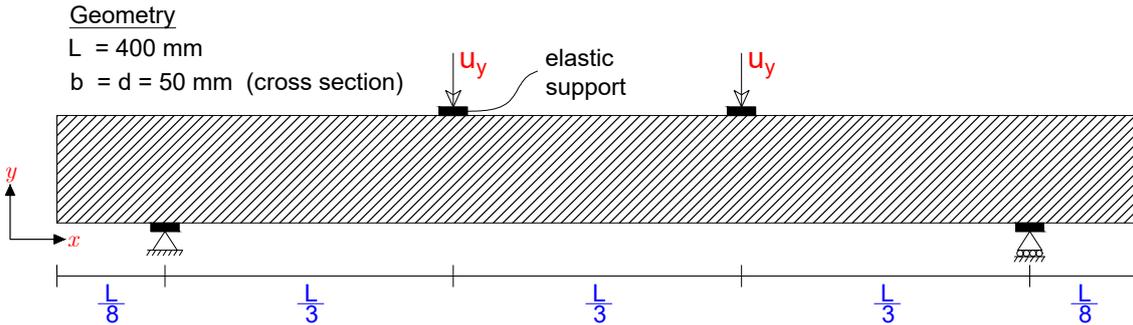


Figure 3: Four point bending test on concrete. Geometry and boundary conditions as shown in illustration. Elastic supports possess equivalent elastic properties as the aggregate-matrix mixture.

Elastic properties of the aggregate-cement matrix mixture follow standard concrete parameters: overall Young's modulus $E = 30$ GPa and $\nu = 0.2$. Numerical results are shown below:

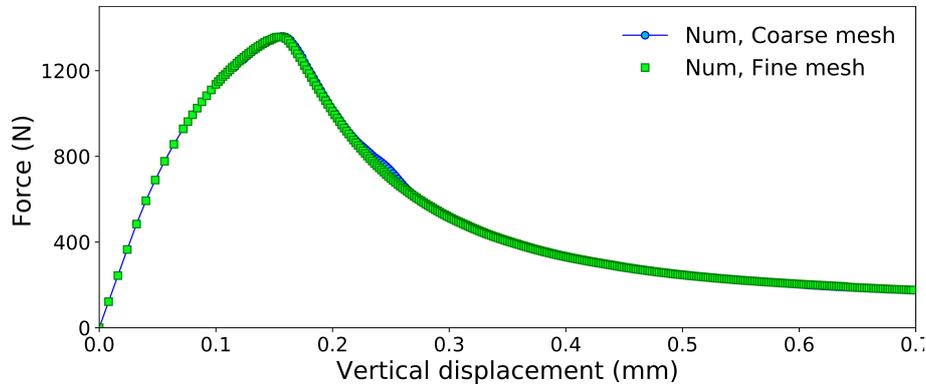
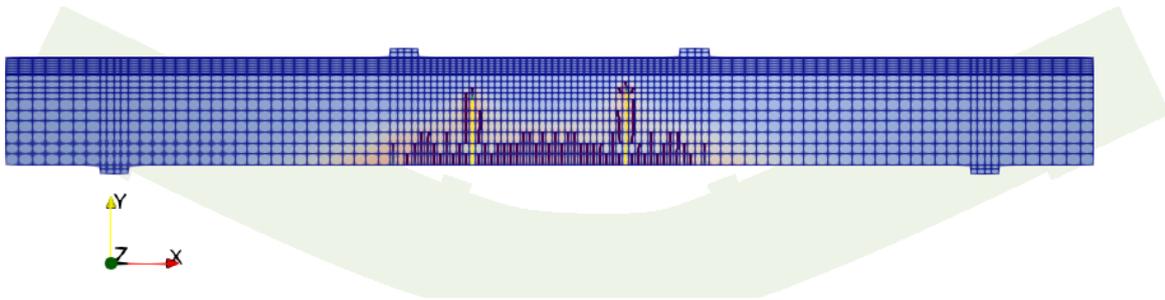


Figure 4: Load-displacement predictions for four-point bending test on concrete.

(a) Coarse mesh (4488 dofs): failure patterns and deformed geometry (shaded background), at $u_y = 0.2mm$.



(b) Fine mesh (7644 dofs): failure patterns and deformed geometry (shaded background), at $u_y = 0.2mm$.

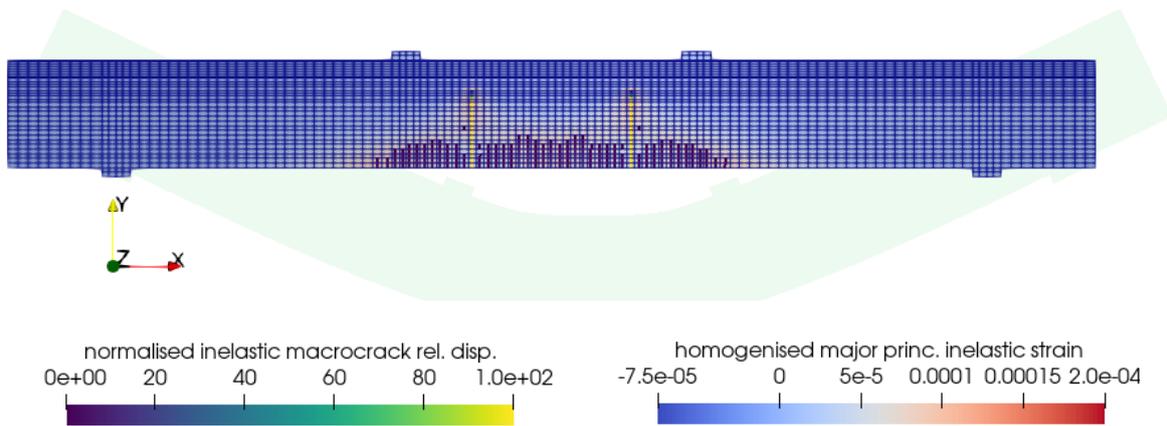


Figure 5: Predictions of failure mechanisms in four-point bending test. Colour-bars indicate inelastic components of (major principal) homogenised strain and normalised macrocrack relative displacement.

7 CONCLUSIONS

A new Multiscale variationally consistent method for modelling fracture, that provides a least-energy solution, is proposed. Distinctive findings read as follows:

- The method is efficient, given that : (i) RVEs are conveniently approximated by a Micromechanical continua; and (ii) macrocracking dofs are condensed at element level.
- The method adequately captures the interaction among diffuse-micro and localised-macro fractures during the onset of material instabilities.
- The method has shown promise in the diagnosis of failure in quasi-brittle materials.

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