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# Kinetics of Gas Phase CO<sub>2</sub> Adsorption on Bituminous Coal from a Shallow Coal Seam

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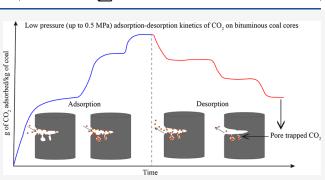




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**ABSTRACT:** This article examines the  $CO_2$  adsorption-desorption kinetics of bituminous coal under low pressure injection (0.5 MPa) in the context of  $CO_2$  sequestration in shallow level coal seams. This study used two different sizes of intact core samples of bituminous samples from seam no. 30 at the Experimental Mine Barbara (EMB) in Katowice, Poland. Manometric adsorption kinetics experiments were conducted on 50 mm dia. 60 mm long coal core samples (referred to as EMB1) and 50 mm dia. 30 mm long coal core samples (referred to as EMB1). The kinetics of adsorption at injection pressures ranging from 0.1 to 0.5 MPa were compared to those at elevated pressures ranging from 0.5 to 4.5 MPa. For the first time, intact sample adsorption-desorption data

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were fitted in pseudo first order (PFO), pseudo second order (PSO), and Bangham pore diffusion models. The PSO model fits the data better than the PFO model, indicating that bulk pore diffusion, surface interaction, and multilayer adsorption are the rate-determining steps. Comparing the equilibrium amount of adsorbed ( $q_e$ ) obtained for the powdered samples (9.06 g of CO<sub>2</sub>/kg of coal at 0.52 MPa) with intact samples (11.68 g/kg at 0.53 MPa and 7.58 g/kg at 0.52 MPa for the intact EMB1 and EMB2 samples) showed the importance of conducting experiments with intact samples. The better fit obtained with the Bangham model for lower pressure equilibrium pressures (up to 0.5 MPa) compared to higher pressure equilibrium pressures (4.5 MPa) indicates that bulk pore diffusion is the rate-determining step at lower pressures and surface interaction takes over at higher pressures. The amount of CO<sub>2</sub> trapped within the coal structure following the desorption experiments strengthens the case for intact bituminous coal samples' pore trapping capabilities.

# 1. INTRODUCTION

 $\rm CO_2$ , along with other greenhouse gases, is the primary contributor to global warming. Accumulative emissions of  $\rm CO_2$ are estimated to be 2035  $\pm$  205 Gt of  $\rm CO_2$  and increasing at the current emission rate of 40 Gt  $\rm CO_2/year.^{1,2}$  Carbon capture and sequestration (CCS) in geological media is viewed as a promising option for limiting the adverse effects of climate change. Deep saline aquifer sequestration, mineralization with rocks, and coal seam sequestration all seem to be viable options for carbon sequestering. Countries were urged to speed up the phaseout of coal use by 2030 in order to limit the temperature increase <1.5 °C preferably by the end of the century.<sup>3-6</sup> CCS in coal might be a practical option for the effective use of un-mineable coal seams.<sup>7</sup>

Coal is a fractured and porous structured carbonous material found in different ranks such as lignite, subbituminous, bituminous, and anthracite depending on the coalification process. The coal's ability to adsorb gas demonstrates its applicability for CCS operations. Adsorption of methane in coal seams is facilitated by the high surface area and porous nature of the coal.<sup>8,9</sup> According to studies, the coal surface has

a stronger affinity for  $\mathrm{CO}_2$  than that for  $\mathrm{CH}_{4}$ , especially in bituminous coal samples.  $^{10-14}$ 

 $CO_2$  trapping in coal is influenced by several factors, including sequestration capacity, gas permeability/injectivity, pressure, temperature, coal swelling behavior, confinement pressure, moisture content, and depth.<sup>9,15,16</sup> According to the gas physical adsorption phenomenon, increasing the equilibrium pressure increased the  $CO_2$  adsorption capacity of coal. The sorption isotherm, on the other hand, showed decreasing trends at pressures near and above the critical pressures (7.38 MPa at a temperature of 304.1 K).<sup>17–21</sup> Typically, the reported adsorption capacity increased with the decrease in temperature,<sup>22</sup> and the majority of the current literature reported the adsorption isotherm obtained at higher temperatures (308.15,

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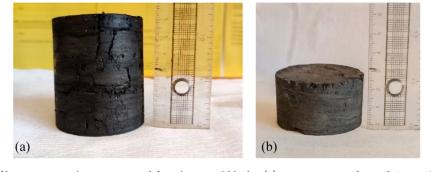


Figure 1. Core samples of bituminous coal cores extracted from large coal blocks. (a) EMB1: 50 mm dia. and 60 mm length, (b) EMB2: 50 mm dia. and 30 mm length.

318.15, 328.15, and 377.15 K).<sup>23,24</sup> However, there is very limited for the  $CO_2$  adsorption on coal at lower temperatures (298.15 and 290.15 K).<sup>25,26</sup>

In general, coal seam depths of less than 1000 m are preferred for  $CO_2$  sequestration. Deeper than 1000 m, the confining pressure may affect coal permeability, eventually reducing the injectivity and  $CO_2$  adsorption capacity.<sup>27</sup> Shallower than 1000 m depth, where the temperature and pressure are expected to be less than the critical parameters of  $CO_2$  (31 °C and 7.38 MPa). The subcritical temperature and pressure adsorption behavior of  $CO_2$  is currently understood to a lesser extent.<sup>7</sup> Most studies have used powdered coal specimens to study adsorption capacity and kinetics, with very limited data on intact samples.<sup>28,29</sup> To understand the  $CO_2$  trapping capabilities of bituminous coal at subcritical pressure adsorption–desorption experimental studies on large intact samples.

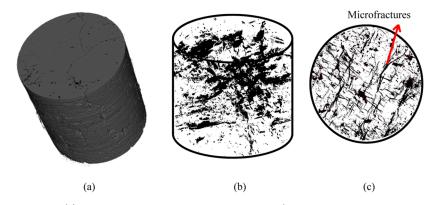
The CO<sub>2</sub> adsorption capacity of coal is correlated to its swelling behavior, and matrix swelling creates a pathway for CO<sub>2</sub> to permeate the coal's microfractures and nanopores.<sup>25</sup> The reversibility of trapped  $CO_2$  in the pores is critical for estimating the coal seam's residual CO<sub>2</sub> retaining capacity. This parameter can be determined by examining the adsorption-desorption kinetics and hysteresis patterns. As such, a positive deviation in the hysteresis indicates that the adsorbate gas is not readily released to its equilibrium pressure and temperature values.<sup>22</sup> The kinetics of CO<sub>2</sub> desorption from coal has received less attention. Until now, it has been reported that a large proportion of CO<sub>2</sub> gas molecules are trapped in the structure of bituminous coal during the desorption process.<sup>10</sup> Previously, manometric experimental setups were used to examine the CO<sub>2</sub> adsorption kinetics of powdered samples of bituminous and anthracite coal at 35, 45, and 55 °C, as well as pressures up to 25 MPa.<sup>23</sup> Similarly, the spontaneity of CO<sub>2</sub> reversibility from the coal's nanopores can be explored by conducting adsorption-desorption kinetics studies with an intact specimen of porous bituminous coal under subcritical  $CO_2$  conditions.

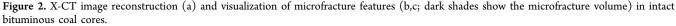
The pseudo-first-order (PFO) kinetic model and pseudosecond-order (PSO) kinetics have been widely applied for predicting the gas phase adsorption of  $CO_2$  on coal.<sup>30–34</sup> The equilibrium amount of  $CO_2$  adsorbed on an intact bituminous coal specimen obtained using the manometric method at pressure ranges up to 5 MPa and temperatures of 298.15, 308.15, and 318.15 K were shown to be in good agreement with the PSO model.<sup>35</sup> The rate-determining factor of adsorption was determined as the pore diffusion/condensation of  $CO_2$ . The PSO model assumes that the  $CO_2$  adsorption on bituminous coal is dominated by surface interaction and bulk diffusion.<sup>30</sup> Nevertheless, the desorption kinetics of the intact specimen holds the key information on the rate-determining factor and most important to know the residual amount of  $CO_2$  remaining in the coal seam. Bangham and Burt (1924, 2002)<sup>36,37</sup> successfully applied a kinetic model from the  $CO_2$ adsorption experiments conducted on glass and Bangham and Sever (1925)<sup>38</sup> extended the pore diffusion model to the van der Waals adsorption of gases, which were well fitted with the model. Probing the rate-determining steps at low pressure injection would highlight the prominent adsorption mechanisms at low pressure injection at shallow depth coal seams.

From the current understanding, the limitation of available desorption kinetic data from the large bituminous sample at subcritical  $CO_2$  conditions, investigation needs to be carried out to substantiate the candidature of shallow level coal seams as CCS reservoirs. Moreover, the gas phase adsorption of  $CO_2$ at low injection pressure, reversibility, and residual CO2 retained in the pores are the crucial information for shallow level sequestration, which has been less understood. Especially, the experimental studies<sup>39</sup> conducted in the subcritical range showed very limited data representing the pressure range below 0.5 MPa to ascertain the  $CO_2$  behavior at these pressure ranges. A large number of studies have been conducted at the supercritical pressure range aiming to inject CO<sub>2</sub> in coal seams located below 1000 m assuming that environmentally safe,  $CO_2$  can be stored at higher volume at high density. However, laboratory conditions cannot be replicated in the field and  $CO_2$ can escape to different pressure and temperature regions in the ground. Moreover the higher confining pressure at deeper coal seams would affect the injectivity of CO2. 40,41 Therefore, the current study attempted a detailed adsorption-desorption kinetic study of gas phase adsorption for shallow level injection. The shallow level of CO2 storage required low pressure injection of gas phase CO<sub>2</sub> owing to the low confining pressures. The present study demonstrates the experimentally observed adsorption-desorption kinetics of CO<sub>2</sub> adsorption on large cores of bituminous coal samples at low pressure injections (less than 0.5 MPa) and at a temperature of 298.15 K obtained using a manometric adsorption apparatus. The data were fitted into PFO, PSO, and Bangham models to predict the rate-determining factors of adsorption and desorption processes.

#### 2. MATERIALS AND METHODS

The bituminous coal specimens have been procured from the "seam-310" located at 30 m depth in Experimental Mine Barbara (hereafter referred to as EMB), at the Central Mining Institute, Katowice,





Poland. A core drilling machine with a drilling bit with a diamond saw tip (50 mm internal diameter) was employed to extract core samples of 50 mm dia. 60 mm length (referred to as EMB1) and 50 mm dia. 30 mm length samples (referred to as EMB2) (Figure 1). Ground pulverized coal was passed through a 63  $\mu$ m mesh to obtain powdered coal samples.

The large-sized adsorbent was characterized for its microfracture network using X-ray computed tomography (X-CT) (Figure 2). The scans were used to quantify the microfractures and not the pores. The microfractures are separated from the matrix, and the volume of these flow paths (connected and unconnected fracture network) is quantified to compare with the He-pycnometry method. The images of the physical structure of the coal core adsorbent showed the unconnected fracture network volume which will become available to CO<sub>2</sub> owing to the swelling behavior of bituminous coal as described in previous studies.<sup>42–45</sup> The connected and unconnected void volume was about 1.5% of the bulk sample. Even though the volume was a negligible addition to the adsorption cell void volume ( $v_{di}$  see Section 2.1), the  $v_d$  was adjusted with the excess volume measured by X-CT to calculate the molar volume of the adsorbed phase.

Proximate and ultimate analysis of EMB coal showed a moisture content of 7.54 and 6.39%, respectively, for the "as received" and "analytical" samples. The carbon content is 71.5% (approx.), the maximum ash content is 15.56%, and the vitrinite's reflectance is  $0.57 \pm 0.03\%$ . The coal is classified as low rank bituminous coal. Table 1 summarizes the properties of the coal samples.

2.1. Measurement of  $CO_2$  Adsorption Kinetics by Manometric/Volumetric Method. A manometric gas adsorption cell was employed to determine the  $CO_2$  adsorption capacity of the core samples. The schematic of the apparatus and experimental setup is presented in Figure 3. The apparatus was designed and installed by GDS Instruments UK. A detailed description of the experimental setup is available at Mosleh (2014).<sup>46</sup>

To measure CO<sub>2</sub> adsorption in a manometric cell, a known amount of gas  $(n_i^{CO_2})$  is injected into the reference cell (RC) and expanded into the sample cell (SC), which contains a coal sample that is degassed prior to the test using a vacuum pump attached to the adsorption cell (each sample was degassed for 24 h) (Figure 3). The amount of gas  $(n_i^{CO_2})$  injected in the RC was calculated using the perfect gas law (eq 1) by precisely measuring the available volume for gas  $(v_{\rm rc})$  in the adsorption cell, pressure (p), and temperature (T). The volumes of adsorption cells were measured using the Hepycnometry method.<sup>47</sup> The pressure was measured using two pressure transducers connected to RC and SC (Figure 3). With time, the CO<sub>2</sub> gas pressure injected in the adsorption cell reduces because the gas molecules continue to adsorb on the adsorbents (coal). At a given time (t), the difference between the amount injected  $(n_i^{CO_2})$  and the amount remaining in the gas phase  $(n_{\rm e}^{\rm CO_2})$  is recorded as the amount of  $\rm CO_2$  adsorbed or desorbed  $(q_{t,\rm ad}^{\rm CO_2})$  on the coal specimens. Once the equilibrium is attained, the pressure in the RC is progressively

Table 1. Proximate and	Ultimate	Analysis	of the	EMB	Coal
Specimen <sup>a</sup>					

parameter	value
As Received	
moisture (%)	7.54
ash (%)	15.56
S total (%)	0.51
calorific value (kJ/kg)	21 708
Analytical	
moisture W <sup>a</sup> (%)	6.39
ash Aª (%)	16.52
volatile matter V <sup>a</sup> (%)	33.94
calorific value Aª (kJ/kg)	23 019
C <sup>a</sup> (%)	71.5
H <sup>a</sup> (%)	3.70
$N^{a}$ (%)	0.87
S <sup>a</sup> total (%)	0.54
S <sub>c</sub> <sup>a</sup> (%)	0.54
O <sup>a</sup> (%)	14.03
vitrinite reflectance	$0.57 \pm 0.03\%$
<sup><i>a</i></sup> Oxygen calculated as follows: $(O^a) = 100$ $(H^a) - (S^a) - (N^a) \%$	$-(W^{a}) - (A^{a}) - (C^{a}) -$

 $(H^{a}) - (S_{c}^{a}) - (N^{a}) \%.$ 

Needle valve

RC Reference cell

SC Sample cell

🔘 Vacuum pump

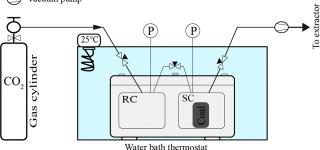


Figure 3. Schematic of the manometric gas adsorption cell and experimental setup.

increased for the next pressure step up stages (the pressure ranges are given in Table 2), and the aforementioned procedures are repeated to calculate the cumulative amount of adsorbed  $CO_2$  corresponding to the thermodynamic equilibrium pressure at a given time. After completing the adsorption test steps, pressure in the RC is progressively reduced and the amount of desorbed  $CO_2$  is determined. In this experiment, the pressure values were recorded

Table 2. CO<sub>2</sub> Adsorption–Desorption Experimental Program

experiment no.	sample	conditions	tests
EXP1	EMB1: 50 mm dia. × 60 mm length	0.5–4 MPa, 298 K	CO <sub>2</sub> adsorption
		3.6–0.085 MPa, 298 K	CO <sub>2</sub> desorption
EXP2		0.1–0.5 MPa, 298 K	CO <sub>2</sub> adsorption
		0.41–0.041 MPa	CO <sub>2</sub> desorption
EXP3	EMB2: 50 mm dia. × 30 mm length	0.1–0.4 MPa, 298 K	CO <sub>2</sub> adsorption
		0.37–0.38 MPa	CO <sub>2</sub> desorption
EXP4	powder (<63 $\mu$ m)	0.1–0.5 MPa	CO <sub>2</sub> adsorption

every 10 s using a data logger. The equilibrium pressure was defined as a pressure value that remained steady for at least 4 h. The selected data points were used for calculating the adsorbed amount of CO<sub>2</sub> ( $q_{t,\mathrm{ad/de}}^{\mathrm{CO}_2}$ ) at a time (t) during adsorption or desorption by employing the following equations<sup>48-52</sup>

$$n_{i}^{CO_{2}} = \frac{p^{CO_{2}}Mv_{rc}}{RTZ_{(p,v)}}; \quad n_{t}^{CO_{2}} = \frac{p_{eq}^{CO_{2}}Mv_{d}}{RTZ_{(p,v)}}$$
(1)

$$q_{t,\text{ad}}^{\text{CO}_2} = \frac{n_t^{\text{CO}_2} - n_i^{\text{CO}_2}}{m_s} \qquad \text{amount adsorbed during adsorption}$$
(2)

$$q_{t,de}^{CO_2} = \frac{n_i^{CO_2} - n_t^{CO_2}}{m_s}$$
 amount adsorbed during desorption (3)

where  $q_{t,ad/de}^{CO_2}$  is the mass of CO<sub>2</sub> adsorbed on coal (g of CO<sub>2</sub>/kg of coal) at time t during adsorption or desorption;  $p_{eq}^{CO_2}$  is the equilibrium pressure of CO<sub>2</sub> (Pa); *R* is the universal gas constant (*R* = 8.314 Pa·m<sup>3</sup>/K/mol); and *M* is the molar mass of CO<sub>2</sub> (*M* = 44.01 g/mol).  $v_d$  is the void volume available for gas (m<sup>3</sup>), the available void volume for gas (V<sub>d</sub>) in the RC and SC is approximated by He-pycnometry method,<sup>47</sup> *Z* is the compressibility factor of CO<sub>2</sub> which is calculated using cubic form of Peng–Robinson equation of state,<sup>53</sup>  $n_i^{CO_2}$  is the known amount present in the gas phase at beginning of the adsorption experiment (g of CO<sub>2</sub>), and  $n_t^{CO_2}$  is the amount of CO<sub>2</sub> at the gas phase at time *t*.

Adsorption experiments were conducted using two different sizes of EMB coal core samples, 50 mm dia. 60 mm length (referred to as EMB1; Table 2) and 50 mm dia. 30 mm length (referred to as EMB2; Table 2) samples, at an injection pressure range of 0.1-0.5 MPa. The experiments were termed EXP2 and EXP3 for EMB1 and EMB2, respectively. The pressure range was chosen to comprehend the adsorption process of CO<sub>2</sub> injection at a low pressure in a shallow level coal seam with low confining stresses (an approximate vertical stress of 0.51-0.7 MPa is expected at 30 m depth). One sample with a 50 mm dia. 60 mm length (EMB1) was tested at an intermediate pressure range of 0.5-4.5 MPa (termed as EXP1; Table 2) to compare the kinetics of the adsorption process at elevated pressure range in the subcritical range. The adsorption kinetics process of the large cores was compared with a powdered sample (termed as EXP4; Table 2). The experimental conditions are outlined in Table 2.

**2.2. Kinetic Models.** Adsorption kinetics data acquired from the experiments were fitted into the PFO and PSO rate eqs 4 and 5 to ascertain the rate-determining steps in  $CO_2$  adsorption on EMB coal.<sup>54,55</sup>

PFO: 
$$q_t = q_e (1 - e^{-k_{al}t})$$
 (4)

PSO: 
$$q_t = \frac{t}{\frac{1}{q_e}t + \frac{1}{k_{a2}q_e^2}}$$
 (5)

where  $q_t$  = mass adsorbed per mass of adsorbent at time t (g of CO<sub>2</sub>/kg of coal),  $q_e$  = mass adsorbed per mass of adsorbent at equilibrium, g of CO<sub>2</sub>/kg of coal,  $k_{a1}$  = first-order rate constant for adsorption,  $h^{-1}$ , and  $k_{a2}$  = second-order rate constants for adsorption, kg/g h.

The PFO and PSO models have not so far been modeled for the desorption kinetics of  $CO_2$  from coal. The current study adopts the desorption kinetic models proposed by Njikam and Schiewer (2012),<sup>56</sup> in which the adsorbate concentration remaining in the adsorbent during the desorption is the rate-determining factor (eqs 6 and 7).

$$PFO: q_t = q_e / e^{k_{dl}t}$$
(6)

PSO: 
$$q_t = \frac{q_e}{(1 + (k_{d2}q_et))}$$
 (7)

where  $q_i = \text{mass}$  adsorbed per mass of adsorbent at time t, g of CO<sub>2</sub>/kg of coal,  $q_e = \text{mass}$  adsorbed per mass of adsorbent at the time of equilibrium, g of CO<sub>2</sub>/kg of coal,  $k_{d1} = \text{first-order}$  rate constant for desorption,  $h^{-1}$  and  $k_{d2} = \text{second-order}$  rate constants for desorption, kg/g h.

The best fitting model was validated by the coefficient of determination  $(R^2)$  combined with the standard error of the estimate (eq 8).

Standard error of estimate (SEOE) = 
$$\sqrt{\left[\frac{\sum (q_{obs} - q_{fit})^2}{n}\right]}$$
 (8)

where  $q_{obs}$  is the experimentally observed mass of CO<sub>2</sub> adsorbed at time *t* (g of CO<sub>2</sub>/kg of coal),  $q_{fit}$  is the predicted mass of CO<sub>2</sub> adsorbed at time *t* (g of CO<sub>2</sub>/kg of coal) by PFO or PSO models, and *n* is the number of experimental observations.

Bangham model have been used to predict the influence of the pore diffusion, the slowest step of the gas adsorption (eq 9).<sup>39,57</sup>

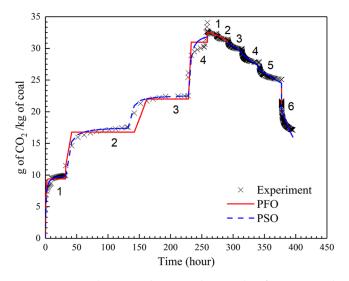
$$q_t = q_e(1 - \exp(-k_b t^n)) \tag{9}$$

where  $q_i$  is the mass adsorbed per mass of adsorbent at time t (g of CO<sub>2</sub>/kg of coal),  $q_e$  is the mass adsorbed per mass of adsorbent at the time of equilibrium, g of CO<sub>2</sub>/kg of coal, and  $k_b$  (h<sup>-1</sup>) and n are constants of the model.

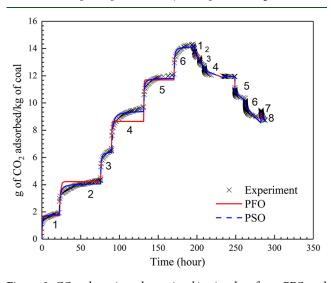
#### 3. RESULTS AND DISCUSSION

The amount of  $CO_2$  adsorbed-desorbed per kg of coal is calculated using eqs 2 and 3, respectively, for each pressure step of the adsorption and desorption experiments described earlier. The PFO, PSO, and Bangham models were fitted to the experimental data and to determine the rate-determining steps in  $CO_2$  adsorption on intact bituminous coal.

**3.1.** Analysis of CO<sub>2</sub> Adsorption–Desorption Kinetics Data. The results of the PFO and PSO model fits to the kinetics data are presented in Figures 4–7 and the summary of the fitting exercises is in Tables 3–6. Overall, the PSO model fits the data better than the PFO model. The PSO model assumes that available surface and pore volume are driving factors and diffusion, or chemisorption/surface interaction, are the primary rate-determining steps. In Figures 4–6, the experimental results of adsorption kinetics are plotted against the PFO and PSO models for intact core samples (EXP1, EXP2, and EXP3), and the model parameters are listed in Tables 3–5. The  $R^2$  values combined with the standard error of estimate indicate that the PSO model adequately describes



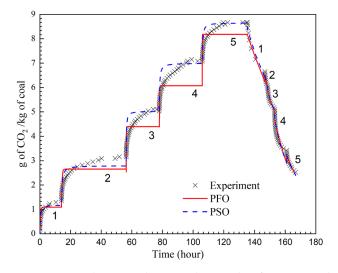
**Figure 4.**  $CO_2$  adsorption-desorption kinetics data fit to PFO and PSO models. Sample EMB1 and experimental condition EXP1 (the numbers in the plot represent the injection pressure stages; Table 3).



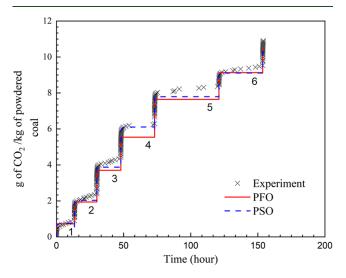
**Figure 5.**  $CO_2$  adsorption-desorption kinetics data fit to PFO and PSO models. Sample EMB1 and experimental condition EXP2 (the numbers in the plot represent the injection pressure stages; Table 4).

 $\rm CO_2$  adsorption on coal. Furthermore, the PSO kinetic model analysis was used to predict  $\rm CO_2$  adsorption on solid adsorbents, as well as the previously observed relationship between the PSO rate constant,  $k_{a2}$ , and the diffusion coefficient of adsorbent microspheres in the unipore model, which says that  $\rm CO_2$  adsorption on coal is controlled by pore diffusion.<sup>30–35</sup>

At higher pressures (up to 4.5 MPa; Figure 4, Table 3), the inconsistent relationship between the equilibrium pressure and the kinetic rate constant  $(k_{a2})$  of the PSO model indicates that the heterogeneous nature of the coal samples has an effect on adsorption and that bulk pore diffusion, surface physical adsorption, and pore filling occur first, followed by slow surface interactions. For example, as the equilibrium pressure increased from 0.63 to 2.5 MPa, the PSO rate constant  $(k_{a2})$  increased (from 0.21 to 0.32 kg/g h). At 3.6 MPa, the rate constant fluctuated to 0.31 kg/g h. The pressure independence of PSO parameters  $(k_{a2} \text{ and } q_{ae})$  at lower pressures (0.5 MPa; Tables 4 and 5; Figures 5 and 6) indicates that the varying



**Figure 6.**  $CO_2$  adsorption-desorption kinetics data fit to PFO and PSO models. Sample EMB2 and experimental condition EXP3 (the numbers in the plot represent the injection pressure stages; Table 5).



**Figure 7.**  $CO_2$  adsorption kinetics data fit to PFO and PSO models. Powdered sample and experimental condition EXP4 (the numbers in the plot represent the injection pressure stages; Table 6).

sizes of the pores in the coal have an effect on the adsorption process and that different mechanisms determine the rate of  $CO_2$  adsorption on intact coal samples. The higher rate constants ( $k_{a2}$ ; Tables 4 and 5) observed in low pressure adsorption experiments indicate that monolayer adsorption/ pore filling occurs initially, followed by multilayer or pore condensation.<sup>30</sup> As previous studies aimed to achieve higher density and higher adsorption at supercritical injection, no detailed comparative adsorption kinetic data for large intact samples at the given low temperature and pressure ranges has been published. As a result, the rate constant values presented in the current study for the intact bituminous coal samples had to be thoroughly evaluated.

Compared to the equilibrium times of lower pressure (Table 4; EXP2) experiments of EMB1 with those of high-pressure experiments (Table 3; EXP1), it took longer to attain equilibrium at higher pressures. The equilibrium times of the individual pressure stages show that the adsorption was a slow process in the low-pressure experiments. For example, to adsorb 10.06 g of  $CO_2/kg$  of coal, it took 36 h to reach

#### Table 3. PFO and PSO Model Parameters Obtained from Fitting EMB1 EXP1 Experimental Data<sup>a</sup>

pressure step-up stage no.					PI	FO			PSO		
adsorption	pressure A (MPa)	pressure B (MPa)	equilibrium time (h)	$\overset{k_{\mathrm{a}\mathrm{l}}}{(\mathrm{h}^{-1})}$	$q_{e1} \choose (g/kg)$	R <sup>2</sup>	SEO	$ \begin{array}{c} k_{a2} \\ (kg/g h) \end{array} $	$q_{e2} \ (g/kg)$	$R^2$	SEOE
1	1.03	0.63	32	1.5	9.39	0.99	9 0.67	0.21	9.81	0.89	0.41
2	2.02	1.43	96	2.32	16.8	0.99	<b>0.</b> 77	0.23	16.9	0.91	0.67
3	3.02	2.50	31	4.2	22	0.99	9 0.98	0.32	21.99	0.81	0.68
4	4.05	3.60	14	3.71	30.98	0.99	9 1.46	0.31	31.2	0.66	1.4
pressure step-up stage no.					PFO				PSO		
desorption	pressure A (MPa)	pressure B (MPa)	equilibrium time (h)	${{k_{d1}}\choose{h^{-1}}}$	$q_{d1} \over (g/kg)$	$R^2$	SEOE	<i>k</i> <sub>d2</sub> (kg/g h)	$q_{e^2} (g/kg)$	$R^2$	SEOE
1	3.08	3.21	14	0.001	32.6	0.76	0.08	$3.7 \times 10^{-5}$	32.62	0.76	0.08
2	2.55	2.73	18	0.001	32.1	0.18	0.58	$5.5 \times 10^{-5}$	32.2	0.18	0.58
3	2.01	2.23	22	0.002	30.9	0.79	0.199	$6.9 \times 10^{-5}$	30.88	0.78	0.199
4	1.5	1.75	27	0.002	29	0.68	0.335	$8.9 \times 10^{-5}$	29.1	0.69	0.332
5	1.02	1.31	36	0.002	26	0.74	0.353	0.0024	26.66	0.74	0.348
6	0.051	0.085	17	0.013	20	0.72	0.79	0.00073	20.27	0.75	0.76
<sup><i>a</i></sup> A = injection pressur	re in RC. $B = e$	quilibrium pres	sure in (RC + SC)	referring	g to the p	ressure	at A.				

Table 4. PFO and PSO	Model Parameters	Obtained from	Fitting EMB1	EXP2 Ex	perimental Data <sup>4</sup>
	mouel i ulumeters	Obtained nom	I tung LunDI		permental Data

pressure step-up stage no.						PF	<sup>S</sup> O			PSO		
adsorption	pressure A (MPa)	pressure B (MPa)	equilibrium (h)	time	$\stackrel{k_{\rm a1}}{\rm (h^{-1})}$	$q_{e1} \choose (g/kg)$	$R^2$	SEOE	k <sub>a2</sub> (kg/g h)	$q_{e2} \over (g/kg)$	$R^2$	SEOE
1	0.14	0.035	22		1.83	1.73	0.99	0.14	1.47	1.81	0.99	0.097
2	0.22	0.09	53		0.86	4.22	0.99	0.39	0.54	4.09	0.77	0.21
3	0.32	0.19	14		3.71	6.27	0.97	1.04	1.17	6.43	0.58	0.41
4	0.45	0.28	41		5.02	8.64	0.98	1.21	0.37	9.43	0.86	0.27
5	0.53	0.39	39		4.53	11.68	0.99	0.29	1.12	11.81	0.6	0.32
6	0.64	0.51	24		4.47	13.99	0.99	0.28	1.1	14.14	0.47	0.38
pressure step-up stage no.						PFO				PSO		
desorption	pressure A (MPa)	pressure B (MPa)	equilibrium time (h)	$k_{d1}$ (1	$h^{-1}$ )	$q_{\rm d1} \ ({ m g/kg})$	$R^2$	SEOE	$k_{\rm d2}~({\rm kg/g~h})$	$q_{e2} \ (g/kg)$	$R^2$	SEOE
1	0.41	0.44	6.5	0.01		14.2	0.77	0.046	0.0007	14.2	0.77	0.046
2	0.31	0.37	6	0.006		13.71	0.66	0.103	0.0005	13.71	0.67	0.102
3	0.26	0.31	25	0.007		13.14	0.73	0.094	0.0005	13.14	0.75	0.093
4	0.2	0.25	14	0.002		12.39	0.5	0.145	0.00015	12.39	0.5	0.145
5	0.15	0.21	13	6.2 ×	$10^{-6}$	11.95	0.71	0.002	$5.15 \times 10^{-6}$	11.95	0.54	0.002
6	0.1	0.16	20	0.004		10.78	0.54	0.142	0.0004	10.78	0.55	0.014
7	0.063	0.094	20	0.007		9.76	0.59	0.23	0.0007	9.77	0.6	0.23
8	0	0.03	5	0.014		9.28	0.78	0.103	0.002	9.28	0.78	0.102
$^{a}A = injection pressu$	ure in RC. B =	equilibrium pre	essure in (RC +	- SC) ±	for the	injection	pressure	A.				

equilibrium pressure of 0.63 MPa (stage no. 1, Table 3) in high injection pressure experiments. To adsorb a similar amount of  $CO_2$  (9.43 g of  $CO_2$ /kg of coal), the EMB1 sample required 130 h of cumulative equilibrium time (stage nos. 1 to 4; Table 4) at low pressure injections (up to 0.5 MPa). The results from the current study indicate that the longer equilibrium times and small step-up injection pressures can yield maximum adsorption capacity at low pressure injections (up to 0.5 MPa; Figures 5 and 6; Tables 4 and 5) in shallow level bituminous coal seams.

Equilibrium times of desorption kinetics show that the equilibrium was attained faster than the adsorption pressure step up kinetic experiments. However, the amount remaining adsorbed was greater than that of the corresponding equilibrium conditions of the adsorption because all the adsorbed  $CO_2$  was not readily desorbed, or the process was not

reversible, which further explains the better fit of the secondorder kinetic model. The significant amount of residual  $CO_2$ trapped in the coal samples (Figures 4–7) was attributed to the pore trapping mechanisms such as pore blockage, gas cavitation, adsorption induced deformation, and pore network effect or ink bottle effect.<sup>58–60</sup> The results in Figure 4 show that 17 g of  $CO_2/kg$  of coal remained in the EMB1 coal core at the end of the desorption experiments. Similar  $CO_2$  entrapment was observed during the lower pressure EXP2 and EXP3 tests on the intact EMB1 and EMB2 coal cores (Figures 5 and 6). The residual amount of  $CO_2$  retained in the EMB1 and EMB2 samples, during low injection pressure, was about 8 g of  $CO_2/kg$  of coal (up to 0.64 MPa injection pressure) and 2.52 g of  $CO_2/kg$  of coal (up to 0.52 MPa injection pressure), respectively. This means that small increments in injection pressures can result in an increased amount of residual  $CO_2$ 

#### Table 5. PFO and PSO Model Parameters Obtained from Fitting EMB2 EXP3 Experimental Data<sup>4</sup>

pressure step-up stage no.					PFC	)			PSO		
adsorption	pressure A (MPa)	pressure B (MPa)	equilibrium time (h)	$\overset{k_{\mathrm{a1}}}{(\mathrm{h}^{-1})}$	$q_{\rm e1} \over ({ m g/kg})$	$R^2$	SEOE	${k_{\mathrm{a2}} \over (\mathrm{kg/g} \mathrm{~h})}$	$q_{\rm e2} \ ({ m g/kg})$	$R^2$	SEOE
1	0.13	0.058	14	3.0	1.09	0.76	0.17	3.57	1.19	0.86	0.12
2	0.21	0.12	42	3.57	2.65	0.65	0.32	12.18	2.79	0.81	0.23
3	0.32	0.21	21	14.74	4.39	0.36	0.49	8.98	5.03	0.3	0.5
4	0.41	0.3	28	7.27	6.07	0.42	0.52	14.7	7	0.47	0.46
5	0.52	0.40	29	36.17	8.18	0.15	0.52	10.77	8.66	0.69	0.31
pressure step-up stage											
no.					PFC	)			PSO		
	pressure A (MPa)	pressure B (MPa)	equilibrium time (h)	$\frac{k_{d1}}{(h^{-1})}$	$\frac{q_{\rm d1}}{(g/\rm kg)}$	0 R <sup>2</sup>	SEOE	$rac{k_{ m d2}}{ m (kg/g~h)}$	$\frac{q_{\rm e2}}{(g/kg)}$	R <sup>2</sup>	SEOE
no.				$k_{d1} \ (h^{-1}) \ 0.025$			SEOE 0.30		g <sub>e2</sub>	R <sup>2</sup> 0.91	SEOE 0.2
no.	(MPa)	(MPa)	(h)	$(h^{-1})$	$q_{\rm d1} \ ({ m g/kg})$	$R^2$		(kg/g h)	$q_{\rm e^2} ({ m g/kg})$		
desorption 1	(MPa) 0.33	(MPa) 0.37	(h) 11.5	$(h^{-1})$ 0.025	q <sub>d1</sub> (g/kg) 7.98	R <sup>2</sup> 0.80	0.30	(kg/g h) 0.0004	9 <sub>e2</sub> (g/kg) 8.43	0.91	0.2
desorption 1 2	(MPa) 0.33 0.24	(MPa) 0.37 0.3	(h) 11.5 1.8	(h <sup>-1</sup> ) 0.025 0.053	$q_{d1} (g/kg)$ 7.98 6.12	R <sup>2</sup> 0.80 0.88	0.30 0.07	(kg/g h) 0.0004 0.009	q <sub>e2</sub> (g/kg) 8.43 6.52	0.91 0.88	0.2 0.07
desorption 1 2 3	(MPa) 0.33 0.24 0.15	(MPa) 0.37 0.3 0.23	(h) 11.5 1.8 4.5	(h <sup>-1</sup> ) 0.025 0.053 0.036	$q_{d1} \ (g/kg)$ 7.98 6.12 5.42	R <sup>2</sup> 0.80 0.88 0.98	0.30 0.07 0.1	(kg/g h) 0.0004 0.009 0.007	$q_{e2}$ (g/kg) 8.43 6.52 5.82	0.91 0.88 0.88	0.2 0.07 0.1

Table 6. PFO and PSO Model Parameters Obtained from Fitting Powdered Coal EXP3 Experimental Data<sup>a</sup>

pressure step-up stage no.					PF	С			PSO			
adsorption	pressure A (MPa)	pressure B (MPa)	equilibrium time (h)	$k_{a1}$	$q_{ae}$	$R^2$	SEOE	k <sub>a2</sub>	<i>q</i> <sub>ae</sub>	$R^2$	SEOE	
1	0.11	0.042	13.4	10.10	0.73	0.83	0.12	16.23	0.76	0.89	0.09	
2	0.20	0.095	16.64	90.47	1.94	0.59	0.26	66.83	2.04	0.75	0.2	
3	0.31	0.17	17.88	130.87	3.75	0.49	0.39	70.51	3.88	0.76	0.27	
4	0.42	0.27	25.13	458.37	5.54	0.22	0.46	14.24	6.11	0.99	0.06	
5	0.51	0.36	47.92	649.36	7.64	0.15	0.45	149.45	7.79	0.59	0.34	
6	0.52	0.43	32.62	967	9.06	0.27	0.27	397	9.1	0.45	0.28	
<sup><i>a</i></sup> A = injection pressure	in RC. B = equili	brium pressure in	(RC + SC) for the	injection	pressure	e A.						

retained in the micropore channels of bituminous coals, independent of sample sizes used in the experiments. Therefore, residual  $CO_2$  in intact cores is correlated with the equilibrium pressures, indicating the small amount of residual was achieved for EMB2 as the pressure was not sufficient for the  $CO_2$  to enter the ultra-nanopores. This further strengthens the assumptions of the PFO and PSO models of surface interaction and pore diffusion and condensation. Overall, the analysis indicates that CO<sub>2</sub> adsorption on bituminous EMB coal is controlled by the pore diffusion process in the initial stages and surface interaction takes over. To compare the desorption kinetics results obtained from PFO and PSO models (Tables 3-5), there are no published desorption kinetics data. Therefore, detailed desorption kinetics studies needed to be studied further to ascertain the reversibility of  $CO_2$  adsorption.

The powder sample showed an increasing trend in equilibrium times (Table 6), with the equilibrium pressure demonstrating that large, exposed polarized sites cause surface interaction mechanisms to take over following pore diffusion. The active sites in bituminous coals are created by functional groups and carbon-containing groups, which become more exposed when coal is pulverized.<sup>26,61</sup> For the powdered sample experimental data, the SEOE values show that the PSO model fit better than the PFO model, supporting the above-mentioned interpretation that surface interaction is the slowest rate-determining step rather than physical adsorption and diffusion processes (Figure 7; Table 6). A similar type of

experiment conducted by Gabruś et al.  $(2021)^{34}$  showed significantly higher  $k_{a1}$  and  $k_{a2}$  values than the current study  $(k_{ad1}$  was in the range of  $1.6 \times 10^6$  to  $1.0 \times 10^6$  h<sup>-1</sup> and  $k_{ad2}$  was in the range of  $5.7 \times 10^6$  to  $12 \times 10^6$  h<sup>-1</sup>). However, the present study intends to allow the equilibrium to occur for each pressure step, whereas in the previous experiments the equilibrium values were reported for only 24 h (for pressure ranging from 0.5 to 6.4 MPa).

Despite the increased surface area of the powdered samples, the intact samples showed similar equilibrium adsorbed amount  $(q_e)$  values obtained for the powdered samples at comparable pressure and temperature conditions. The  $q_e$  values were 11.68 g/kg (at 0.53 MPa) and 7.58 g/kg (at 0.52 MPa) for the intact EMB1 and EMB2 samples, whereas the powdered sample showed 9.06 g/kg (at 0.52 MPa). These results indicate the influence of channel-like pores on the high-density CO<sub>2</sub> (liquid like) adsorption in intact samples. These pores will be lost or modified when the samples are powdered, and less density gas phase adsorption occurs in the large surface area exposed.

**3.2.** Bangham Model for the Pore Diffusion-Controlled Adsorption Process. To ascertain the pore diffusion theory, the experimental data set was fitted into the Bangham model. The Bangham model fitting, shown in Figure 8, predicts that the  $q_e$  values are closely matched to those calculated using the PSO and the PFO model. Moreover, for PFO and PSO the data needed to be fitted segmentally for the specific equilibrium pressure stages, whereas the entire data set

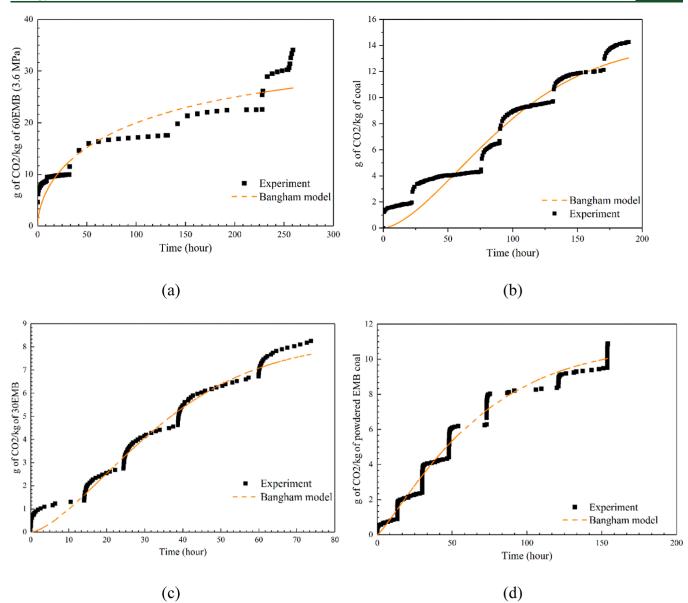


Figure 8.  $CO_2$  adsorption-desorption kinetics data fitted to the Bangham pore diffusion model. (a) Sample EMB1, experimental condition EXP1 and (b) EXP2; (c) sample EMB2, experimental condition EXP3; and (d) powdered sample and experimental condition EXP4.

has been (all the stages) used in the nonlinear fitting of the Bangham model (Figure 8). The model parameters and the coefficient of determination  $(R^2)$  values listed in Table 7 show that the CO<sub>2</sub> adsorption on bituminous EMB coal is pore diffusion controlled at a pressure range of 0.5 to 4.5 MPa at a temperature of 298.15 K.

The pressure dependency of the adsorption kinetic model parameters (n and  $k_b$ ) and the coefficient of determination ( $R^2$ ) values show that bulk pore diffusion is not the only the rate-determining factor. At lower pressure experiments, the

 Table 7. Fitting Parameters of the Bangham Pore Diffusion

 Model

experiment	sample	$k_{\rm b}~({\rm h}^{-1})$	n	SEOE	$R^2$
EXP1	EMB1	0.061	0.58	2.94	0.87
EXP2		0.0006	1.6	0.98	0.94
EXP3	EMB2	0.004	1.52	0.35	0.98
EXP4	powder	0.007	1.18	0.45	0.98

parameters n and  $k_b$  are greater than at higher-pressure experiments, implying that the pore diffusion is the ratedetermining step at lower pressures and the surface interaction is the rate-determining step at higher equilibrium pressures. The coefficient of determination values complies with the observations as the value observed for high pressure experiment (up to 3.6 MPa) was 0.87 and which are smaller than that of low-pressure (up to 0.5 MPa) adsorption experiments of same sized EMB1 coal ( $R^2 = 0.94$ ). Much lower equilibrium pressure experiments with the EMB2 sample (up to 0.4 MPa) were in good agreement with the model  $(R^2 = 0.98)$ , underscoring that the pore diffusion is the predominate ratedetermining factor at lower pressure and surface interaction takes over at higher pressures.<sup>62</sup> The standard error of estimate was correlated with the coefficient of determination  $(R^2)$ values. The powdered samples showed a similar trend to the pore diffusion model data fitting (Figure 8d). The better fit in the PSO model for powdered materials (Figure 7 and Table 6) and longer equilibrium durations imply that the rate

controlling process is  $CO_2$  interaction with polarized sites, followed by early pore diffusion and condensation.

## 4. CONCLUSIONS

This study presented extensive data from adsorption– desorption kinetics for injection pressures of up to 0.5 MPa in the context of injecting  $CO_2$  into shallow level coal seams for the first time. The powdered samples took longer to reach equilibrium, indicating exposed surface sites that are unlikely to be present if the coal is intact. At the same corresponding equilibrium pressures, the comparable equilibrium amount of  $CO_2$  adsorbed on the intact and powdered samples indicated the importance of conducting experiments with large intact samples.

The PSO model fitted the experimental data well for both adsorption and desorption kinetics, implying that pore diffusion and surface interaction are the rate-determining steps. The cumulative experimental data fitting to the Bangham diffusion model supported the idea that pore diffusion is the rate-determining step in the  $CO_2$  adsorption process on bituminous EMB coal at lower pressures.

The current study established detailed  $CO_2$  desorption kinetics from intact coal samples for perhaps the first time, and the data fitted into the modified PFO and PSO models. The data from desorption kinetics confirm the prediction by demonstrating the pore trapping capabilities. The amount of residual  $CO_2$  retained in the coal sample at the end of the desorption tests demonstrates the pore trapping capabilities of the bituminous coal sample. The amount of  $CO_2$  trapped was proportional to the equilibrium pressure.

In broad sense, the adsorption-desorption kinetics experiments provided insights into rate-determining mechanism, reversibility of  $CO_2$  adsorption, or pore entrapment of  $CO_2$  at the low-pressure injection in shallow level bituminous coal seams.

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#### Notes

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