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Citation for final published version:

Qin, Zixuan, Guo, Jian, Cleall, Peter J. , Xu, Qiang, Cherry, John A. and Parker, Beth L. 2026. Gain-phase characteristics of groundwater responses to barometric pressure: interpreting subsurface confinement in layered systems. *Journal of Hydrology* 671 , 135296. 10.1016/j.jhydrol.2026.135296

Publishers page: <https://doi.org/10.1016/j.jhydrol.2026.135296>

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1 **Gain–Phase Characteristics of Groundwater Responses to Barometric Pressure:**
2 **Interpreting Subsurface Confinement in Layered Systems**

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14 **Keywords:**

15 Barometric response; Aquifer confinement; Frequency analysis; Layered systems; Groundwater

16 **Highlights:**

- 17 • Time- and frequency-domain analyses reveal lithology-controlled barometric responses
18 in layered systems
19 • Gain–phase relationships differ systematically between unconfined and confined-like
20 response regimes
21 • Gain–phase co-variation trends provide insight into confinement-related pressure
22 transmission behavior

23 Abstract

24 Aquifer confinement plays a key role in controlling vertical hydraulic connectivity and pressure
25 transmission, yet its identification in heterogeneous systems remains challenging using
26 conventional methods. This study applies frequency-domain barometric response functions
27 (BRF) to analyze groundwater response to atmospheric pressure. A six-port Continuous
28 Multichannel Tubing (CMT) system was installed in a layered aquifer. Long-term groundwater,
29 barometric pressure, and precipitation data were analyzed using cross-correlation, FFT, and BRF
30 methods. Time- and frequency-domain analyses reveal pronounced lithology-controlled
31 differences. Ports screened in sandstone units exhibited stronger barometric signals and shorter
32 response lags, while mudstone-adjacent ports showed attenuated responses. Detailed BRF
33 analysis was performed on two representative ports: Port 1 (upper sandstone above mudstone)
34 and Port 6 (lower sandstone below mudstone). The upper sandstone showed a negative gain-
35 phase co-variation, characteristic of unconfined systems, while the lower sandstone exhibited a
36 positive gain-phase relationship, suggesting functional confinement. These findings highlight the
37 utility of BRF analysis for interpreting pressure transmission and confinement in vertically
38 heterogeneous aquifers.

39 1 Introduction

40 Aquifers often exhibit vertical heterogeneity, and variations in confinement-related hydraulic
41 behavior can substantially influence surface–groundwater interactions (Gulley et al., 2013),
42 solute transport (Koh et al., 2016; Wang et al., 2024), waste storage (Maliva & Walker, 1998;
43 Liu et al., 2025), and groundwater resource management (Bui et al., 2012; Rausch & Dirks,
44 2024). Conventional approaches for characterizing aquifer confinement, such as pumping tests
45 and borehole drilling, are often constrained by subjectivity, high costs, disturbance, and limited
46 capacity for continuous monitoring. Periodic barometric tides (e.g., diurnal and semi-diurnal
47 tides) induce groundwater level fluctuations, offering a natural perturbation means to infer
48 aquifer hydraulic properties (Merritt, 2004; Acworth et al., 2017; McMillan et al., 2019; Qi et al.,
49 2023). Thus, analyzing groundwater responses to barometric pressure fluctuations can provide
50 valuable insights into aquifer confinement and vertical hydraulic connectivity.

51 Groundwater level responses to atmospheric loading are governed by multiple factors, including
52 well construction, aquifer hydraulic properties, and site-specific geological conditions, resulting
53 in a wide range of barometric response behaviors. These responses are commonly discussed in

54 terms of confined, semi-confined, and unconfined conceptual end-members, reflecting
55 contrasting pressure transmission pathways and storage mechanisms (Rojstaczer & Agnew,
56 1989). In confined systems, barometric pressure variations are generally transmitted rapidly to
57 the pore fluid and shared between the aquifer matrix and groundwater. Under ideal conditions
58 where wellbore storage and skin effects are negligible, the resulting groundwater level
59 fluctuations can be approximated by a constant response, referred to as the static barometric
60 efficiency (Jacob, 1940). By contrast, in unconfined and semi-confined systems, thick
61 unsaturated zones or low-permeability confining layers may attenuate and delay pressure
62 transmission, leading to reduced and time-dependent groundwater level responses (Weeks, 1979;
63 Spane, 2002; Lai et al., 2013). Such delayed propagation can generate transient pressure
64 gradients between the aquifer and the well, causing groundwater responses that vary across both
65 time- and frequency-domains. Barometric response functions (BRF) provide a quantitative
66 framework for characterizing these response behaviors and for examining the physical
67 mechanisms governing pressure transmission and damping.

68 Rasmussen and Crawford (1997) introduced a regression–deconvolution approach to derive
69 time-domain BRFs, characterizing the shape and lag of groundwater level responses to
70 atmospheric pressure fluctuations. Subsequent studies have applied to estimate barometric
71 efficiency (BE), identify wellbore effects, and assess aquifer confinement (Landmeyer, 1996;
72 Butler et al., 2011; Patton et al., 2021; Akara et al., 2025). However, time-domain interpretations
73 are often sensitive to uncertainties in unsaturated zone thickness, leakage conditions, and
74 nonstationary forcing, and response lag is difficult to quantify robustly under high-frequency
75 perturbations. Frequency-domain BRF provide a more time-invariant and mathematically
76 rigorous framework, wherein the gain and phase functions characterize aquifer responses to

77 periodic loading and reveal differences in transmission mechanisms across temporal scales. In
78 frequency-domain BRF analyses, aquifer responses to barometric loading are commonly
79 characterized using gain and phase functions. Gain describes the ratio of groundwater level
80 fluctuation amplitude to atmospheric pressure forcing at a given frequency, reflecting the
81 efficiency of pressure transmission into the subsurface. Phase represents the temporal offset
82 between the two signals in the frequency-domain and provides information on the characteristic
83 response time and damping behavior of the aquifer system (Rojstaczer, 1988; Evans et al., 1991).
84 From a system-response perspective, gain and phase are complementary descriptors of the same
85 physical process and are inherently linked across frequencies. Analytical solutions have been
86 developed for semi-confined aquifers by Rojstaczer (1988) and Evans et al. (1991), and for
87 unconfined conditions by Rojstaczer and Riley (1990) and Quilty and Roeloffs (1991).
88 Frequency-domain BRF have been widely used to examine spatial variability in barometric
89 responses across wells (Oldling et al., 2015; Sun & Xiang, 2020; Kennel & Parker, 2024) and to
90 monitor changes in aquifer properties following events such as earthquakes, pumping, and
91 landslides (Elkhoury et al., 2006; Hessein et al., 2013; Sun & Xiang, 2019; Zhang et al., 2019;
92 Thomas et al., 2023; Qi et al., 2024; Qin et al., 2025). However, systematic evaluation of gain–
93 phase behavior across vertically distributed monitoring depths remains limited, particularly with
94 respect to interpreting confinement-related response behavior in layered aquifer systems.

95 In this study, we aim to evaluate whether frequency-domain gain–phase relationships can be
96 used as a diagnostic indicator of aquifer confinement and vertical hydraulic connectivity in
97 layered groundwater systems. To this end, a Continuous Multichannel Tubing (CMT) monitoring
98 system was deployed to obtain long-term, vertically resolved groundwater level records under
99 natural atmospheric forcing. By focusing on the systematic behavior of gain and phase across

100 monitoring depths, rather than on individual response metrics alone, this study seeks to address a
101 key limitation of existing BRF applications in heterogeneous aquifers. The proposed framework
102 emphasizes the interpretive value of gain–phase co-variation and provides a physically grounded
103 approach for assessing confinement-related hydraulic behavior in multilevel monitoring wells.
104 It should be noted that confinement in this study is operationally defined in the context of its
105 functional impact on pressure transmission, as inferred from observed barometric response
106 behavior, rather than as a strict stratigraphic classification. Unlike traditional rigid-flow theory,
107 which treats confinement as a static condition governed by impermeable layers, the observed
108 responses in this study are more consistent with a poroelastic framework, in which pressure
109 transmission is controlled by the elastic and diffusive properties of the aquifer system and
110 overlying materials. Accordingly, confinement is interpreted through frequency-dependent gain–
111 phase characteristics, which reflect the effective vertical hydraulic connectivity and pressure
112 transmission behavior under atmospheric loading.

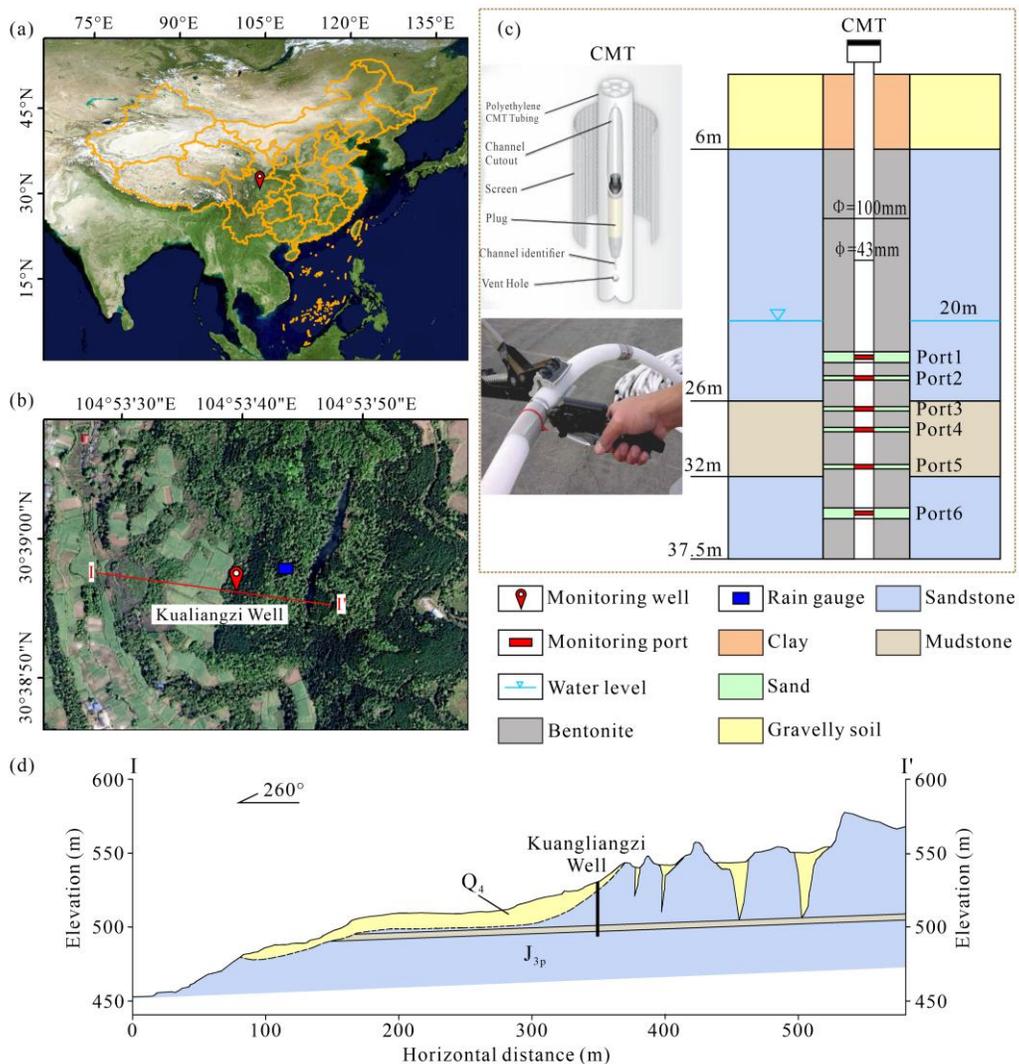
113 **2 Study Area and Data**

114 2.1 Study Area and Monitoring Network

115 The Kualiangzi monitoring well is located in Sichuan Province, southwestern China
116 ($30^{\circ}39'01''\text{N}$, $104^{\circ}53'40''\text{E}$), situated on the midslope of a local hillslope groundwater system
117 (Figure 1a, b). The study area is predominantly covered by a layer of residuals and diluvials (Q₄),
118 consisting of silty clay mixed with a small amount of gravel. The underlying bedrock comprises
119 interbedded sandstone and mudstone of the Upper Penglaizhen Group of the Jurassic Period (J_{3p})
120 (Figure 1d).

121 The well–aquifer system and borehole completion details are illustrated in Figure 1c. The
122 monitoring well is completed as a sealed, multi-level system using Continuous Multichannel

123 Tubing (CMT), which enables depth-discrete groundwater level monitoring while minimizing
 124 hydraulic interference between stratigraphic units. The borehole diameter is 100 mm, and the
 125 CMT tubing has an outer diameter of 43 mm. Six monitoring ports (Ports 1–6) are installed at
 126 depths corresponding to the center of the sand-packed intervals: 21.9–22.9 m, 24.0–24.3 m,
 127 26.4–26.7 m, 28.0–28.3 m, 30.9–31.2 m, and 34.3–35.3 m, respectively. Continuous core data
 128 from the well site revealed a stratigraphic sequence of approximately 6 m of gravelly soil, 20 m
 129 of sandstone, 6 m of mudstone, and 5.5 m of sandstone. The thickness of the unsaturated zone is
 130 approximately 20 m.



131

132 **Figure 1.** (a) The location map of the Kualiangzi well, (b) Topography in the Kualiangzi area
133 around the Kualiangzi well (red dot), (c) Schematic diagram of the CMT well illustrating port
134 depths and borehole construction, and (d) Simplified geological profile and the monitoring well
135 location of section I-I'.

136 2.2 Data Collection and Observation

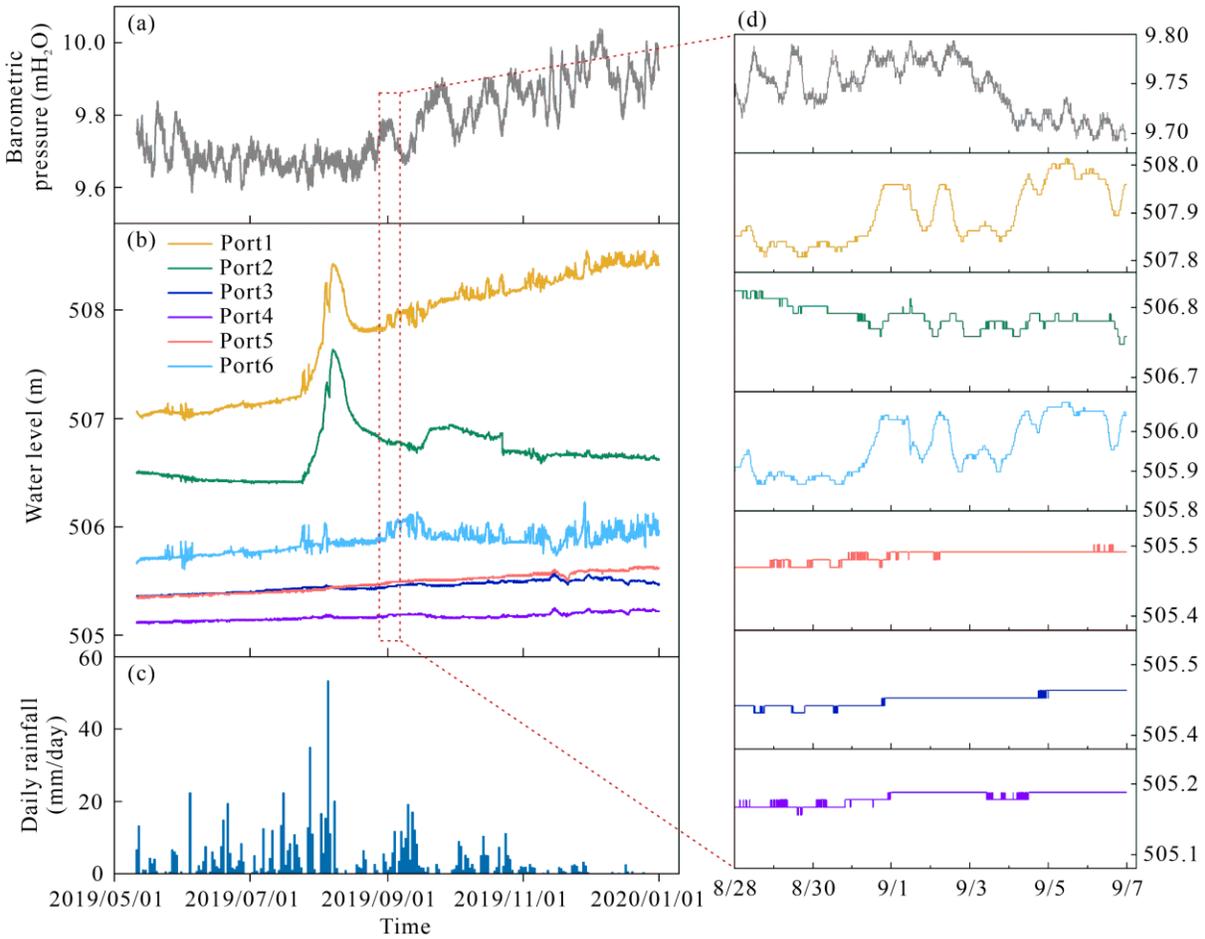
137 Groundwater levels at each monitoring port were measured using Micron MP102 gauge
138 piezometers, each with a measurement resolution of 0.01 m and a sampling interval of 10 min.
139 Barometric pressure was recorded using a Baro-Diver with a precision of 0.01 mH₂O (0.1 hPa)
140 and sampling interval of 10 min. Rainfall data were obtained from a real-time precipitation
141 monitoring station located within the study area, with a temporal resolution of 1 hour and an
142 accuracy of 0.01 mm. It is important to note that sensor resolution plays a critical role in the
143 observed data. The limits of analogue-to-digital conversion are reflected in the data, and any
144 signals smaller than this threshold are not captured by the sensors.

145 As observed in Fig. 2, groundwater levels in Ports 1 and 2 show a clear response to rainfall
146 events, while the relatively elevated heads at Ports 5 and 6 suggest a contrasting hydraulic
147 behavior compared to the shallow monitoring ports. Across all six monitored depths,
148 groundwater levels generally declined in response to rising barometric pressure and rose when
149 atmospheric pressure decreased. Peaks in barometric pressure commonly coincided with troughs
150 in groundwater levels, indicating a predominantly negative correlation (Wang & Manga, 2023).

151 Although barometric responses appeared broadly synchronous across depths within the borehole,
152 a measurable lag time was observed between atmospheric pressure changes and groundwater
153 level responses. Such temporal delays are consistent with previous observations (Furbish, 1991;

154 Rasmussen & Crawford, 1997; Valois et al., 2023) and reflect site-specific hydraulic and well-
 155 aquifer interaction processes.

156



157

158 **Figure 2.** Time series data from 10 May to 31 December 2019, including: (a) barometric

159 pressure; (b) groundwater levels at six monitoring ports; (c) rainfall; and (d) an enlarged view of

160

groundwater levels from 28 August to 7 September 2019.

161 **3 Methods and Results**

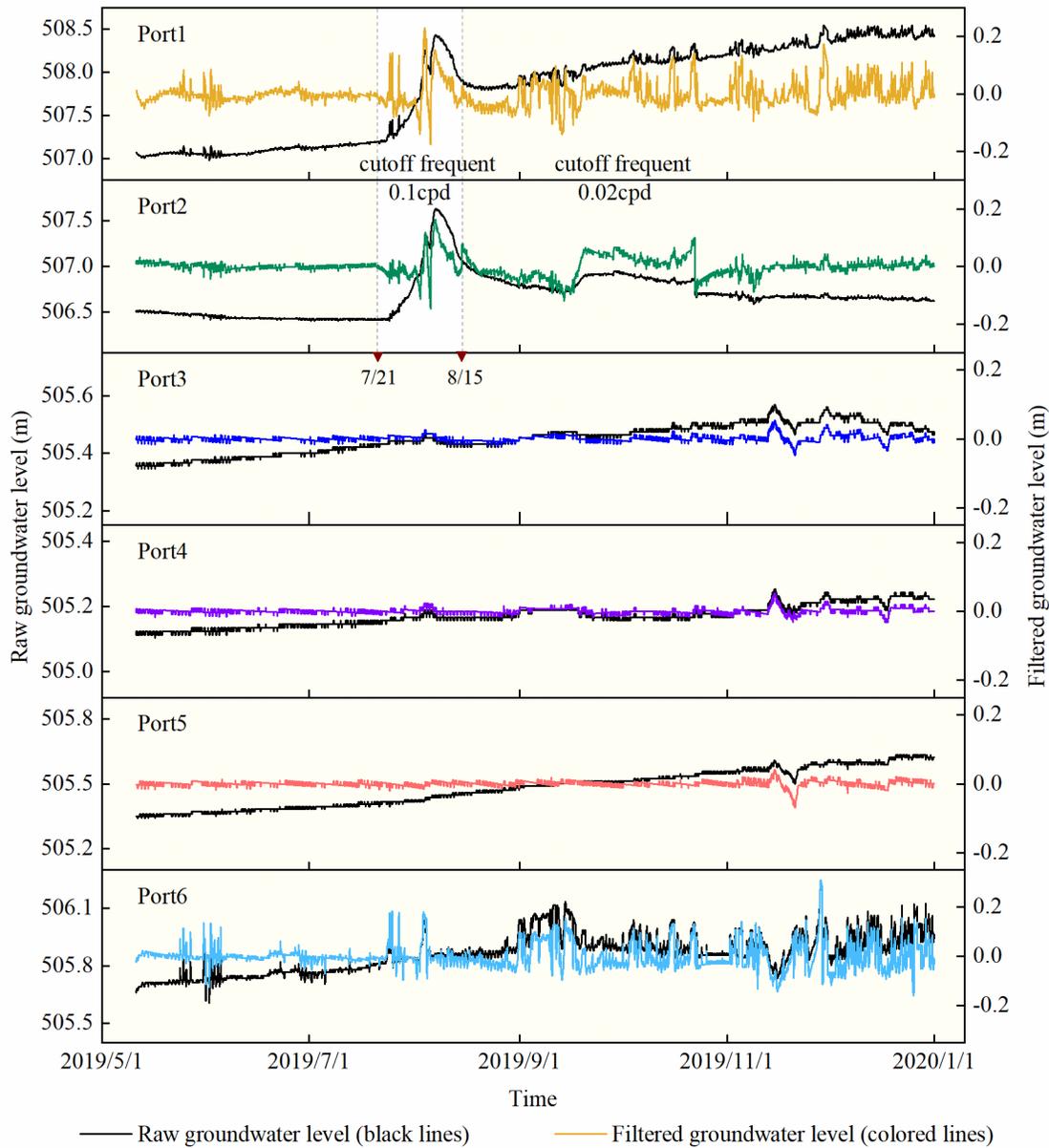
162 3.1 Data Preprocessing

163 Data preprocessing is essential for isolating groundwater responses to barometric pressure, as

164 groundwater level fluctuations are influenced by multiple hydrological factors (Jan et al., 2007).

165 In the study area, rainfall represents the dominant non-barometric forcing and must be removed
166 prior to barometric response analysis. Although the region experiences substantial precipitation,
167 the presence of a thick unsaturated zone in the central part of the slope body can attenuate and
168 delay the transmission of recharge signals to groundwater (Xu et al., 2015).

169 High-pass Butterworth filtering was applied to groundwater level time series to suppress low-
170 frequency components associated with rainfall recharge and long-term trends, while preserving
171 barometric pressure-induced fluctuations. A first-order Butterworth filter was implemented
172 using a forward-backward (zero-phase) filtering scheme (filtfilt function in MATLAB), ensuring
173 that no phase distortion was introduced during preprocessing. Figure 3 compares the original and
174 filtered groundwater level time series. Due to pronounced differences in rainfall sensitivity
175 across monitoring depths and time periods, cutoff frequencies were selected adaptively to
176 effectively remove recharge-related signals. For Ports 1 and 2, which exhibited strong rainfall-
177 induced groundwater level rises during periods of intense precipitation (21 July–15 August
178 2019), a higher cutoff frequency of 0.1 cycles per day was applied. For other periods at these
179 ports (11 May–20 July and 16 August–31 December 2019) and Ports 3 to 6 to ensure consistency
180 across monitoring ports, a uniform cutoff frequency of 0.02 cpd was applied to all monitoring
181 depths. As shown in Fig. 3, this filtering strategy effectively removed recharge-related
182 fluctuations, enabling subsequent analyses to focus on groundwater responses to atmospheric
183 pressure variations. To evaluate the robustness of the BRF results to the choice of cutoff
184 frequency, a sensitivity analysis using alternative filtering parameters was conducted, and the
185 results are presented in Supplementary Material S1.



186

187

Figure 3. Groundwater level time series at Ports 1–6, showing raw water level signals (black

188

lines) and filtered signals with recharge effects removed (colored lines).

189

3.2 Cross-Correlation Analysis

190

The cross-correlation function (CCF) is a statistical tool commonly used to quantify the

191

relationship between an input time series $\{x_t\}_{t=1}^n$ and an output time series $\{y_t\}_{t=1}^n$ by evaluating

192

their correlation at different time lags (Padilla & Pulido-Bosch, 1995; Molénat, 1999; Shi, 2018).

193 In groundwater studies, CCF analysis is widely applied to identify the delayed responses of
 194 groundwater levels to external forcings, such as atmospheric pressure. The magnitude of the
 195 cross-correlation coefficient reflects the strength of the relationship between the two series, while
 196 the lag at which the correlation reaches an extremum provides an estimate of the response delay
 197 (Manna, 2022). In this study, the cross-correlation function between barometric pressure and
 198 groundwater level is defined as:

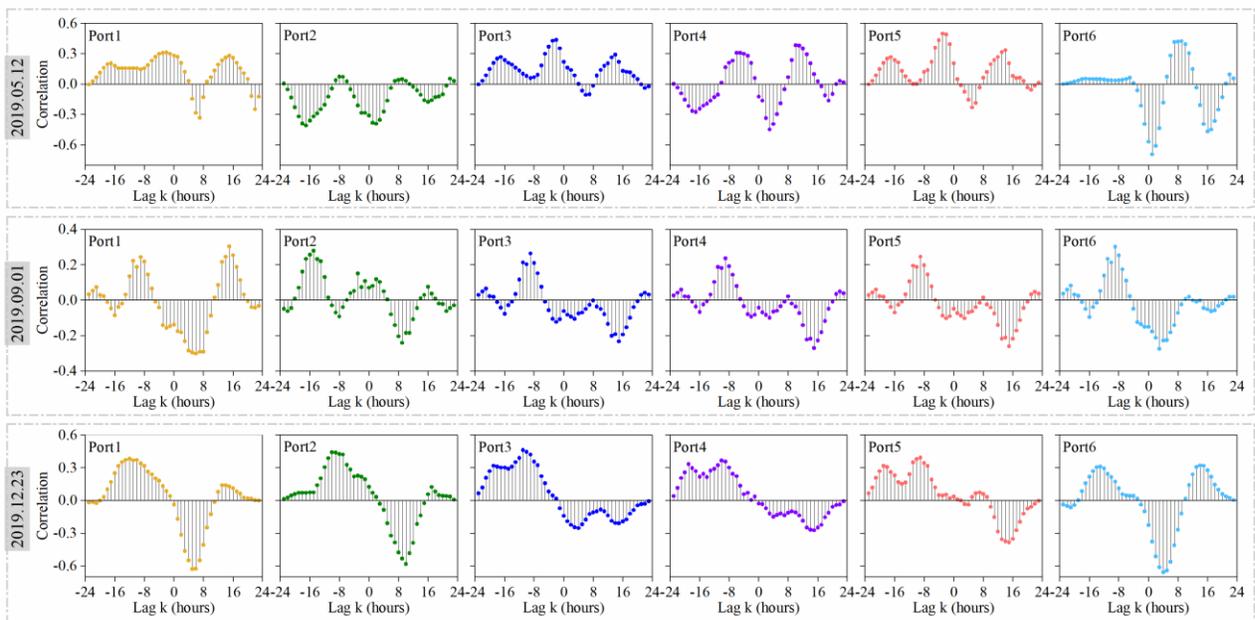
$$199 \quad CCF_{BP,GW}(\tau) = \frac{cov[BP(t),GW(t+\tau)]}{\sigma_{BP}\sigma_{GW}} \quad (1)$$

200 where $BP(t)$ and $GW(t)$ denote barometric pressure and groundwater level at time t ,
 201 respectively, σ_{BP} and σ_{GW} are their standard deviations, and τ is the time lag. Positive values of τ
 202 indicate a delayed groundwater response to barometric pressure variations.

203 CCF analysis requires quasi-stationary signals. Applying CCF to the entire filtered dataset,
 204 which may still contain nonstationary components related to recharge and long-term trends,
 205 could bias the lag time estimation. Therefore, CCF was performed on short, stationary windows
 206 dominated by barometric forcing. Groundwater level data, originally recorded at 10-minute
 207 intervals, were downsampled to hourly intervals prior to cross-correlation analysis to reduce
 208 high-frequency noise and enhance the stability of lag estimations. This resampling does not
 209 affect the frequency band of interest and preserves all relevant barometric signals.

210 Both barometric pressure and groundwater level time series were high-pass filtered with a cutoff
 211 frequency of 0.02 cpd to remove low-frequency components related to recharge and long-term
 212 trends. This filtering was essential to isolate short-term pressure-driven signals and ensure stable
 213 lag time estimation. As shown in Figure 4, to assess the temporal stability of the barometric
 214 response and minimize the influence of nonstationary signals, cross-correlation analysis was

215 performed on three representative 24-hour time windows selected from early, middle, and late
 216 stages of the monitoring period (mid-May, early September, and late December 2019,
 217 respectively). These 24-hour windows were objectively selected based on (i) minimal rainfall,
 218 (ii) stable groundwater levels, and (iii) high barometric coherence, ensuring that the analyzed
 219 signals primarily reflected pressure-driven groundwater responses. Each window also captured at
 220 least one full diurnal barometric cycle while minimizing the influence of nonstationary recharge
 221 signals. For each window, CCF was computed between atmospheric pressure and groundwater
 222 level time series, with the response lag times identified based on the lag corresponding to the
 223 maximum negative correlation within the physically meaningful positive-lag range.



224
 225 **Figure 4.** Cross-correlation functions between barometric pressure and groundwater levels at
 226 Ports 1–6, evaluated over three representative 24-h periods. The peak negative correlation
 227 identifies the lag time of groundwater response to barometric loading.

228 Across all three analysis windows, groundwater levels at all monitoring ports generally exhibited
 229 a negative correlation with atmospheric pressure at positive lag times, indicating a consistent

230 inverse barometric response. Temporally, during the early stage of the monitoring period, the lag
231 corresponding to the strongest negative correlation ranged from approximately 1 to 7 hours
232 across Ports 1–6. In the middle stage, the lag times increased to about 3–15 hours, and a
233 comparable range was observed during the late stage of the monitoring period.

234 From a vertical perspective, monitoring ports located within or immediately adjacent to the low-
235 permeability mudstone layer (Ports 1–5) consistently exhibited longer lag times than those
236 situated in sandstone units. The lower sandstone aquifer (Port 6) responded most rapidly to
237 atmospheric pressure fluctuations, while the upper sandstone aquifer (Port 1) displayed
238 intermediate lag characteristics. These differences reflect the contrasting pressure transmission
239 mechanisms associated with lithological heterogeneity. Atmospheric pressure variations can be
240 transmitted relatively rapidly to the lower sandstone aquifer at Port 6 through elastic deformation
241 of the aquifer framework, resulting in shorter response lags. In contrast, Ports 2–5, located within
242 or strongly influenced by the mudstone layer, exhibited substantially delayed responses,
243 indicating pronounced attenuation and retardation of pressure propagation in low-permeability
244 media. The intermediate lag behavior observed at Port 1 may suggest the influence of
245 unsaturated zone thickness on the barometric response. Although the absolute lag times varied
246 among different time windows, the relative depth-dependent pattern of barometric response
247 remained stable, indicating that the time-domain groundwater response to atmospheric loading
248 derived from cross-correlation analysis is temporally robust.

249 3.3 Fast Fourier Transform

250 High-frequency groundwater monitoring data commonly contain multiple overlapping signals
251 that are difficult to interpret directly in the time domain. To extract dominant periodic
252 components and clarify the underlying spectral structure, frequency-domain analysis based on

253 the Fast Fourier Transform (FFT) is widely applied (Welch, 1967; Davis, 1986). The FFT
 254 transforms a time series from the time domain into the frequency domain, decomposing periodic
 255 signals into sinusoidal components with distinct frequencies and amplitudes. In hydrogeological
 256 contexts, this approach facilitates the recognition of cyclic responses associated with external
 257 forcing and aquifer system behavior (Barco, 2010).

258 FFT analysis was performed on both atmospheric pressure and groundwater level time series
 259 using 10-min evenly sampled data. Groundwater level records were analyzed after high-pass
 260 filtering to suppress low-frequency recharge-related variations and long-term trends, whereas
 261 atmospheric pressure data were analyzed in their original form. For a discretely sampled
 262 groundwater level time series $x(n)$ with a constant sampling interval Δt , the discrete Fourier
 263 transform (DFT) is expressed as:

$$264 \quad X(k) = \sum_{n=0}^{N-1} x(n)e^{-j2\pi kn/N}, \quad k=0,1, \dots, N-1 \quad (2)$$

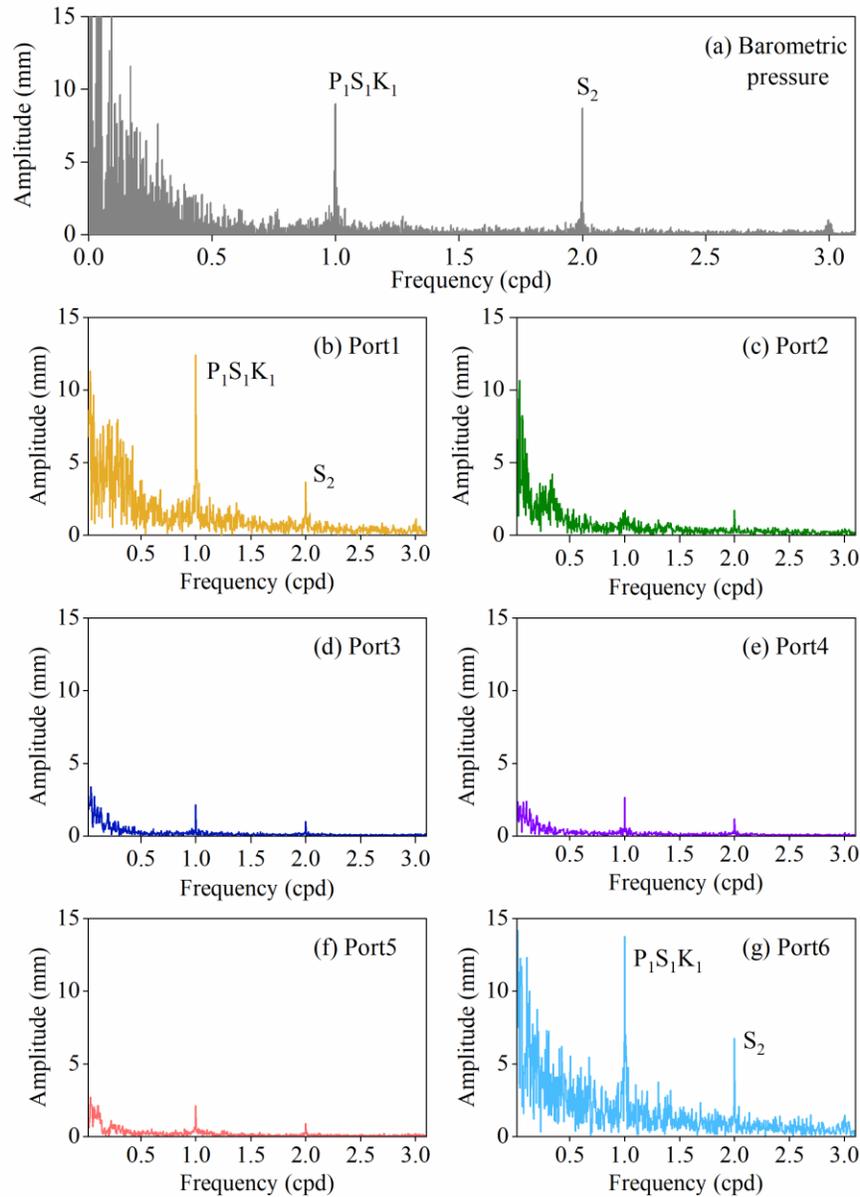
265 where N is the total number of samples, $X(k)$ represents the complex Fourier coefficient at the
 266 k -th frequency component, and j is the imaginary unit.

267 Figure 5 and Table 1 present the FFT spectra of atmospheric pressure and groundwater levels,
 268 together with the amplitudes of the main spectral components. The results show that the
 269 amplitudes of the solid Earth tide components, including O_1 (Lunar diurnal tide) and M_2 (Lunar
 270 semi-diurnal tide), are consistently small in the groundwater level spectra (generally < 1 mm).
 271 This indicates that solid Earth tides contribute negligibly to the observed groundwater level
 272 fluctuations at the study site (Weeks, 1979; Acworth et al., 2017). The barometric pressure
 273 spectrum is dominated by broadband energy below approximately 0.8 cpd, superimposed with
 274 distinct spectral peaks at 1 cpd and 2 cpd. These peaks correspond to the diurnal (S_1) and

275 semidiurnal (S_2) atmospheric tides, which are primarily driven by thermal forcing associated
276 with solar heating and ozone absorption (Chapman and Lindzen, 1969). After high-pass filtering,
277 the groundwater level spectra at all six monitoring ports exhibit corresponding peaks at 1 cpd
278 and 2 cpd, indicating persistent groundwater responses to atmospheric tidal loading throughout
279 the monitoring period.

280 Notably, marked depth-dependent differences in spectral amplitudes are observed. Monitoring
281 ports located above the mudstone layer (Port 1) and below it (Port 6) exhibit strong and well-
282 defined S_1 and S_2 peaks, with amplitudes substantially higher than those recorded at ports
283 situated within or adjacent to the mudstone layer (Ports 2–5). For example, the S_1 and S_2
284 amplitudes at Port 1 reach 12.39 mm and 3.66 mm, respectively, while Port 6 exhibits even
285 larger amplitudes of 13.64 mm (S_1) and 6.73 mm (S_2). In contrast, the corresponding amplitudes
286 at Ports 2–5 generally remain within 1–2 mm and, in some cases, approach the background noise
287 level.

288 This pronounced vertical contrast highlights the controlling role of lithological structure on the
289 transmission of atmospheric pressure signals. The mudstone layer, characterized by low
290 permeability and strong damping capacity, significantly attenuates vertical pressure propagation,
291 resulting in muted barometric responses within and near the layer. In contrast, the sandstone
292 aquifers located above and below the mudstone allow more efficient transmission of atmospheric
293 loading through elastic deformation or hydraulic adjustment mechanisms, producing clearer and
294 stronger atmospheric tide signatures in groundwater levels.



295
 296 **Figure 5.** Amplitude spectra derived from FFT analysis: (a) barometric pressure, showing
 297 dominant diurnal (S₁) and semidiurnal (S₂) components; (b)–(g) groundwater level amplitude
 298 spectra for monitoring ports Port1 to Port6, respectively. Spectral peaks at ~1 and ~2 cpd reflect
 299 periodic atmospheric influences.

300 **Table 1.** Amplitudes of the main spectral components

Component	Frequency (cycles/day)	Origin	Barometric pressure (mm)	Port1 (mm)	Port2 (mm)	Port3 (mm)	Port4 (mm)	Port5 (mm)	Port6 (mm)
-----------	------------------------	--------	--------------------------	------------	------------	------------	------------	------------	------------

O ₁	0.9295	Lunar diurnal	0.8352	0.9534	0.4967	0.1653	0.2066	0.2304	1.1941
P ₁	0.9973	Solar diurnal	6.0704	7.5658	1.3227	0.9091	1.1581	1.3025	9.0848
S ₁	1.0000	Solar diurnal	8.9761	12.3947	1.1406	2.1354	2.652	2.1456	13.6419
K ₁	1.0027	Lunar-Solar diurnal	5.3492	7.195	1.5086	0.8417	1.1673	1.065	8.2521
N ₂	1.8959	Lunar semi-diurnal	0.4721	0.7631	0.3831	0.1069	0.1187	0.0691	0.8009
M ₂	1.9323	Lunar semi-diurnal	0.7387	0.3298	0.2572	0.1934	0.0766	0.0792	0.6084
S ₂	2.0000	Solar semi-diurnal	8.6894	3.6595	1.7229	0.9772	1.1742	0.892	6.7347

3.4 Observed Barometric Response Functions

The frequency-domain barometric response of the well-aquifer system was quantified using barometric response functions (BRF), which characterize groundwater level fluctuations as a linear response to atmospheric pressure loading. In this framework, barometric pressure is treated as the input signal and groundwater level as the output, and the system behavior is described through a transfer function estimated in the frequency-domain (Bendat and Piersol, 1986; Quilty, 1991). The barometric pressure data were used in their original form (without filtering) to retain the full atmospheric pressure spectrum. The groundwater level time series, however, were high-pass filtered with a cutoff frequency of 0.02 cpd to remove low-frequency fluctuations related to recharge and long-term trends. This allowed for a more precise examination of the frequency-domain responses driven by barometric loading. The observed BRF in the frequency-domain is defined as:

$$BRF(\omega) = X_{WB}(\omega)/X_{BB}(\omega) \quad (3)$$

where $X_{WB}(\omega)$ denotes the cross-spectrum between groundwater level and barometric pressure, and $X_{BB}(\omega)$ is the auto-spectrum of barometric pressure, and ω is the angular frequency. The gain and phase response to the barometric pressure can be calculated by the modulus and the argument of $BRF(\omega)$, respectively:

$$G(\omega) = |BRF(\omega)| \quad (4)$$

$$\Phi(\omega) = \arg \{BRF(\omega)\} \quad (5)$$

320 While the BRF framework assumes linear system behavior, we recognize that the vadose zone
 321 can exhibit nonlinear responses due to the interactions between air and water in variably
 322 saturated conditions. The use of a linear framework in this study provides a simplified but
 323 practical means to quantify barometric pressure transmission. To quantify uncertainty in the
 324 estimated gain and phase, the normalized standard error $\sigma(\omega)$ was calculated to determine
 325 standard errors for gain, $\sigma A(\omega)$, and phase, $\sigma\theta(\omega)$ (Beavan et al., 1991; Bendat & Piersol, 2010;
 326 Hussein et al., 2013; Zhang et al., 2019b), which are given by:

$$327 \quad \sigma(\omega) = \left[\frac{1}{2p} \left(\frac{1}{C_{xy}(\omega)^2} \right) - 1 \right]^{1/2} \quad (6)$$

$$328 \quad p = N - (N - 1) \times \delta \quad (7)$$

$$329 \quad \sigma A(\omega) = \sigma(\omega) \times gain(\omega), \sigma\theta(\omega) = \sigma(\omega) \times \frac{180}{\pi} \quad (8)$$

330 where $C_{xy}(\omega)$ is the coherence between the water level and barometric pressure, N is the number
 331 of segments, and δ is the percentage of overlap. The calculation of coherence and its role in
 332 defining the valid frequency range for BRF analysis are described in detail in Text S2.

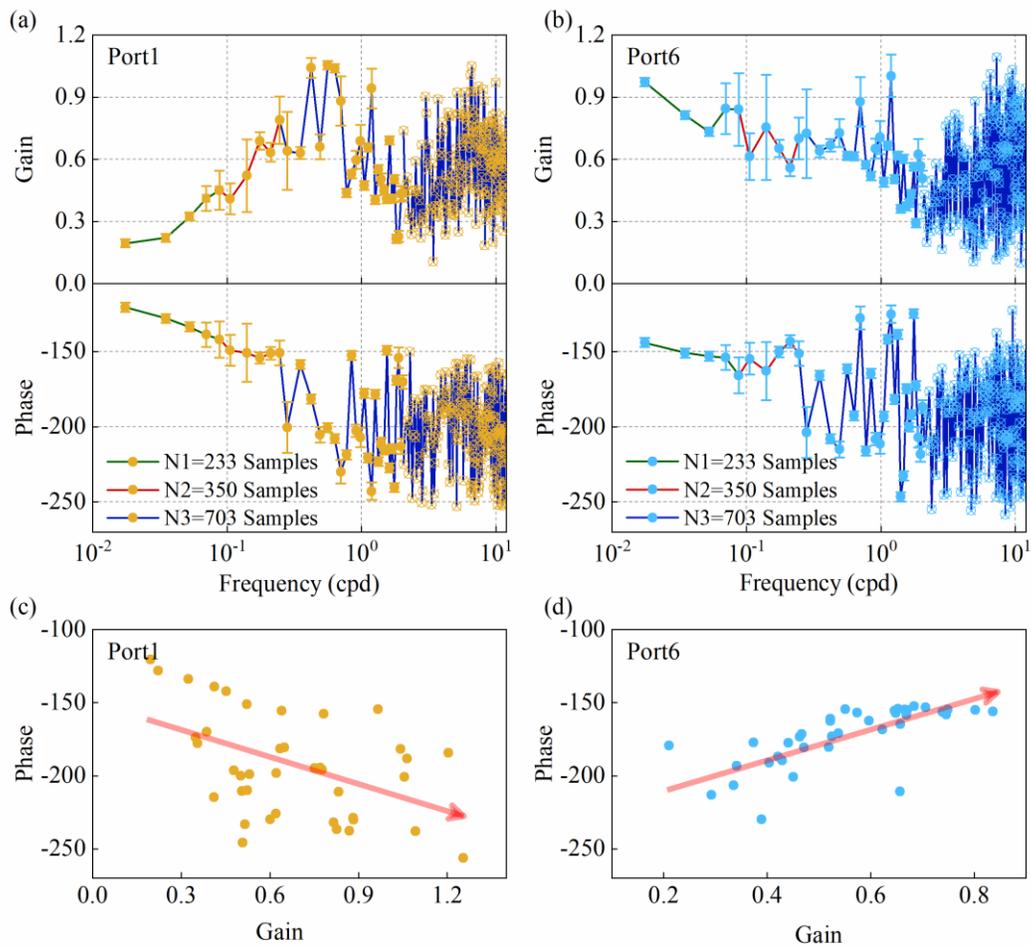
333 In the present study, detailed BRF estimation was performed primarily for Ports 1 and 6. This
 334 selection was motivated by CCF and FFT analyses, which indicated that Ports 1 and 6 exhibited
 335 strong responses to atmospheric pressure variations throughout the monitoring period. In
 336 contrast, groundwater levels recorded at Ports 2-5 showed substantially attenuated barometric
 337 signals, with long response delays and spectral amplitudes close to background noise levels,
 338 which precluded reliable identification of barometric response functions. Port 1 is screened in the
 339 upper sandstone aquifer above the mudstone layer, whereas Port 6 is screened in the lower
 340 sandstone aquifer beneath the mudstone. These two monitoring intervals therefore represent

341 contrasting hydrostratigraphic conditions within the vertically layered system. Focusing on Ports
342 1 and 6 allows for a clear comparison of barometric response behavior above and below the low-
343 permeability mudstone layer.

344 The transfer functions were estimated using Welch's averaged periodogram method (Welch,
345 1967), with a Hamming window applied to reduce spectral leakage (Lai et al., 2013). To capture
346 more low-frequency information and ensure statistical stability across a broad frequency range,
347 the same window–overlap combinations were applied consistently to both the groundwater level
348 and barometric pressure data. Window lengths of 4320, 2880, and 1440 ten-minute intervals
349 were used for both signals, with corresponding step sizes of 1440, 960, and 480 ten-minute
350 intervals, respectively. These settings correspond to window durations of 30, 20, and 10 days at a
351 10-minute sampling interval, with approximately 66.7% overlap. Gain and phase frequency plots
352 were generated to show estimates of barometric response functions for three overlapping
353 frequency bands, with the number of segments N1, N2, and N3 corresponding to 233, 350, and
354 703.

355 The viable frequency range for BRF analysis was determined based on the frequency-dependent
356 coherence between groundwater level and barometric pressure and spans 0.02–2 cpd (see Text
357 S2 for details). This range encompasses the dominant diurnal and semidiurnal atmospheric
358 pressure components while excluding low-frequency variability associated with recharge and
359 long-term trends (Rojstaczer, 1988; Rojstaczer and Riley, 1990). Gain and phase estimates
360 within this frequency band were combined across the three window configurations to obtain the
361 final BRF. For consistency with the analytical solutions of Rojstaczer (1988), 180° was
362 subtracted from the phase estimates. The resulting gain and phase spectra are shown in Figures
363 6a and 6b. Gain and phase values within the 0.02–2 cpd band were extracted to construct gain–

364 phase correlation plots (Figures 6c and 6d). Port 1 exhibits a negative gain–phase relationship,
 365 whereas Port 6 displays a positive gain–phase trend, indicating fundamentally different
 366 frequency-domain response behaviors at the two depths. These contrasting gain–phase patterns
 367 highlight systematic vertical differences in groundwater response to atmospheric loading within
 368 the layered aquifer system. The observed BRF provide the empirical basis for comparison with
 369 theoretical barometric response models, which are examined in the following section.



370
 371 **Figure 6.** Observed barometric response function for Port 1 and Port 6: (a) Gain and phase
 372 spectra for Port 1, (b) Gain and phase spectra for Port 6, (c) Scatter plot of gain versus phase
 373 for Port 1 (0.02–2 cpd, showing a negative correlation), (d) Scatter plot of gain versus phase
 374 for Port 6 (0.02–2 cpd, showing a positive correlation).

375 3.5 Theoretical Barometric Response Functions

376 The frequency-domain barometric response model for a semi-confined aquifer incorporates three
 377 physically independent processes (Fig. 7a): (1) vertical air diffusion through the unsaturated
 378 zone; (2) vertical groundwater diffusion from the water table to the aquifer; and (3) horizontal
 379 groundwater flow between the aquifer and the wellbore. The theoretical BRF, expressed in terms
 380 of gain and phase, is given by:

$$381 \quad Gain(\omega) = \left| \frac{x_0 \rho g}{A} \right| = \left| \frac{p_0 - A - s_0 \rho g}{A} \right| \quad (9)$$

$$382 \quad Phase(\omega) = \arg \left(\frac{x_0 \rho g}{A} \right) = \arg \left(\frac{p_0 - A - s_0 \rho g}{A} \right) \quad (10)$$

383 where x_0 is the amplitude of water-level fluctuation in the well, A is the amplitude of barometric
 384 loading, ρ is water density, and g is gravitational acceleration. The terms p_0 and s_0 represent the
 385 aquifer pore-pressure response and the well drawdown response, respectively. These two terms
 386 are defined as:

$$387 \quad p_0 = A(M + iN - 1 + BE) \cdot \exp[-(i + 1) \cdot Q^{0.5}] + A \cdot (1 - BE) \quad (11)$$

$$388 \quad s_0 = i0.5Wx_0K_0 \left\{ \left[W^2 \left[S_{aqu}^2 + \left(\frac{S_{con}}{2Q} \right)^2 \right] \right]^{0.25} \cdot \exp \left[0.5 \tan^{-1} \left[2Q \cdot \frac{S_{aqu}}{S_{con}} \right] \right] \right\} \quad (12)$$

389 where BE is the static barometric efficiency. The coefficients M and N describe the pneumatic
 390 response of the unsaturated zone and are given by:

$$391 \quad M = \frac{2 \cosh(\sqrt{R}) \cos(\sqrt{R})}{\cosh(2\sqrt{R}) + \cos(2\sqrt{R})}, N = \frac{2 \sinh(\sqrt{R}) \sin(\sqrt{R})}{\cosh(2\sqrt{R}) + \cos(2\sqrt{R})} \quad (13)$$

392 where K_0 is the modified Bessel function of the second kind and order zero, and S_{aqu} and S_{con}
 393 denote the storativity of the aquifer and confining layer, respectively. The dimensionless

394 parameters R , Q , and W describe the frequency-dependent behavior of the three governing
 395 processes and are defined as:

$$396 \quad R = \frac{L_{unsat}^2 \omega}{2D_{unsat}}, \quad Q = \frac{L_{con}^2 \omega}{2D_{con}}, \quad W = \frac{r_w^2 \omega}{T_{aqu}} \quad (14)$$

397 where L_{unsat} and D_{unsat} are the thickness and pneumatic diffusivity of the unsaturated zone, L_{con}
 398 and D_{con} are the thickness and hydraulic diffusivity of the confining layer, r_w is the well radius,
 399 and T_{aqu} is the aquifer transmissivity.

400 Figure 7b shows theoretical BRF of the semi-confined aquifer model was computed to simulate
 401 groundwater responses ($BE = 0.5$). R is assumed to be much less than Q ($R/Q = 0.0001$), with
 402 specific storage parameters S_{con} and S_{aqu} are set to 10^{-4} . The dimensionless parameter Q/W was
 403 varied from $10^{-1} \sim 10^3$. In the low-frequency range, the well is assumed to be in pressure
 404 equilibrium with the aquifer (i.e., $s_0=0$), where barometric loading is modulated primarily by air
 405 diffusion in the unsaturated zone and vertical groundwater diffusion. This configuration is
 406 representative of wells in unconfined or weakly confined settings, where overlying materials
 407 dominate pressure transmission. In this case, the model simplifies to the following equation for
 408 gain:

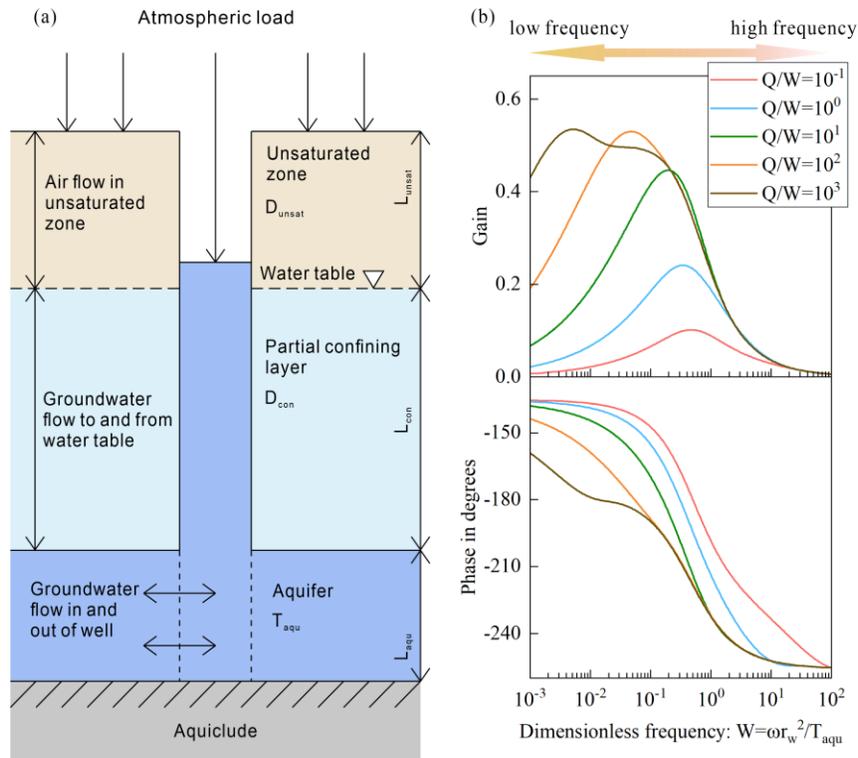
$$409 \quad Gain(\omega) = \left| \frac{p_0}{A} - 1 \right| \quad (15)$$

410 In the high-frequency range, the aquifer responds more rapidly than the well, and the effects of
 411 the unsaturated zone and confining layer become negligible. Here, the aquifer pore pressure can
 412 be considered effectively constant ($Q \rightarrow \infty$), and groundwater response is governed mainly by
 413 well-aquifer interactions. This scenario applies to wells in confined aquifers, where barometric
 414 loading propagates directly into the aquifer with minimal attenuation from overlying layers. The
 415 model is reduced to:

416

$$Gain(\omega) = \left| \frac{s_0 \rho g}{A} + BE \right| \quad (16)$$

417



418

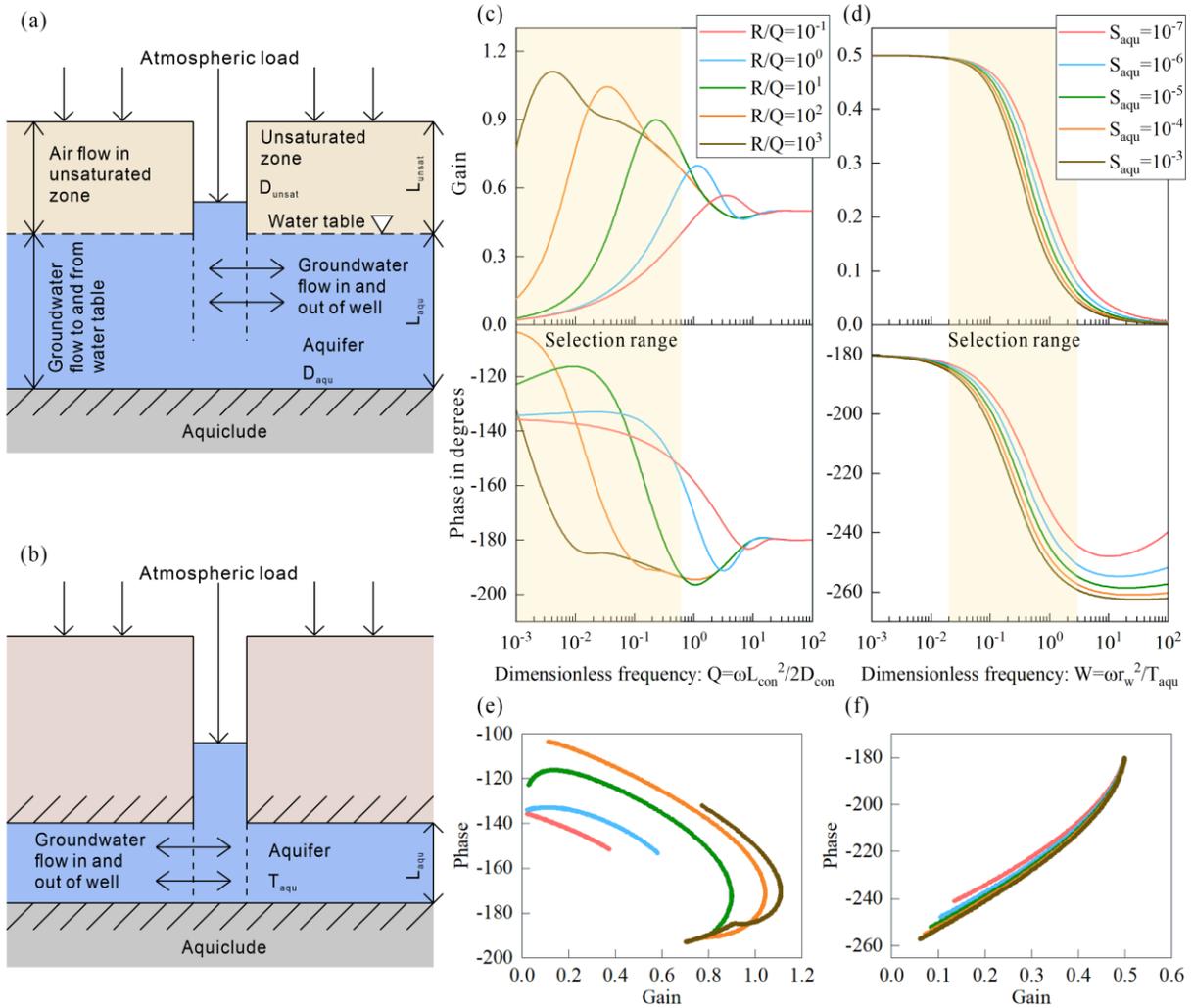
419 **Figure 7.** (a) Idealized representation of open wells under barometric loading in a semi-confined
 420 aquifer, incorporating air diffusion, vertical groundwater flow, and well-aquifer interaction
 421 (modified from Rojstaczer, 1988); (b) Theoretical BRF for semi-confined aquifers with fixed
 422 R/Q , S_{con} , and S_{aqu} but varying Q/W .

423 These two end-member cases of the semi-confined model, representing unconfined (Fig. 8a) and
 424 confined aquifer (Fig. 8b) behavior, then theoretical BRFs were computed under different
 425 contrasting aquifer conditions ($BE = 0.5$). The dimensionless parameter R/Q was set from 10^{-1}
 426 $\sim 10^3$ in the unconfined aquifer model (Fig. 8c), while for the confined aquifer model (Fig. 8d),
 427 aquifer storativity S_{aqu} ranged from $10^{-7} \sim 10^{-3}$. Figures 8e and 8f show gain–phase data points
 428 from different frequency bands, a selection that ensures each aquifer model is evaluated within
 429 the frequency domain where its characteristic response mechanisms dominate. In the unconfined

430 model, the gain–phase curves were analyzed over the low-frequency range of 10^{-3} ~0.5 cpd,
431 which is below the characteristic transition frequency associated with pressure diffusion through
432 the unsaturated zone and overlying materials. The result shows that unconfined systems exhibit a
433 negative correlation between gain and phase. However, for large values of R/Q, a transition from
434 negative to positive correlation occurs at higher frequencies, reflecting a shift from diffusion-
435 dominated to elasticity-dominated behavior. The characteristic transition frequency thus shifts
436 towards lower frequencies (Bendat & Piersol, 2010). In contrast, the confined model was
437 evaluated within a higher frequency range of 0.02~2 cpd, encompassing diurnal and semi-diurnal
438 barometric components, where pressure transmission is dominated by aquifer–well elastic
439 interaction, resulting in a pronounced positive gain–phase correlation.

440 As demonstrated in Figure 6, Port 1 exhibits a negative gain–phase correlation, consistent with
441 unconfined behavior, while Port 6 shows a positive gain–phase trend, indicative of confined
442 behavior. These contrasting patterns highlight fundamental differences in vertical hydraulic
443 connectivity and pressure transmission mechanisms.

444 Theoretical BRF models are used here not for parameter inversion but to provide a reference
445 framework for interpreting observed frequency-domain responses. Due to the strong parameter
446 coupling and non-uniqueness inherent in semi-confined models, direct fitting of model
447 parameters with barometric data alone is not feasible without independent constraints. Thus, we
448 adopt a response-based comparison approach, focusing on the qualitative and semi-quantitative
449 correspondence between observed gain–phase trends and theoretical end-member behaviors.



450
 451 **Fig. 8.** (a) Conceptual model of an unconfined aquifer governed by unsaturated and confining
 452 layer diffusion (modified from Rojstaczer, 1988); (b) Conceptual model of a confined aquifer
 453 dominated by well-aquifer interaction (modified from Rojstaczer, 1988); (c) Theoretical BRF
 454 for unconfined aquifers with varying R/Q and Q ; (d) Theoretical BRF for confined aquifers
 455 with varying S_{aqu} , represented through variations in W ($BE = 0.5$); (e) Gain–phase data points
 456 for selected frequencies in the unconfined model; (f) Gain–phase data points for selected
 457 frequencies in the confined model.

4 Discussion

458 Groundwater responses to barometric pressure, particularly within vertically distributed
459 monitoring systems, provide valuable insights into aquifer confinement and pressure
460 transmission mechanisms. Time-domain cross-correlation and frequency-domain spectral
461 analyses across six monitoring ports consistently revealed pronounced contrasts in barometric
462 response behavior between sandstone and mudstone intervals. All ports exhibited inverse
463 barometric responses, with systematic variations in response lags and spectral amplitudes
464 according to lithology. These results suggest that hydrostratigraphic contrasts, rather than
465 monitoring depth alone, exert a dominant influence on pressure transmission dynamics. Ports
466 screened within sandstone units exhibited shorter response lags and higher spectral amplitudes,
467 whereas those located within or adjacent to mudstone layers displayed attenuated and delayed
468 responses, highlighting the strong damping effect imposed by low-permeability strata.

470 FFT analyses further demonstrated that atmospheric pressure signals at diurnal and semi-diurnal
471 frequencies were consistently recorded in groundwater level spectra, with higher amplitudes in
472 sandstone-associated ports compared to mudstone-associated intervals. This indicates that
473 vertical heterogeneity in barometric pressure transmission is primarily governed by
474 hydrostratigraphic contrasts, with even relatively thin mudstone layers significantly attenuating
475 and delaying pressure signals. These findings provide the foundation for interpreting contrasting
476 gain–phase relationships observed in frequency-domain BRF analyses.

477 In semi-confined aquifers, the barometric response function exhibits a pronounced frequency
478 dependence, which can be divided into three distinct bands. The low-frequency response is
479 controlled by vertical pneumatic diffusivity and thickness of the unsaturated zone, and by
480 vertical hydraulic diffusivity and thickness of the confining unit. The mid-frequency response

481 corresponds to static barometric efficiency, while the high-frequency response is increasingly
482 influenced by well–aquifer interaction. The unconfined aquifer system exhibits similar
483 frequency-dependent behavior, also dividing into three bands. At low frequencies, the response
484 is largely governed by the aquifer's specific yield, storativity, and vertical hydraulic conductivity.
485 Mid-frequency behavior reflects the relative magnitudes of gas diffusivity in the unsaturated
486 zone and vertical hydraulic diffusivity within the aquifer. At high frequencies, a phase plateau
487 near -180° emerges, with the unsaturated zone functioning similarly to a confining layer,
488 resulting in gain magnitudes comparable to the static barometric efficiency expected under
489 confined conditions. Port 1, screened in an upper sandstone unit, reflects typical free-surface
490 conditions consistent with an unconfined aquifer. Spectrally, Port 1 exhibits an inverse trend
491 between gain and phase across low- to mid-frequency ranges, where gain slightly increases while
492 phase decreases with frequency. This negative gain-phase correlation is typical of unconfined
493 systems, influenced by vadose zone thickness, air–water interactions, and boundary
494 heterogeneity (Rojstaczer & Riley, 1990; Li et al., 2012). Although similar patterns can appear in
495 semi-confined systems over specific frequency bands, Port 1's geological context and static
496 water table conditions suggest it most closely represents a typical unconfined aquifer response.
497 In confined aquifer systems, barometric disturbances propagate rapidly via elastic deformation of
498 both pore water and the aquifer matrix, leading to coherent and prompt water level responses,
499 particularly at low frequencies. Gain decreases monotonically with frequency, and phase lag
500 progressively shifts, resulting in a persistent positive correlation between gain and phase. This
501 synchronized decay reflects the elastic storage response, primarily governed by aquifer-specific
502 storativity (S_0) (Narasimhan & Kanehiro, 1984; Rojstaczer, 1988). Port 6, screened in the lower
503 sandstone aquifer beneath a thin mudstone layer, exhibits a positive gain-phase relationship

504 typical of a confined system, reflecting functional confinement induced by the low-permeability
505 mudstone layer. While confined-like responses were observed at Port 6, these are more likely
506 attributable to localized hydraulic impedance imposed by the thin mudstone layer, rather than
507 indicating a fully confined aquifer in the traditional sense. This highlights the scale sensitivity of
508 BRF analysis, emphasizing its ability to detect functional confinement even in systems with fine
509 vertical resolution.

510 The joint evolution of gain and phase across frequencies provides a robust framework for
511 interpreting barometric response behavior in vertically heterogeneous groundwater systems.
512 Rather than serving as a strict classification tool, gain-phase co-variation reflects frequency-
513 dependent response regimes influenced by pressure transmission pathways, storage mechanisms,
514 and hydraulic impedance imposed by low-permeability layers. Monitoring intervals exhibiting
515 opposite or synchronous gain-phase trends correspond to contrasting modes of barometric signal
516 propagation, closely related to differences in functional confinement and vertical hydraulic
517 connectivity. This response-based approach transcends static lithologic descriptions, offering a
518 dynamic interpretation of aquifer behavior under atmospheric forcing.

519 It is important to note that the high-pass filtering used to remove rainfall effects inherently
520 suppresses low-frequency groundwater dynamics related to long-term recharge or storage
521 processes. Although zero-phase filtering was applied to avoid phase distortion, the magnitude of
522 phase lag is sensitive to preprocessing choices. As such, phase-based interpretations in this study
523 are emphasized comparatively rather than as absolute metrics, focusing on relative differences in
524 barometric response characteristics.

525 5 Conclusions

526 This study investigated groundwater responses to barometric loading using a vertically distributed
527 multilevel monitoring system in a layered aquifer. Time-domain cross-correlation and frequency-
528 domain spectral analyses across six monitoring ports revealed pronounced lithology-controlled
529 differences in groundwater responses to atmospheric pressure variations. Monitoring ports
530 screened within sandstone units exhibited stronger barometric signals, whereas those located
531 within or adjacent to mudstone layers showed markedly attenuated responses, highlighting the
532 damping effect imposed by low-permeability strata on pressure transmission.

533 Frequency-domain barometric response function (BRF) analysis conducted for the two most
534 barometrically sensitive ports further highlighted contrasting response behaviors. Port 1 located in
535 the upper unconfined sandstone exhibited a negative gain–phase co-variation, consistent with
536 delayed and attenuated pressure transmission influenced by unsaturated zone buffering and
537 drainage processes. In contrast, Port 6 screened in sandstone beneath a thin mudstone layer
538 displayed a positive gain–phase relationship, indicative of a confined-like elastic response
539 characterized by synchronous attenuation of gain and phase. Comparison with theoretical BRF
540 models demonstrates that these contrasting gain–phase patterns arise from fundamentally different
541 pressure transmission regimes associated with unconfined and functionally confined conditions.
542 This study specifically emphasized functional confinement, which reflects pressure transmission
543 controlled by the elastic properties of the aquifer and overlying materials, as opposed to the
544 traditional rigid-flow assumption that treats confinement as a static condition governed by
545 impermeable layers.

546 Overall, the results show that vertically resolved, frequency-domain analysis of barometric
547 responses provides a robust, physically grounded framework for interpreting pressure transmission

548 behavior and vertical hydraulic connectivity in heterogeneous aquifer systems. Rather than serving
549 as a strict classification tool for aquifer types, gain–phase co-variation reflects frequency-
550 dependent response regimes controlled by hydrostratigraphic structure and hydraulic impedance.
551 This response-based perspective underscores the value of multilevel groundwater monitoring
552 under natural atmospheric forcing for elucidating subsurface pressure dynamics in layered systems.
553 The study demonstrates the potential of frequency-domain BRF analysis for quantifying vertical
554 heterogeneity in pressure transmission mechanisms in layered aquifer systems. It highlights the
555 utility of this approach in interpreting functional confinement and vertical hydraulic connectivity
556 based on observed barometric response behaviors.

557 **Acknowledgments**

558 This research is financially supported by the Opening Fund of State Key Laboratory of
559 Geohazard Prevention and Geoenvironment Protection (SKLGP2017K001 and
560 SKLGP2018K003), and Program of China Scholarship Council (Grant No.202409230004).

561 **Open Research**

562 Data are available upon reasonable request from the corresponding author.

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