A Study on the Performance of Half-wave Plates **Designed for Sub-mm Studies**



Charlotte Braithwaite¹, Carole Tucker¹, Erminia Calabrese¹, Giulio Fabbian^{2,1}, Serena Giardiello¹, Giampaolo Pisano³, Giorgio Savini⁴ ¹Cardiff University, ²Institute of Astronomy, Cambridge, ³Sapienza Università di Roma, ⁴University College London Email: braithwaitec1@cardiff.ac.uk

Goal – Spectral characterisation of a metal mesh HWP designed for sub-mm, simulate the sky and study the effect of HWP systematics in CMB searches of r for mitigation strategies and compare to current HWPs used.

Introduction

To measure linearly polarised signals within the CMB sapphire HWPs have typically been used as polarisation modulators. However, more recently⁴ embedded metal mesh (MM) based HWPs have shown good performance over a broad band in the sub-mm regime, presenting the possibility of replacing sapphire HWPs in CMB studies. This work presents the spectral characterisation of a MM HWP & bias on *r* caused by the HWPs systematics.

Method

Optical setup using an FTS to measure the spectral performance of a HWP shown in Fig 1, with the data extraction routine given below.



Fig 1: Schematic diagram of the optical test bench for transmission measurements of the NIKA2⁴ HWP using a Fourier Transform Spectrometer¹ (FTS). Co-polarisation (co-pol) measurements obtained by orientating the polarisers parallel to one another. Cross-polarisation (cross-pol) measurements were obtained by rotating the polariser on the righthand side by 90°. HWP was held in a rotator and rotated through 360° to obtain full spectral data cubes.





Fig 4: A "reduced" Mueller matrix of the NIKA2 HWP using the optical setup in Fig 1. Errors (1 σ) are included in red and the green shaded regions represent the NIKA2 frequency bands, indicating the frequencies over which the HWP is performing over.



Fig 6: Left) BB power spectra and right) BB power spectra for an ideal HWP (orange) and the NIKA2 HWP (blue). Calculated using results in Fig 5 and maps generated by substituting ideal Mueller matrix components into s4cmb. The black curves represents the input C_{ℓ}^{BB} and C_{ℓ}^{EB} respectively. This assumes a CMB only case and does not include contributions from foregrounds



Fig 5: Sky patch maps generated by injecting the averaged components across the 150 GHz band in Fig 4 into the s4cmb³ pipeline. Left column shows the I (top), Q (middle) and U (bottom) components of the input sky maps. The middle column shows the maps after demodulation and the right column shows the difference between the left and middle columns which is an order of magnitude smaller than the sky maps

• *BB*, *EE* and *EB* power spectra indicate an effective polarisation angle miscalibration

Power spectra in Fig 6 calculate⁵ a bias of $\delta r = 0.009 \pm 0.002$

- Further work required:
- Cross check implementation of matrix components in s4cmb
- Replicate calculation of δr using other pipelines^{5,6}

Comparison

Sapphire HWPs (Pancharatnam designed) Embedded metal mesh HWPs Good transmission across broad band² Good transmission across broad band⁴ Limitations on diameter size of sapphire Potential for HWPs to be made to diameters plates, ~50 cm >50 cm (65cm mesh-reflective HWP built and ~20 kg (3 plate sapphire HWP) tested) ~1 kg – dependent on size Can be difficult to apply ARC⁷ Temperature dependence² Easier to apply ARC Frequency dependence² No temperature dependence Simulated performance⁸ shows potential bias More work needs to be done to understand on $r \sim 10^{-4}$ the effects of their non-idealities

Conclusions

The spectral characterisation of a metal mesh HWP produced Mueller matrix values close to the theoretically ideal values. Maps were produced with the injected 150 GHz band averaged matrix parameters and used to generate the angular power spectra for both the NIKA2 HWP and an ideal HWP. Subtracting $C_{\ell,ideal}^{BB}$ and $C_{\ell,NIKA2}^{BB}$ resulted in $\delta r = 0.009 \pm 0.002$. Further work is required to cross check method and ensure no miscalibration in the polarisation angle is occurring.

Literature Cited

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